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Tests of CMS hadron forward calorimeter upgrade readout box prototype

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ABSTRACT: A readout box prototype for the CMS Hadron Forward calorimeter upgrade was built and tested in the CERN H2 beamline. The prototype was designed to enable simultaneous tests of different readout options for the four anode upgrade PMTs, new front-end electronics design and new cabling. The response of the PMTs with different readout options was uniform and the background response was minimal. Multi-channel readout options further enhanced the background elimination. Passing all the electronic, mechanical and physics tests, the readout box proved to be capable of providing the forward hadron calorimeter operational requirements in the upgrade era.

KEYWORDS: Cherenkov detectors; Photon detectors for UV, visible and IR photons (vacuum); Calorimeters; Cherenkov and transition radiation
1 Introduction

The Compact Muon Solenoid (CMS) [1] is a general-purpose detector designed to run at the highest luminosity provided by the CERN Large Hadron Collider (LHC). Coverage between pseudorapidities ($\eta$) of 3.0 and 5.0 is provided by the steel/quartz fiber Hadron Forward (HF) calorimeter. The front face is located at 11.2 m from the interaction point and the depth of the absorber is 1.65 m. The signal originates from Čerenkov light emitted in the quartz fibers, which is then channeled by the fibers to photomultipliers. The absorber structure is created by machining 1 mm square grooves into steel plates, which are then diffusion welded. The diameter of the quartz fibers is 0.6 mm and they are placed 5 mm apart in a square grid. The quartz fibers, which run parallel to the beamline, have two different lengths (1.43 m and 1.65 m) which are inserted into grooves, creating two effective longitudinal samplings. The so-called “short fibers” start 22 cm inside the absorber, hence are mostly sensitive to hadron interactions. There are 13 towers in $\eta$, all with a size given by $\Delta \eta \approx 0.175$, except for the lowest-$\eta$ tower with $\Delta \eta \approx 0.1$ and the highest-$\eta$ tower with $\Delta \eta \approx 0.3$. The $\phi$ segmentation of all towers is $10^\circ$, except for the highest-$\eta$ which has $\Delta \phi = 20^\circ$. This leads to 900 towers and 1800 channels in the two HF calorimeter modules [2]. Details of the HF calorimeter design, together with test beam results and calibration methods, can be found in [3].
The photomultiplier tubes (PMTs) of the CMS HF calorimeter generate a large, fake signal when the PMT window is traversed by a relativistic charged particle due to Čerenkov light production at the PMT window. These PMTs have circular windows with 2.54 cm diameter and 2 mm thickness at the center that gets thicker towards the rim (Hamamatsu R7525 [4]). This already-known problem was observed in the 2010 and 2011 CMS data to degrade data quality and to constitute a potential to interfere with rare physics events. In the framework of the CMS HF upgrade program, several types of PMTs were tested and the four-anode R7600U-200-M4 by Hamamatsu [4], was selected as the replacement PMT for the upgrade [5]. The upgrade PMT has a square window of size 1.8 cm × 1.8 cm and thickness less than 1 mm indicating a significant reduction in the amount of glass seen by the traversing relativistic particles. The new PMT not only reduces the intrinsic level of background, but it also enables tagging of background events and recovering the underlying signal event (if any) by using the multi-anode features.

A readout box (RBX) prototype was built to enable the tests of different readout options for the new four anode PMTs. The new readout boards provide the flexibility to switch between four-channel, two-channel and single-channel readout of the four anode PMTs where the four-channel readout option enables the full multi-anode functionality. Both the internal and external cabling of the RBX were also specific designs and selections, therefore form an integral part of the prototype.

The prototype RBX was tested in the CERN H2 beamline [6] in Summer–Fall 2011 with electron and muon beams to mimic calorimeter and background responses respectively. Here we describe the details of certain performance tests of the RBX and report on the compatibility of the new RBX with the CMS HF upgrade framework.

