

Speckle Reduction Using Multiple Tones of Illumination

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The occurrence and smoothing of speckle are studied as a function of the line width for a highly collimated illuminating source. A general theory is presented for speckling in the image of a partially diffuse, phase type of object, which has a variable number of random scattering centers per resolution element. Then, an expression is derived for the wavelength spacing required to decouple the speckle patterns arising from two monochromatic tones in an imaging system, thereby establishing that it is feasible to smooth speckle using multicolor illumination. This theory is verified in a series of experiments using both laser illumination and band-limited light from a carbon arc. With highly collimated sources, we show that speckle appears laserlike for an imaged diffuser even up to line widths of 5 Å. Then, smoothing of speckle is demonstrated in the imaging of a diffuser and for a section of an optic nerve when the illumination is provided by six narrow lines spread over 1500 Å. Since with color-blind, panchromatic viewing the speckle smooths, a direct extension of this method to holographic microscopy, using a multitone laser, should permit one to record and reconstruct holograms of diffraction-limited resolution that are essentially speckle-free.

Introduction

Under monochromatic illumination, objects with a scale of roughness grossly on the order of the wavelength are hard to discern in feature detail, owing to the rapid spatial variations that occur in the scattered radiation. This characteristic of laser illumination to speckle has been studied by many investigators; however, owing to space limitations, we cite only a few of the publications.¹⁻²² It is difficult to quote a specific numerical value for this resolution loss since it varies widely with the roughness of the object being studied. However, in the application of laser holography to microscopy, this speckle effect has been a severe obstacle,^{8-10,12,17,20} limiting the *working* resolution to from a few to several times the classical optics limit. As examples, Young *et al.* report that "the usual resolution criterion should be divided by five or more whenever diffused laser light is used"¹²; Close reports resolutions of a few microns on test samples¹⁷; and Cox *et al.* have obtained similar resolutions with biological specimens.¹⁰

Gabor¹⁴ has classified speckle into two categories: The *objective* speckle that arises owing to uneven illumination falling on the subject. The *subjective* speckle that arises from the roughness of the subject in conjunction with the convolving effect of a finite aperture. The objective type can occur when one holographically records a smooth transparency but

with a diffuser placed in the beam illuminating the transparency. While the diffuser creates a helpful redundancy in the recording, it also leads to the deleterious speckle. Most prior studies of speckle elimination have considered only this objective type, and good results have been reported, although the subject is far from closed.^{5-9,14,22}

In this paper we consider the smoothing of subjective speckle. This is a somewhat neglected topic, since it has been generally argued that the only effective means for smoothing this type is to increase the aperture.¹⁴ However, if one draws this conclusion, it is implicitly assumed that operation is at a single wavelength or that separate, independent looks are not being made in the over-all process. In the method we are to describe, separate wavelengths are used to provide independent looks.^{20,21} In this way, we will show that one can smooth subjective speckle at a fixed value of aperture. Probably, too, a method that smooths subjective speckle also smooths the objective type (but not conversely). Hence, in this instance, the need for making the distinction is not great.

An analysis for the wavelength variation of speckle in an imaging system has not been found in the literature; however, Goodman has treated the related problem of the wavelength sensitivity of speckle in the far-field region of a coherently illuminated group of scatterers.² Recent experiments have been reported in confirmation of the thesis that speckle patterns vary spatially in a marked way with change in wavelength.¹⁹⁻²¹

We feel that an interesting possibility for dramati-

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cally reducing the speckle effect in holographic microscopy is to use a multicolor recording process with several widely spaced laser tones spanning the visible optical region. The hologram-volume effects permit one to record and play back these images in a noninteracting way, provided that adequate spatial separation and wavelength intervals have been chosen between each reference beam.²³ In viewing, the same multitone spectra are used for the reference beams so that no spatial distortions occur, but a color-blind monitor with uniform response over the visible spectrum must be provided, e.g., by a vidicon apparatus, in order to average the multitone speckle.

Within this context, we report the first study of the spatial variations of speckle in the imaging system of a microscope as the wavelength of a monochromatic source is scanned through the visible. First, we analyze the imaging of a diffuser in which there is a variable number of random phase heights per resolution cell. This is a good model for the objects of practical interest covering the smooth case, through the troublesome case where five to ten random scatterers per resolution element are limiting the resolution, and the case where the number of random contributors per resolution cell is very high. We show that the multicolor speckle will decorrelate when

$$\lambda_2 - \lambda_1 \geq (\lambda_0^2 / 2\pi n_3 h_0) \{ [1 - e^{-(ph_0)^2}] / [1 + (N-1)(ph_0)^2 e^{-(ph_0)^2}]^{1/2} \},$$

where the n_3 is the difference in the refractive index of the air and the diffuse object, N is the number of scatterers per resolution cell, and the heights h_r of the scatterers have been assumed to have a normal distribution with an expected value of zero and a standard deviation h_0 , $p = -2\pi n_3 / \lambda_0$, and $\lambda_0 = (\lambda_1 + \lambda_2) / 2$. As an alternative interpretation, speckle will appear laserlike as a given line width increases from the few hertz band up to a small fraction of the above $\lambda_2 - \lambda_1$ (this fraction is typically a few angstroms). We note too that wavelength diversity may also prove useful in *electron microscopy* where the monoenergetic electrons typically have a monochromaticity $d\lambda/\lambda \lesssim 10^{-5}$, where λ is the de Broglie wavelength of the electron. This is easily small enough to cause speckle, however a further consideration of speckle in matter waves is beyond the scope of this paper.

Analysis of Diffuser Imaging

An imaging system for a microscope is idealized by a lens of focal length F and aperture D , an input plane (ξ, η) at a distance $s' = F + \delta$ from the lens (Fig. 1), and thus with the image plane at a distance s given by $1/s + 1/s' = 1/F$. For monochromatic illumination, $e^{i\omega t}$, of an arbitrary object D_0 , we describe the transverse scalar component of the input electric field by $f(\xi, \eta)e^{i\omega t}$. In the image plane, this corresponding field amplitude is found by two applications of the usual Fresnel-zone approximation of Sommerfeld's formula²⁴; i.e., the output field amplitude $E(x, y)e^{i\omega t}$ is given by

$$E(x, y) = - \frac{\exp[-(i2\pi/\lambda_0)(s + s')]}{\lambda_0^2 s s'} \times \iiint_{-\infty}^{\infty} d\xi d\eta dudv f(\xi, \eta) T(u, v) \times \exp \left\{ - \frac{i\pi}{\lambda_0 s'} [(u - \xi)^2 + (v - \eta)^2] - \frac{i\pi}{\lambda_0 s} [(x - u)^2 + (y - v)^2] \right\}, \quad (1)$$

in which (u, v) are Cartesian coordinates in the plane of the lens, $\lambda_0 = 2\pi c/\omega$, and $c = 3 \times 10^8$ m/sec. The transmission function for the lens $T(u, v)$ will be taken with the spherical convergence factor $\exp[+(i\pi/\lambda_0 F)(u^2 + v^2)]$ and a pupil function that is Gaussian, i.e., it is given by

$$T(u, v) = \exp[-(i\pi/\lambda_0)(u^2 + v^2)/\rho], \quad (2a)$$

where

$$1/\rho = -(1/F) - (i4\lambda_0/\pi D^2), \quad (2b)$$

and D is the diameter of the lens of focal length F .²⁵ Substitution of Eq. (2) into Eq. (1) and integration over the (u, v) plane, defining the magnification factor $M = s/s'$ and the up-scaled variables $x' = -M\xi$, $y' = -M\eta$, give the result:

$$E(x, y) = - \frac{\exp\{-i2\pi/\lambda_0(M+1)s' - (i\pi/\lambda_0)[(x^2 + y^2)/Ms']\}}{\lambda_0^2 s'^2 M^3} \times \frac{\pi D^2}{4} \iint_{-\infty}^{\infty} dx' dy' f\left(-\frac{x'}{M}, -\frac{y'}{M}\right) \exp \left\{ - \frac{i\pi}{\lambda_0 s'} \left[\frac{(x'^2 + y'^2)}{M^2} \right] - \left(\frac{\pi D}{2\lambda_0 s} \right)^2 [(x - x')^2 + (y - y')^2] \right\}. \quad (3)$$

In the basic imaging equation, Eq. (3), the convolving effect of a finite aperture, D , is readily seen. As is well known, subjective speckle arises from this averaging or smearing of the input function $f(-x'/M, -y'/M)$, i.e., for a finite aperture $E(x, y)$ will not be a perfectly resolved scaled replica of $f(-x'/M, -y'/M)$. The departures here from the usual imag-

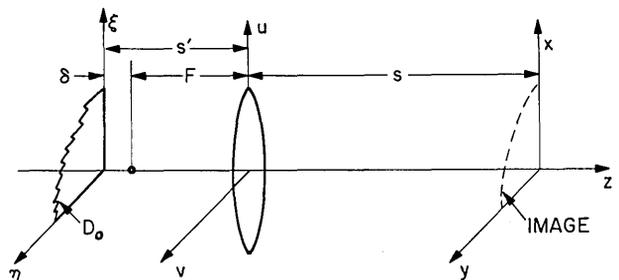


Fig. 1. Single lens magnification with object plane (ξ, η) and image plane (x, y) .

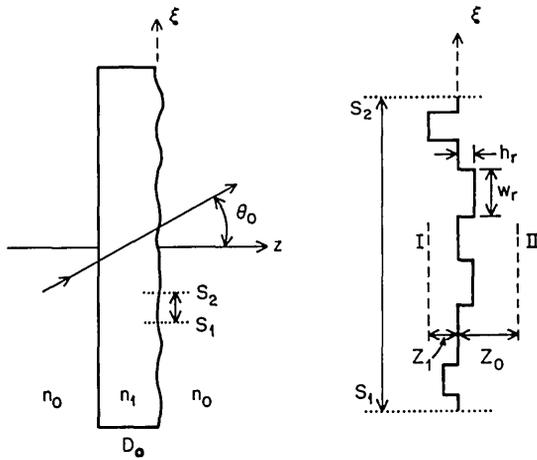


Fig. 2. The idealized diffuser object (D_0) in the (ξ, η) plane showing a magnified inset between S_1S_2 for the computation of the transmission function, Eq. (10). The diffuser has steps of width w_r and random height h_r .

ing formula are that phase terms have been retained and the Gaussian transmission function of Eq. (2) is used. Hence, it is instructive to find the radius of the resolution cell for comparison to the conventional circular pupil function. By integration of Eq. (3) with a delta function impulse as input, i.e., $f = \delta(x', y')$, we find that the output spot size is given by

$$\bar{E}(x, y) \propto \exp[-(\pi D/2\lambda_0 s)^2 (x^2 + y^2)].$$

Thus, in the output plane (x, y) , the intensity falls to a $1/e^2$ fraction of its peak at a radius of $0.637\lambda_0 s/D$. From this impulse interpretation, we define the radius of the resolution cell referenced to the (x, y) plane or the (ξ, η) plane, respectively, as

$$\Delta w = (2\lambda_0 s / \pi D) \text{ or } \Delta w_0 = (2\lambda_0 s' / \pi D). \quad (4)$$

If we would have used the usual circ $[(u^2 + v^2)^{1/2}/(D/2)]$ as the pupil function portion of Eq. (2a), the resulting Airy disk would have the function value $[2J_1(z)/z]^2$. This would result in a radius for the $1/e^2$ power down locus of $0.82 \lambda_0 s/D$, which is close enough for our purposes to the corresponding value of $0.637 \lambda_0 s/D$, obtained for a Gaussian pupil function.²⁶

Model for the Phase-Type Diffuser

There have been various ways, in the past, of describing the electric field transmitted by a rough object. Hopkins and Tiziani,¹⁶ for instance, idealize the diffuser as a series of closely packed lenslets of varying sizes and focal length. Enloe⁴ and Goodman,² on the other hand, idealize the diffuser as a randomly spaced array of infinitesimal radiators, each radiating with a random phase.

A semitransparent object of complex-valued amplitude transmission factor $D_0(\xi, \eta)$ is placed in the input plane and illuminated by a monochromatic plane wave incident at the polar angle θ_0 in the (ξ, η) plane (Fig. 2). Thus, the input amplitude function $f(\xi, \eta)$ is given by

$$f(\xi, \eta) = D_0(\xi, \eta) \exp[-i(2\pi/\lambda_0)n_0\xi \sin\theta_0], \quad (5)$$

where n_0 and n_1 are the relative indices of refraction in the two media and $n_0 \sin\theta_0 = n_1 \sin\theta_1$. For a general object consisting of an amplitude transmittance, denoted by real-valued function $D_1(\xi, \eta)$ and the phase delay $\psi(\xi, \eta)$, we write

$$D_0(\xi, \eta) = D_1(\xi, \eta) \exp[-i\psi(\xi, \eta)]. \quad (6)$$

For the surface contour $h(\xi, \eta)$ of the diffuser (shown between planes I and II spaced by $Z_0 + Z_1$ in Fig. 2), we use a ray optics approximation to $\psi(\xi, \eta)$. Thus, we write the phase delay

$$\psi(\xi, \eta) = (2\pi n_0/\lambda_0)(Z_0 - h)/\cos\theta_0 + (2\pi n_1/\lambda_0)(Z_1 + h)/\cos\theta_1;$$

and suppressing the nonessential constant phase delays, we can rewrite Eq. (5) as follows:

$$f(\xi, \eta) = D_1(\xi, \eta) \exp[-(i2\pi/\lambda_0)n_0\xi \sin\theta_0] \exp\left[-\frac{i2\pi}{\lambda_0}n_3h(\xi, \eta)\right], \quad (7)$$

in which $n_3 = (n_1/\cos\theta_1 - n_0/\cos\theta_0)$.