2 Prototype RBX design

The RBX houses three front-end electronics boards and each board can read out 8 PMTs. The prototype RBX was built with 11 four anode PMTs (R7600U-200-M4) in two front-end electronics boards. The boards can provide different readout options with the help of internal cabling and jumper settings. This is primarily obtained with a two-board approach: A main base board where the PMTs are connected, and an adapter board where the signals from different anodes are combined to produce the desired readout option. Figure 1a shows a picture depicting the base and adapter boards as well as the internal cabling.

The readout board assembly consists of 3 major components: Base board with high voltage (HV) divider, power and safety ground connectors; PMT sockets with local dynode bypassing (installed on base boards) and adapter boards for forming any desired readout scheme (out of 4 available anodes). Figure 1b shows the readout board components.

The base board features a voltage divider design per Hamamatsu specifications [4] with a total divider resistance of 2.75 MΩ. The maximum PMT operating voltage is 900 V (330 µA for 8 PMTs). It houses bypass capacitors between all dynodes (10 nF × 200 V) and a voltage divider ground connects to the RBX safety ground. For better high signal rate performance, the two last dynodes have boost power supply inputs: 8% and 16% of operational HV.

A virtual ground is implemented on the base board to reduce PMT-to-PMT cross-talk and ground loop interference. All 4 anodes of each PMT and their reference signals are routed to a signal header. Anode and reference circuits have bleeder resisters for HV charging prevention.
Figure 1. (a) Picture depicting the prototype RBX anatomy. The PMTs appear inverted on the table. The base boards, adapter boards and internal cabling are also visible. The entire RBX can read out 24 PMTs in three front-end electronics boards where only 11 PMTs in two boards were read out during the beam tests. (b) Picture of the base (bottom) and adapter (top) boards before assembly. Major parts of the boards are labeled.

Figure 2. Schematics depicting the PMT socket, output signals and virtual ground.

Reference signals are equalized for the capacitance of the PMT anode, socket, and base board artwork (additional 9 pF).

The PMT socket is implemented as a sub-assembly, made of high quality gold-plated individual sockets, press-fit into a printed circuit board (PCB) with a PMT key-hole. Each PMT socket has a full set of bypass capacitors between dynodes. The last 3 dynodes have series damping resistors (50Ω, 50Ω and 4.7Ω). Figure 2 shows the schematics of the PMT socket, output signals and virtual ground.

In order to comply with the different phases of the upgrade program, the adapter board is designed to provide convenient switching between different readout options. The adapter board uses through hole mounted MMCX (micro miniature coaxial) signal connectors. There are screw/standoff retainers for attachment to the base board.

In the overall design of the readout boards, shortest possible connections for critical nets are used to lower series inductance. No conductors that belong to different grounds overlap. This decreases AC coupling between the grounds. The ground planes are on internal layers (i.e. against surface discharges).
Figure 3. The sketch of the PMTs in the RBX as seen by the beam. The labels indicate the PMT names used in this text. The color code shows single-channel (black), two-channel (blue) and four-channel (red) readout options.

<table>
<thead>
<tr>
<th>PMT</th>
<th>8B</th>
<th>6B</th>
<th>4B</th>
<th>2B</th>
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<tr>
<td></td>
<td>X</td>
<td>5B</td>
<td>3B</td>
<td>1B</td>
</tr>
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<td></td>
<td>X</td>
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<td>4C</td>
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<tr>
<td></td>
<td>X</td>
<td>5C</td>
<td>3C</td>
<td>X</td>
</tr>
</tbody>
</table>

Figure 4. The sketch of the test setups for the calorimeter signal (top) and muon background (bottom) measurements.

3 Experimental setup and data acquisition

The position of the PMTs in the RBX together with their labels used throughout this text is shown in figure 3. 5B, 6B, 8B, 5C and 6C are single-channel (black); 3B, 4B, 3C and 4C are two-channel (blue); 1B and 2B are four-channel (red) readout PMTs.

The RBX was tested with 80 GeV electron and 150 GeV muon beams in the CERN H2 beamline [6] during Summer-Fall 2011 (energy and momenta units are used interchangeably to describe the beam throughout the text). Figure 4 shows the two setups used for measuring the calorimetric performance and the background response of the RBX.