Now, consider the simplified one-dimensional case with a pure phase object, i.e., $D_1 = 1$, consisting of randomly positioned steps of height h_r and width w_r centered at $\xi = \xi_r$, i.e.,

$$h(x, y) = \sum_r h_r \text{rect}[(\xi - \xi_r)/w_r].$$

Then, the one-dimensional idealization of Eq. (7) becomes

$$f(\xi) = \exp[-(i2\pi/\lambda_0)n_0\xi \sin\theta_0] \exp\left\{-\left(\frac{i2\pi}{\lambda_0}\right) n_3 \sum_r h_r \text{rect}[(\xi - \xi_r)/w_r]\right\}, \quad (8)$$

where the function $\text{rect}(x) = 1$ when $|x| < 1/2$ and is zero otherwise. If nonoverlapping steps are assumed in the expression

$$\sum_r h_r \text{rect}[(\xi - \xi_r)/w_r],$$

one can prove the following identity:

$$\exp\left\{-\left(\frac{i2\pi}{\lambda_0}\right)n_3 \sum_r h_r \text{rect}[(\xi - \xi_r)/w_r]\right\} = 1 + \sum_r \text{rect}[(\xi - \xi_r)/w_r] \{\exp[-(i2\pi/\lambda_0)n_3 h_r] - 1\}.$$

Substituting this into Eq. (8) we obtain

$$f(\xi) = \exp[-i(2\pi/\lambda_0)n_0\xi \sin\theta_0]$$

$$\left(1 + \sum_r \text{rect}[(\xi - \xi_r)/w_r] \left\{ \exp[-i(2\pi/\lambda_0)n_3h_r] - 1 \right\}\right) \quad (9)$$

Equation (9) for a pure phase type of diffuser could equally well have been postulated directly, as follows. The multiplicative term $\exp[-i(2\pi/\lambda_0)n_0\xi \sin\theta_0]$, with the linear phase taper in (ξ) , occurs for a plane wave incident at an angle θ_0 , as shown in Fig. 2. With nonoverlapping steps assumed in the

$$\sum_r \text{rect}[(\xi - \xi_r)/w_r],$$

the term within the square brackets, $[\]$, is either 1 or $\exp[-i(2\pi/\lambda_0)n_3h_r]$. This holds for an arbitrary value of ξ , hence $|f(\xi)| \equiv 1$ as it must for a pure phase object.

We could adapt this transmitted field to fit a variety of models for the diffuser. Thus we can consider the height of a step given by $h_r(\xi)$ to be roughly constant over the width w_r . On the other hand, if one prefers the randomly positioned lenslets of Hopkins and Tiziani, then h_r becomes the quadratic phase transmission for each lens, i.e., $h_r(\xi) = [(\xi - \xi_r)^2/f_r]$, where f_r is the focal length of the lenslet centered at ξ_r .

If we make the assumption that the width of each random step is much less than the resolution cell size, i.e., $w_r \ll \Delta w_0$, then insofar as integrations of the form of Eq. (3), we can replace the $\text{rect}[(\xi - \xi_r)/w_r]$ by the Dirac delta function, i.e., by $w_r\delta(\xi - \xi_r)$. Thus, combining Eqs. (8) and (9), we find a convenient approximation for the one-dimensional input transmittance

$$f(\xi) = \exp\left[-\left(\frac{i2\pi}{\lambda_0}\right)n_0\xi \sin\theta_0\right]$$

$$\left(1 + \sum_r w_r\delta(\xi - \xi_r) \left\{ \exp[-i(2\pi/\lambda_0)n_3h_r] - 1 \right\}\right). \quad (10)$$

To facilitate the consideration of our diffuser, we arbitrarily define the one-dimensional lens process, reducing Eq. (3), as follows:

$$E_1(x) = \exp[-i\pi n_0/\lambda_0(x^2/Ms')] \int_{-\infty}^{\infty} dx' f\left(-\frac{x'}{M}\right) \exp\left\{-\frac{i\pi n_0(x')^2}{\lambda_0 M^2 s'} - \left[\frac{(x-x')}{\Delta w}\right]^2\right\}. \quad (11)$$

Substitution of Eq. (10) into Eq. (11) and integrating give

$$E_1(x) = \Delta w(\pi)^{1/2} \exp\left[-\frac{i\pi n_0}{\lambda_0} \left(\frac{x^2}{Ms'} - \frac{2x \sin\theta_0}{M}\right) - \frac{4\pi n_0^2 x^2 \sin^2\theta_0}{\lambda^2 M^2}\right] + \exp\left[-\frac{i\pi n_0}{\lambda_0} \left(\frac{x^2}{Ms'}\right)\right] \\ \times \sum_r \exp\left[-\left(\frac{x-x_r'}{\Delta w}\right)^2 + \frac{i\pi n_0}{\lambda_0} \left(\frac{2x_r' \sin\theta_0}{M} - \frac{(x_r')^2}{M^2 s'}\right)\right] \\ \times M w_r \left[\exp\left(-\frac{i2\pi}{\lambda_0} n_3 h_{r-1}\right) - 1\right]. \quad (12)$$

Now define the intensity or energy density factor by $I(x) = E_1 E_1^*$, and from Eq. (12) we find

$$I(x) = \pi(\Delta w)^2 e^{-2\alpha} + 2(\pi)^{1/2} \Delta w e^{-\alpha} \sum_r M w_r \\ \exp\left[-\left(\frac{x-x_r'}{\Delta w}\right)^2\right] \left\{ \cos(\chi - \phi_{1r} + \phi_{2r}) - \cos(\chi - \phi_{1r}) \right\} \\ + 2 \sum_r \exp[-2(x-x_r')^2/(\Delta w)^2] (M w_r)^2 [1 - \cos\phi_{2r}] \\ + \sum_{\substack{m \\ m \neq r}} \sum_r \exp\left[-(x-x_m')^2/(\Delta w)^2 - (x-x_r')^2/(\Delta w)^2\right] \\ \times \exp[i(\phi_{1m} - \phi_{1r})] \\ \times M^2 w_m w_r (e^{-i\phi_{2m}} - 1)(e^{+i\phi_{2r}} - 1), \quad (13)$$

in which $\alpha = 4\pi(n_0 x \sin\theta_0)^2/(\lambda_0 M)^2$,

$$\chi = (2\pi/\lambda_0)(n_0 x \sin\theta_0/M),$$

$$\phi_{1r} = (\pi n_0/\lambda_0)\{2x_r' \sin\theta_0/M - (x_r')^2/(M^2 s')\}, \text{ and}$$

$$\phi_{2r} = (2\pi/\lambda_0)n_3 h_r.$$

Equation (13) is a convenient starting point for the statistical analysis of decorrelation based on combining intensity patterns taken at *separate* wavelengths.²¹ Equation (12) is the more useful starting point in the simpler amplitude decoupling criterion presented in Eq. (21) of the following section.

Expected Value and Variance for the Electric Field

To calculate the wavelength spacing required to decouple the speckle pattern described by Eqs. (12) and (13), first we analyze the simpler case when θ_0 is constant, e.g., when $\theta_0 = 0$. Later separate comment is included for the important case when a distributed angular spectrum is used for the illumination.

We assume the response of a panchromatic viewing system is given by $I = E_1 E_1^* + E_2 E_2^* + \dots$ when there are multiple tones of monochromatic illumination, i.e., beat terms are negligible with long exposure times. Hence, we must compare the intensities in the image plane at two different wavelengths and find when these two intensity patterns are decorrelated. Since in computing $E_1 E_1^*$, common phase terms will cancel, we factor Eq. (12) extracting and suppressing the term $\exp\{(i\pi n_0/\lambda_0)[(2x \sin\theta_0/M) - (x^2/Ms')]\}$. The *remainder* of the electric field we denote by E_1 , and rewriting Eq. (12) gives

$$E_1(x) = \Delta w(\pi)^{1/2} + \sum_r \exp\left[-\left(\frac{x-x_r'}{\Delta w}\right)^2 - \frac{i\pi n_0(x_r')^2}{\lambda_0 M^2 s'}\right] M w_r \left\{ \exp\left(-\frac{i2\pi}{\lambda_0} n_3 h_r\right) - 1 \right\}. \quad (14)$$

Additionally, comparing Eqs. (12) and (14), one will note that we have dropped the quadratic multiplier $\exp[-4\pi n_0^2 x^2 \sin^2\theta_0/(\lambda_0^2 M^2)]$ from the first term in Eq. (14); and the *small* phase term $\exp\{(i\pi n_0/\lambda_0)[2(x_r' - x) \sin\theta_0/M]\}$ from the summation.

To study the speckle in the image plane, we consider an arbitrary position x . In Eq. (14), the rapid falloff of the Gaussian term, $\exp\{-[(x - x_r')/\Delta w]^2\}$, limits the number of scatterers from among the entire set x_r' that contribute effectively to \mathbf{E}_1 at x . Thus, if there are N scatterers remaining from this set that are positioned (in image plane coordinates) with values of x_r' in the range $x - \Delta w < x_r' < x + \Delta w$, then we can approximate Eq. (14) by

$$\mathbf{E}_1(x) = A - BN + B \sum_{r=1}^N \exp(+iph_r). \quad (15)$$

We have defined $A = \Delta w(\pi)^{1/2}$,

$B = Mw_c \exp[-(i\pi n_0 x^2)/(\lambda_0 M^2 s')]$ and p as

$$p = -(2\pi n_3/\lambda_0). \quad (16)$$

To simplify the analysis, we assume that the step widths w_r are constant for all scatterers and equal to w_c . Also, with negligible error, the Gaussian permits us to approximate the phase term $\exp[-[i\pi n_0(x_r')^2/\lambda_0 M^2 s']]$ in Eq. (14) by the term $\exp[-[i\pi n_0 x^2/\lambda_0 M^2 s']]$ in Eq. (15).

If we assume that the real random variable h_r is distributed according to some known density function, $f(h_r)$, and the corresponding characteristic function for this distribution is given by $F(p) = \int_{-\infty}^{\infty} \exp(+iph) f(h) dh$, then we also obtain the following results for the expectation and variance of e^{iph} (Ref. 27):

$$\langle e^{iph} \rangle = F(p), \quad (17)$$

$$\sigma^2(e^{iph}) = 1 - F(p)F^*(p). \quad (18)$$

If we also assume that the random variables h_r represented by different scattering points are independent, then we can calculate the expected value and variance of our amplitude defined by Eq. (15). Thus, we obtain the following expression for the expected value of the electric field at a point in the image plane

$$\langle \mathbf{E}_1(x) \rangle = A - NB + BNF(p). \quad (19)$$

Also, the variance in this electric field, defined by $\sigma^2[\mathbf{E}_1(x)] = \langle (\mathbf{E}_1 - \langle \mathbf{E}_1 \rangle) (\mathbf{E}_1 - \langle \mathbf{E}_1 \rangle)^* \rangle$, is readily computed by substitution of Eq. (15) into this form and simplification using Eqs. (17)–(19). The resulting expression for the variance in the electrical field is

$$\sigma^2[\mathbf{E}_1(x)] = N(1 - FF^*)BB^*, \quad (20)$$

where $BB^* = (Mw_c)^2$ and the characteristic function F is given by Eq. (17).

Wavelength Spacing for Speckle Decorrelation

We note that our expected value is some complex number, while the variance is a real number since it

is defined by $\sigma^2 = \langle |\mathbf{E}_1 - \langle \mathbf{E}_1 \rangle|^2 \rangle$. Thus, Eq. (20) gives us the square of the radius of a circle centered around the expected value within which roughly half of our values of \mathbf{E}_1 lie. The intensity at some fixed point x can thus be considered to have changed significantly when the magnitude of the change in $\mathbf{E}_1(x)$ with wavelength is of the order of the standard deviation. Thus, we adopt the criterion that the speckle is decoupled when the wavelength change causes the average of the magnitude squared change in $\mathbf{E}_1(x)$ to be equal to the variance for a particular wavelength λ_0 , i.e., *decorrelation occurs whenever*

$$\langle \Delta \mathbf{E}_1(x) \Delta \mathbf{E}_1(x)^* \rangle \geq \sigma^2[\mathbf{E}_1(x)]. \quad (21)$$