The 80 GeV electron beam was used to generate Čerenkov light through a fiber bundle. The fibers of the bundle were identical to those used in the HF calorimeter. The electromagnetic shower was initiated with approximately 10 cm (6 $X_0$) of iron absorber. The bundle-shower crossing was downstream of the absorber at a 45° angle, i.e. the bundle was at 45° with respect to the beamline. The bundle was divided into two sections at the readout end which were inserted into the air light guides of the RBX. Therefore two PMTs could be read out simultaneously. The operating voltage for the RBX PMTs was 600 V in order to reproduce the real operating conditions, i.e. gains comparable to the currently installed PMTs of HF calorimeter.

The quartz fiber calorimeter that was built for the 2009 beam tests was used as a tail catcher to tag pions in the electron beam. The calorimeter consisted of 20 cm × 20 cm array of 6 mm diameter, 45 cm long steel rods, and quartz fibers with properties similar to those used in HF calorimeter between the rods. The fibers were bundled at the downstream end and read out with a four-anode PMT in the four-channel mode.
The 150 GeV muon beam was used to generate background events on the PMT windows. For this purpose, the light guides were removed and the RBX was placed directly in front of a wire chamber in order to perform precise position measurements. The wire chamber was ∼20 cm upstream of the test setup and had a 1 mm resolution.

The readout was performed by charge integration and encoding units (QIEs) [7] and the data were stored in CMSSW (CMS SoftWare) data format. Each QIE channel was read out in 10 time slices of 25 ns each. The trigger was given by the coincidence of two scintillation counters of sizes 14 cm × 14 cm and 4 cm × 4 cm. Therefore, a beam spot of size 4 cm × 4 cm was anticipated. Another scintillation counter of size 14 cm × 14 cm was used to veto multiple particles. All counters were within 5 m upstream of the test setup.

For all the electron triggers, the tail catcher quartz fiber calorimeter was utilized to tag pions. Pion contamination in the electron beam was measured to be less than 1% and the pion events were not included in the analysis.

4 Fiber bundle characteristics

The fiber bundle was tested for signal uniformity by reading out the two ends with the same PMT in two separate electron datasets. Figure 5 shows the integrated charge profile as a function of the wire chamber coordinates for PMT 6B when it was reading out the two ends of the fiber bundle labeled A and B. The rectangles show the selection regions for the bundle location. As can be seen in the charge profiles, there are two distinct sections at the interaction end of the bundle i.e. the selection regions for the bundle locations indicate different locations in the profiles.

Figure 6 shows the distribution of the number of photoelectrons for PMT 6B when it was reading A (red) and B (black) ends of the bundle with the selections in figure 5 applied accordingly. The response of the fiber bundle is equivalent in the two readout ends. Therefore, a correction for the differences in the two readout ends is not necessary.
Measurement of multi-channel readout signal variations

The PMTs with two-channel (3B, 4B, 3C and 4C) and four-channel (1B and 2B) readout options show channel-to-channel signal variations due to various factors. These include the intrinsic gain variations between anodes, variations in the PMT alignment in the RBX, coupling of the fiber bundle to the light guide and the variations in the light guide conditions. The overall signal for these multi-channel readout PMTs is calculated as $S = \sum c_i s_i$ where $s_i (c_i)$ is the signal (correction factor) for each channel. The correction factors are the mean ratios between the signals of the multiple channels. Therefore the mean responses of different channels are normalized to a particular one which is chosen arbitrarily.

Figure 7 shows the ratio of the signal in one of the quadrants to the signal in the other quadrants for the two four-channel readout PMTs - 1B and 2B. Variations between 10–30% are observed.

Figure 8 shows the ratio of the signal in one half to the signal in the other half for the four two-channel readout PMTs - 3B, 4B, 3C and 4C. The anode signals are combined using a nearest neighbor approach to produce the two readout channels (see section 9 for a discussion). Variations up to 15% are observed.