The change in the electric field $\mathbf{E}_1(x)$ with wavelength interval $\Delta\lambda$ is given by

$$\Delta \mathbf{E}_1(x) = [\partial \mathbf{E}_1(x)/\partial \lambda] \Delta \lambda.$$

Thus differentiating Eq. (15) with respect to λ and noting that $dp/d\lambda = (+2\pi n_3/\lambda^2)$, we obtain

$$\Delta \mathbf{E}_1(x) = \left(-\Delta BN + B \sum_{r=1}^N ih_r e^{iph_r} \frac{2\pi n_3}{\lambda_0^2} + \Delta B \sum_{r=1}^N e^{iph_r} \right) \Delta \lambda, \quad (22)$$

where

$$\Delta B = i\pi n_0 x^2 M w_c / (\lambda_0^2 M^2 s') \exp[i\pi n_0 x^2 / (\lambda_0 M^2 s')].$$

We now consider the speckle near the axis, i.e., when ΔB is negligible (worst case). In this case Eq. (22) reduces to

$$\Delta \mathbf{E}_1(x) \simeq B \sum_{r=1}^N ih_r \frac{2\pi n_3}{\lambda_0^2} e^{iph_r} \Delta \lambda. \quad (23)$$

If we now compute $\langle \mathbf{E}_1(x) \Delta \mathbf{E}_1(x)^* \rangle$, we obtain the following result, assuming that the expected value of h_r is zero and that the standard deviation is h_0 ,

$$\langle \Delta \mathbf{E}_1(x) \Delta \mathbf{E}_1(x)^* \rangle = (2\pi n_3 \Delta \lambda / \lambda_0^2)^2 \{ h_0^2 N + (N^2 - N)[(d/dp)F(p)][(d/dp)F(p)]^* \} BB^*. \quad (24)$$

Substituting Eqs. (20) and (24) into the criterion, Eq. (21), we obtain a value for the wavelength spacing $\lambda_2 - \lambda_1$ required to decorrelate the speckle:

$$\lambda_2 - \lambda_1 = \frac{\lambda_0^2}{2\pi n_3} \left\{ \frac{1 - F(p)F^*(p)}{h_0^2 + (N - 1)[(d/dp)F(p)][(d/dp)F(p)]^*} \right\}^{1/2} \quad [decoupled \text{ case}]. \quad (25)$$

The speckle pattern will therefore be laserlike when the spectral line width of a single tone is much less than is given by Eq. (25), i.e., when the line width $\Delta\lambda$ is given by

$$\Delta\lambda \leq \frac{1}{10} (\lambda_2 - \lambda_1) \leq \frac{\lambda_0^2}{20\pi n_3} \left\{ \frac{1 - F(p)F^*(p)}{h_0^2 + (N-1)[(d/dp)F(p)][(d/dp)F(p)]^*} \right\}^{1/2} \quad [\text{laserlike case}]. \quad (26)$$

To illustrate the above results with an example, assume that the heights of the scatterers are distributed normally, where our expected value and standard deviation for the heights have already been taken to be zero and h_0 , respectively. Thus, we write the density function for h_r as

$$f(h_r) = \exp[-h_r^2/(2h_0^2)]/h_0(2\pi)^{1/2} \quad (27a)$$

and the corresponding characteristic function as

$$F(p) = \exp(-\frac{1}{2}p^2h_0^2). \quad (27b)$$

Substituting Eq. (27) into Eq. (25) we obtain the wavelength spacing required to decorrelate the speckle pattern as

$$\lambda_2 - \lambda_1 = \frac{\lambda_0^2}{2\pi n_3 h_0} \left[\frac{1 - e^{-p^2 h_0^2}}{1 + (N-1)(h_0 p)^2 e^{-p^2 h_0^2}} \right]^{1/2}. \quad (28)$$

We note that for the case of a very rough diffuser, where (ph_0) is greater than 1, Eq. (28) can be approximated by

$$\lambda_2 - \lambda_1 = \lambda_0^2 / (2\pi n_3 h_0), \quad \text{when } (ph_0)^2 \gg 1. \quad (29)$$

In the case of a relatively smooth diffuser, Eq. (28) can be reduced to

$$\lambda_2 - \lambda_1 = \frac{\lambda_0}{[1 + (N-1)(ph_0)^2]^{1/2}}, \quad \text{when } (ph_0)^2 \ll 1. \quad (30)$$

Now assuming monochromatic illumination, we study the condition under which we can expect a particular diffuser to give a large amount of speckle. If we take the ratio of the standard deviation to the amplitude of the expected value, i.e., by Eqs. (19) and (20), we obtain the average fractional change in amplitude among different resolution cells of width $2\Delta w$. When this ratio is very small, we have the case when most cells have the same intensity; and there is practically no speckle. In the case where this ratio approaches 1, we have a badly speckled case. Thus, for the normal distribution, as defined by Eq. (27), this ratio is given by

$$R = \frac{(N)^{1/2}(1 - e^{-p^2 h_0^2})^{1/2} |B|}{|A - NB + NB e^{-p^2 h_0^2/2}|}. \quad (31)$$

By Eq. (31), we note that R goes to zero, i.e., no speckle, when the roughness as characterized by ph_0 decreases. Alternatively, taking A to be of the same order of magnitude as NB , we note that the ratio R is proportional to $1/(N)^{1/2}$. Thus, the badly speckled case occurs with small numbers of scatterers per

resolution element. And as N gets very large, say exceeding 100, the amount of speckle is drastically reduced.

If we assume operation at a single wavelength, it is still possible to obtain averaging of speckle by superimposing image intensities formed when the diffuser is illuminated successively by plane waves at different angles of incidence. We can calculate the angular difference $\Delta\theta_0$ between successive plane waves incident at angles θ_{01} and θ_{02} , which will decouple these respective image intensities. Since we are considering the sequential recording of intensities, the phase term containing θ_0 , which was suppressed in writing Eq. (14), still does not enter: and Eqs. (15) and (16) form a convenient starting point. From $n_3 = (n_1/\cos\theta_1 - n_0/\cos\theta_0)$ and $n_1 \sin\theta_1 = n_0 \sin\theta_0$, we compute the angular variation of n_3 :

$$\frac{dn_3}{d\theta_0} = (1/2)(n_0^2/n_1)(\sin 2\theta_0/\cos^3\theta_1) - (n_0 \sin\theta_0/\cos^2\theta_0). \quad (32)$$

The variation of p , at fixed wavelength, is found by differentiation of Eq. (16), i.e.,

$$dp/d\theta_0 = (-2\pi/\lambda_0)(dn_3/d\theta_0). \quad (33)$$

Following the same mathematical procedure as we did in deriving Eq. (25) except that now $\Delta E_1(x) = [\partial E_1(x)/\partial\theta_0]\Delta\theta_0$, one can readily show that the angular spacing $\Delta\theta_0 = \theta_{02} - \theta_{01}$ is given by

$$\Delta\theta_0 = \left(\lambda_0 \left\{ \frac{1 - F(p)F^*(p)}{h_0^2 + (N-1)[(d/dp)F(p)][(d/dp)F(p)]^*} \right\}^{1/2} \right)' / \left\{ \pi n_0 [2\sin\theta_0/\cos^2\theta_0 - n_0 \sin 2\theta_0/(n_1 \cos^3\theta_1)] \right\}. \quad (34)$$

For the case when the heights are distributed normally, by substitution of Eq. (27) into (34), we find the angular separation required to decouple the speckle patterns reduces to

$$\Delta\theta_0 = (\lambda_0 \{ (1 - e^{-p^2 h_0^2}) / [1 + (N-1)(h_0 p)^2 e^{-p^2 h_0^2}] \}^{1/2}) / \left[\pi n_0 h_0 \left(\frac{2\sin\theta_0}{\cos^2\theta_0} - \frac{n_0 \sin 2\theta_0}{n_1 \cos^3\theta_1} \right) \right]. \quad (35)$$

We will use Eq. (35) in the following section to establish a numerical value for the degree of collimation required to assure that our speckle averaging is due to wavelength variation and not to multiangular illuminating beams.

Experiments with Laser Sources

Three different experiments were conducted using a laser. In the first, a single mode argon laser was used to illuminate a ground glass diffuser and the speckle positions were charted as the wavelength was set to the various principal lines (4579 Å, 4727 Å, 4765 Å, 4880 Å, 4965 Å, 5017 Å, and 5145 Å). In this experiment, the statistical problem is different in the details from the analysis presented herein

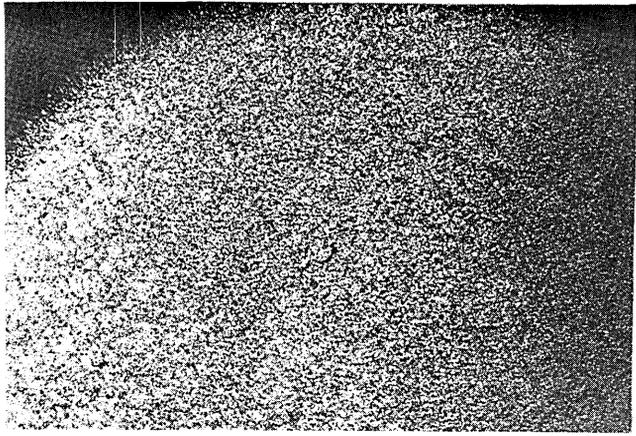


Fig. 4. Speckle pattern with collimated laser illumination at 6328 Å incident on diffuser made from Scotch Magic Tape. Imaging is as shown in Fig. 3.

source (A) is collimated, dispersed by the grating (G) for band limiting by pinholes P_2, P_3 ; then it is highly collimated by the pinhole-objective lens combination (P_3, O_1 in Fig. 3). The objects are placed at D for magnification by the microscope, O_M , and photographically recorded by the camera (C).

Since the principal objective of this experiment is a detailed study of the averaging of speckle from a multitone source, first we must establish values for the allowable width of the single tone; then, we will take a series of exposures with wavelength differences exceeding the interval given by Eq. (28). The quantitative treatment of the degree of smoothing that results from a number of independent tones is beyond the scope of this paper.²¹

For experimental purposes in the classification of diffusers, it is convenient to recognize that $[\Delta w_0 / \langle w_r \rangle]^2$ sets an upper limit to the number of samples per resolution cell and that h_0 and $\langle w_r \rangle$, are coupled, i.e., by coupled, we mean that in making a finer diffuser, $\langle w_r \rangle$ becomes less, but the attainable h_0 usually decreases too. Hence, we rewrite Eq. (28) as follows:

$$\frac{\Delta \lambda}{\lambda} = \frac{\lambda}{2\pi n_3 h_0} \left(\{1 - \exp[-(2\pi n_3 h_0 / \lambda)^2]\} / \{1 + [(\Delta w_0 / \langle w_r \rangle) - 1] [h_0 (2\pi n_3 / \lambda)]^2 \exp[-(2\pi n_3 h_0 / \lambda)^2]\} \right), \quad (36)$$

where $\Delta w_0 = 2\lambda F / (\pi D)$.

The Scotch Magic Tape diffuser is relatively rough; separate measurements using a depth microscope fix the depth $h_0 \gtrsim 8 \mu\text{m}$, although it could be as high as $14 \mu\text{m}$ and the width $\langle w_r \rangle \approx 1 \mu\text{m}$. For $n_3 = 0.6$ and $\lambda_0 = 0.5 \mu\text{m}$, we find $ph_0 = 50$, hence by Eq. (29) we predict that

$$\lambda_2 - \lambda_1 = 80 \text{ \AA} \quad (37)$$

decouples, and the speckle should remain laser-like for line widths up to about one tenth of this, i.e., for

8 Å. We note that N does not enter into this computation, since $ph_0 \gg 1$.

For the spectrometer used, the output line width from P_3 in Fig. 3 is just slightly under 5 Å for the input pinhole (P_2) of $400 \mu\text{m}$ and the exit pinhole (P_3) of $60 \mu\text{m}$. In the customary language of partial coherence,²⁹ an equivalent viewpoint on the need to restrict $\Delta\lambda$, as by Eq. (26), is that we must restrict the temporal coherence so that axial path differences inherent in traversing the diffuser will not smooth out the laserlike speckle. Thus, we have $n_3 h_0 \ll c / \Delta\nu$; hence, we see that $n_3 h_0 \Delta\lambda / \lambda^2 \ll 1$, which is precisely the expression used to compute the 8-Å limit in the preceding paragraph.

P_2 essentially controls $\Delta\lambda$ in the apparatus; and in a relatively independent manner, the much smaller P_3 controls the transverse coherence. This is the reason for the disparity in our choices of their sizes. This, too, can be understood directly from Eq. (13). A larger pinhole P_3 permits a continuous range of angle θ_0 from zero up to some maximum θ_{02} in the illumination of the sample.