Global calibration of the RBX

Once the individual PMT calibrations are performed, a global calibration for the entire RBX is necessary since the two-channel readout PMTs have a less effective correction for multi-channel readout signal variations than the four-channel readout PMTs and the single-channel readout PMTs have no correction. PMT 2B is chosen as the basis for this calibration. Figure 9 shows the signal from PMT 2B (a) and 6B (b) together with the Gaussian fits. The signal for a particular PMT is corrected by a factor obtained from the ratio of the Gaussian fit mean for this PMT signal to that of PMT 2B. These correction factors imply a 5–20% variation between PMTs (17% for the particular case in figure 9).
7 Response to Čerenkov light with the Fiber bundle

Figure 10 shows the response of PMTs 1B–6C (a-k) to Čerenkov light through the HF-like fiber bundle after calibration. The response over the entire RBX is uniform. A cut at 30 photoelectrons, which corresponds to about 7.5 GeV in terms of HF energy, is applied to exclude any possible muon contamination. Overall, the signal variation within the RBX is less than 0.5%.

8 Testing muon interactions with the RBX

Figure 11 a shows the integrated charge profile of the entire RBX for the muon data. PMT locations are clearly visible as light green squares. In order to investigate the response of the PMTs to traversing muons (called “window events” herein), tight selections around their windows are applied. The selection region for PMT 6B is shown in figure 11 a as a black square frame. Figure 11 b shows the response of the PMTs after the window selections are applied. The event rate has fallen by more than three orders of magnitude at the cut level of 30 photoelectrons which corresponds to ∼ 7.5 GeV in HF energy units. The fraction of events above this level is ∼ 5 × 10^{-4}.

9 Tests of recovery algorithms for background elimination

Several algorithms to tag the background events and recover the underlying real signal (if any) were developed since Summer 2009 to comply with the progression of the upgrade program. Although
Figure 8. Ratio of the signal in one half to the signal in the other half for two-channel readout PMTs 3B (a), 4B (b), 3C (c) and 4C (d).

Figure 9. Signal before global calibration of the RBX for PMT 2B (a) and 6B (b). 2B is a four-channel and 6B is a single-channel readout PMT.

All these algorithms are based on measuring the signal deviations between the multiple channels of the PMT, they have different systematics and efficiencies. Contrary to the real calorimeter signal, the background, either coincident with the calorimeter signal or not, will result in an excessive, measurable signal in one or more of the readout channels of the PMT, where the relativistic particle traverses the window.
Figure 10. Response of each PMT in the RBX after calibration.
Figure 11. (a) Integrated charge profile of the RBX for muons. (b) Response of the PMTs to muons traversing their windows. The fraction of events higher than 30 photoelectrons (∼ 7.5 GeV HF energy) is ∼ 5 × 10^{-4}.

Figure 12. The distribution of the maximum absolute deviation of the signal in any quadrant from the average for the four quadrants divided by the average.

The four-channel readout algorithm was presented in detail in [5]. The identification of the window events is performed by observing the maximum deviation of the signal in any quadrant from the average for the four quadrants. If this deviation is greater than the average quadrant signal, the event is tagged as a window event. Figure 12 shows the distribution of this deviation for both fiber signal (red) and muon incidence data (black). A cut at a maximum deviation of 1 unit results in ∼ 98 % efficiency for window event identification. The next steps in the algorithm consist of simple tests to identify whether the deviation is due to a single or multiple quadrant hit. The PMT signal is then recovered by weighting the sum of the signal(s) in the untagged channel(s). The unidentified 2–2.5 % of window events are due to muons traversing the window close to the center. In this case, the fake signal is distributed evenly over the four quadrants as in the case of a real calorimeter signal and there is no significant difference between the signals in the different quadrants. Although, this constitutes an inefficiency for the algorithm, the probability of such events is very low and the overall response of the PMT for this case is still much lower than for real calorimeter signals.
Table 1. The measures used for tagging window events in two-channel readout option. \( S_1 \) and \( S_2 \) are the signals of the two channels with \( S_1 > S_2 \), and \( \mu = (S_1 + S_2)/2 \).