From Eq. (35) and the discussion of the previous section, we obtain the maximum angular bandwidth allowable for laserlike speckle to be

$$\Delta\theta = \frac{1}{10} \left\{ \frac{\lambda \cos^2 \theta_0}{\pi h_0 [n_0 - (n_0^2 / n_1)]} \right\}^{1/2},$$

in the case of rough diffuser, i.e., $ph_0 \gg 1$, where θ_0 is the mean incident angle. For the Scotch Magic Tape diffuser, this value is 0.02 rad. A simple geometrical consideration gives the illumination on the diffuser (D) in Fig. 3 to have an angular bandwidth of 1.9×10^{-3} rad, and so we are well within the limit to see speckle. (Parenthetically, we note that when the diffuser is very rough, the occurrence of speckle is reasonably estimated using a simple temporal coherence requirement and the usual transverse coherence requirement, which results from the van Cittert-Zernike theorem. However, in the intermediate

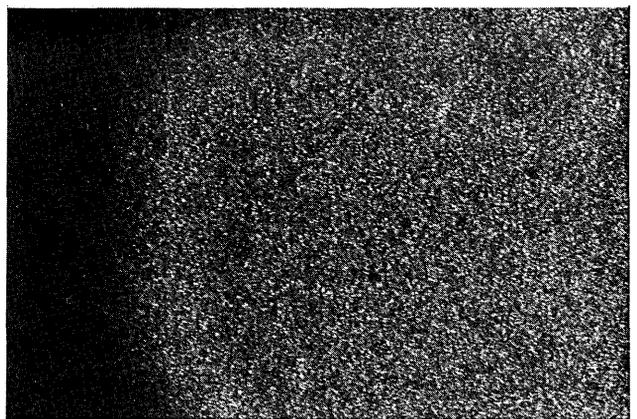


Fig. 5. Speckle pattern for Scotch Magic tape diffuser, as in Fig. 4, but illuminated with band-limited light from a carbon arc (5 Å band limited at 6000 Å and 70 min of exposure using Tri-X film). Beam collimation angle is 2×10^{-3} rad.

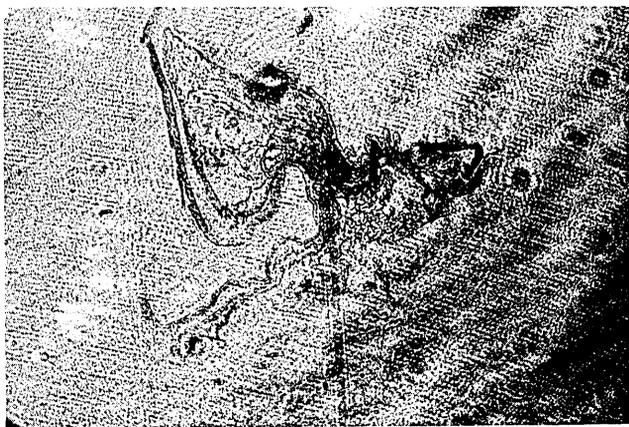


Fig. 6. Section of optic nerve at low magnification illuminated by collimated laser light.

range, $ph_0 \sim 1$, the statistical properties control, and the formulas of the last section should be used.)

Band limiting the source to a 5 Å width and maintaining adequate transverse coherence greatly reduces the illumination level at the camera. A value for the exposure time is estimated in the following discussion. Referring to Fig. 3, and noting that the energy radiated by the source A (carbon arc lamp) is $10^{-2} \text{ W sr}^{-1} \text{ Å}^{-1}$ and that the f numbers of the lenses L_1 and L_2 and mirrors M_1 and M_2 have been matched, we obtain the energy transmitted through the pinhole P_3 to be $3 \times 10^{-6} \text{ W}$ in a 5-Å bandwidth. The intensity at the diffuser is approximately $2 \times 10^{-5} \text{ W/cm}^2$. The magnification of the objective and camera system (O_M and C) is 20 and so the intensity of the light hitting the film is $4 \times 10^{-8} \text{ W/cm}^2$. Now the film requires, including the reciprocity loss factor, $50 \mu\text{J/cm}^2$ of energy to be at threshold for recording, and so this gives a minimum exposure time of 20 min.

The speckle pattern using a collimated 6328-Å laser to illuminate the Magic Tape diffuser D in Fig. 3 is shown in Fig. 4. The laserlike speckle pattern using the high pressure arc source is shown in Fig. 5. Even so, some averaging of the speckle pattern is evident with the highly collimated arc source band limited to 5 Å. While a narrower line width would have been desirable, the extremely long exposure times, 70 min for one tone, forced this compromise. With the arc source illumination, the speckle is also easily seen visually through the microscope eyepiece (after 15 min of dark adaptation). A precise motorized scan (Spex monochromator) of the grating G also permits one to observe the speckle variations with wavelength. Visual observation during motorized scanning at 2 Å/sec was used in order to establish that the characteristic decorrelation is in the range from 30 Å to 100 Å for the diffusers used. The corroboration with the computed value of 80 Å in Eq. (37) is excellent.

A separate series of exposures to show the averaging effect of multicolor speckle is presented in Figs. 6 through 9. Its an $8\text{-}\mu\text{m}$ thick section from the optic

nerve of a crayfish, prepared and stained by Roach.³⁰ All exposures have the same magnification, and the major characteristic length of the nerve is 1 mm. First, we should compare the appearance of this optic nerve when illuminated in laser light (no diffuser is used in this case, since it would cause speckle) and in white light as is shown in Figs. 6 and 7, respectively. It is to be emphasized that this type of comparison is essential to an understanding of the speckle problem, since the degree of difficulty in seeing things that are illuminated by a laser is highly dependent on their roughness; and of course with biological specimens, a great range of roughness is experienced. For example, from this comparison we conclude that the sample shown is not unusually diffuse, hence its visibility with laser illumination, while low, is by no means representative of a badly speckled case.

Now, a single exposure of 180-min duration for one wavelength of our 5-Å band-limited source is shown in Fig. 8. A multiple exposure with six separate wavelengths each spaced by 300 Å is shown in Fig. 9. Great care is taken to minimize the relative motion as the grating is scanned to each new wavelength. An exposure duration of 50 min is used at each wavelength, the longer total exposure time being a characteristic aspect of the averaging process. A comparison of Figs. 6 and 8 shows the slight smoothing of the laser speckle caused by the finite (5-Å) width of the band-limited carbon arc source. Comparing Figs. 8 and 9 dramatically shows the improved resolution that results from using six tones of the multicolor illumination. In the holographic application, Fig. 6 shows the representative speckle for one-wavelength recording, and Fig. 9 is approximately the improvement that one would expect using six tones spanning 1500 Å.

Conclusions

A theoretical study of the wavelength dependence of speckle that has been so troublesome in holo-

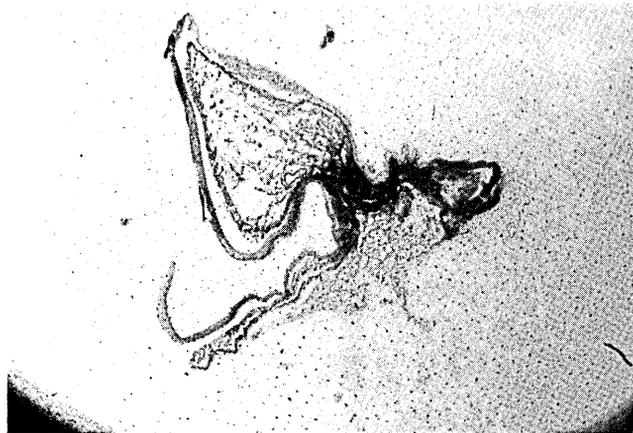


Fig. 7. Optic nerve illuminated in white light. Resolution here is much better than in the speckled image of Fig. 6. The maximum length of this specimen is approximately 1 mm (actual length).

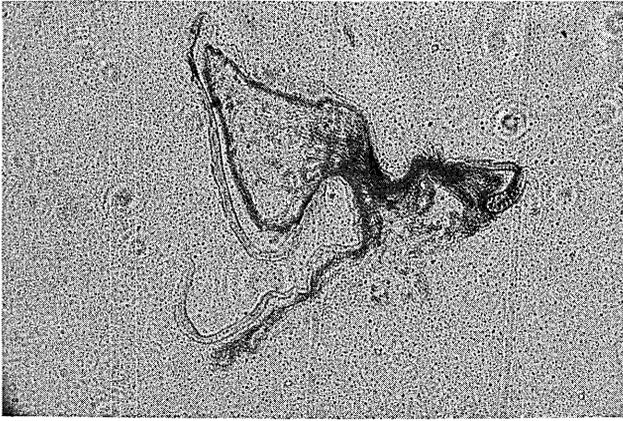


Fig. 8. Optic nerve illuminated by a collimated source at 5500 Å with 5-Å line width (180-min exposure using a high pressure mercury arc and Tri-X film). Note that the image is speckled to a slightly lesser degree than with laser illumination.

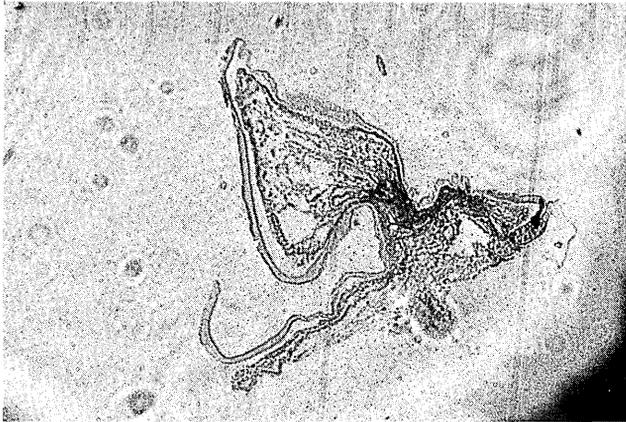


Fig. 9. Optic nerve illuminated by six separate band-limited wavelengths, spanning the spectrum from 4300 Å to 5800 Å. Note that the resolution is considerably improved over that for a single tone as shown in Fig. 8. The beam collimation angle of 2×10^{-3} rad is maintained throughout the series.

graphic microscopy is used to establish general criteria for the wavelength interval required in order to decouple speckle in an imaging system. A simple statistical argument is presented in analysis of Eq. (12) for the imaging of a diffuser with variable roughness; expressions for $\Delta\lambda$ to decouple with speckle or to keep it laserlike are given by Eq. (25) and (26), respectively. These are specialized for a Gaussian distribution of heights in the diffuser in Eq. (28) and then applied and discussed in an experimental context in Eq. (36).

Experiments are described that verify that decorrelation results as the wavelength is scanned. In approximate terms, for highly collimated illumination, speckle is laserlike for $\Delta\lambda \leq 8$ Å and is greatly smoothed for $\Delta\lambda \geq 80$ Å. Perhaps the most significant implication of this study is that it demonstrates the feasibility of eliminating speckle in holographic microscopy while still requiring only a single rapid exposure from some multimono-chromatic-toned source, e.g., a dye laser.

We acknowledge that J. H. Wayland's and R. J. Bing's interest in making holograms of microcirculatory blood vessels first stimulated our interest in speckle-free holographic microscopy; also we are pleased to acknowledge helpful discussions with D. MacQuigg and R. B. MacAnally as well as the enthusiastic participation of Francois Bertiere in the first series of experiments with the laser sources.

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26. As we have employed it here, the Gaussian transmission function in Eq. (2) is chosen for theoretical convenience, although for electronic optics it is physically appropriate as well. In the results it will not make any qualitative difference; in fact, in deriving the form in Eq. (15) we further approximate the actual case using a simple rect function as the impulse response of the lens.
27. In this simplification, the assumption is that the phase terms in the integrand of Eq. (3) involving the variables x' , y' do not vary appreciably within the interval w_r . For a consideration of the extent of this type of phase variation, the reader is referred to D. A. Tichenor and J. W. Goodman, *J. Opt. Soc. Am.* **62**, 293 (1972).
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30. The 8- μ m section of the optic nerve is prepared by perfusing the eyestalk in 1% $K_4Fe(CN)_6$ in crayfish saline; it is removed from the crayfish, soaked in saline saturated with picric acid, dehydrated in alcohol, embedded in paraffin, sectioned with a rotary microtome, stained in a Ponceau acid fushin solution, and mounted with Permount on glass.

SYMPOSIUM ON MAN-MACHINE COMMUNICATION FOR SCIENTIFIC DATA HANDLING

The Task Group on Computer Use of the ICSU Committee on Data for Science and Technology (CODATA) will hold a symposium at the University of Freiburg, Freiburg-im-Breisgau, Germany, from July 22nd to 27th, 1973.

The purpose of the symposium is to bring together specialists concerned with the application of computer technology to the compilation, storage, and utilization of quantitative scientific data in the physical, biological, geological, and engineering sciences.

The symposium will be patterned on the Gordon Research Conferences, centering around a series of invited lectures with opportunities provided for small groups to deal collectively with areas of specialized interests in working seminars.

Attendance will be by invitation; interested organizations and individuals are requested to write without delay to the Secretary of the Task Group, c/o Mr. A. K. Ward, International Conferences Office, National Research Council of Canada, Ottawa K1A 0R6, Canada, including a brief statement of their areas of special interest.