<table>
<thead>
<tr>
<th>Label</th>
<th>Measure</th>
<th>Window event selection</th>
</tr>
</thead>
<tbody>
<tr>
<td>M1</td>
<td>( \frac{S_1}{S_2} )</td>
<td>( M1 &gt; 3 )</td>
</tr>
<tr>
<td>M2</td>
<td>( \frac{\sqrt{(S_1 - \mu)^2 + (S_2 - \mu)^2}}{S_1 + S_2} )</td>
<td>( M2 &gt; 0.3 )</td>
</tr>
<tr>
<td>M3</td>
<td>( \frac{S_1 - \mu}{S_1 + S_2} )</td>
<td>( M3 &gt; 0.25 )</td>
</tr>
<tr>
<td>M4</td>
<td>( \frac{S_1 - S_2}{S_1 + S_2} )</td>
<td>( M4 &gt; 0.4 )</td>
</tr>
</tbody>
</table>

Figure 13. The distribution of the four measures for two-channel readout in 2011 beam tests.

In case it is not possible to implement the four-channel readout option in the first phase of the upgrade, window event tagging and signal recovery algorithms for the two-channel case were studied in detail. There are technically two schemes to combine the signals of the four quadrants: Nearest-neighbor and cross-neighbor combination. It is obvious that the cross-neighbor combination increases the inefficiency of the tagging algorithms as the boundary between the two signal regions is maximized. Hence, the nearest neighbor combination is the viable choice.
Figure 14. The results of application of the 4-ch and 2-ch M4 algorithms to muon data of 2011 beam tests.

Figure 15. The results of application of the 4-ch and 2-ch M4 algorithms to the 2011 fiber bundle test beam data (a) and the differences caused by the algorithms (b).

The two-channel tagging algorithms are summarized in table 1. The measures have 5–8% inefficiency in tagging window events with the selections defined in table 1. The distributions of these measures for the fiber signal (red) and the window events (black) in 2011 test beam data are shown in figure 13. After tagging the window event, the signal is recovered as $2S_2$.

Figure 14 demonstrates the application of the four-channel algorithm and one of the two-channel algorithms (M4) to muon data. For responses larger than 30 photoelectrons, the two-channel algorithm is approximately a factor of two more inefficient than the four-channel algorithm as expected. In any case, the fraction of events larger than 30 photoelectrons remains below $2 \times 10^{-4}$.

Figure 15 shows the application of the same algorithms to the fiber bundle data of 2011 beam tests. Since the response is solely due to the Čerenkov light generated in the fiber bundle, the algorithms are expected to produce no difference in the distributions. Above the 30 photoelectron level, both algorithms result in a misidentification rate around $1 \times 10^{-5}$. 
10 Conclusions

Within the CMS HF upgrade framework, a prototype readout box, which consists of specific designs of readout boards and cabling, and the new four-anode upgrade PMTs, was built. The readout box was extensively tested in two beam test campaigns in Summer – Fall 2011 at the CERN H2 beamline.

The readout box offers different readout options (single-channel, two-channel and four-channel) for the four anode PMT in a single compact design. During the tests, 11 four-anode PMTs were used with 5 of them in single-channel, 4 of them in two-channel and 2 of them in four-channel readout mode.

The response of the PMTs to Čerenkov light that is generated by exposing an HF-like fiber bundle to an electron shower is uniform through the entire readout box less than 0.5 % variation.

The background response of the PMTs in the readout box is measured using muon beams. The fraction of events above the 30 photoelectron level, which corresponds to $\sim 7.5$ GeV of HF energy, is $\sim 5 \times 10^{-4}$. This already corresponds to approximately an order of magnitude improvement on the background rate when compared to the current HF conditions.

Several algorithms for window event tagging and signal recovery were developed for both the two-channel and four-channel readout cases. On the average, the four-channel algorithm is 98 % and the two-channel algorithms are 92 % efficient. The fraction of events above the 30 photoelectron level is $\sim 6 \times 10^{-8}$ after the application of the four-channel algorithm and $\sim 1 \times 10^{-7}$ after the application of the two-channel algorithms. All algorithms have negligible misidentification rates.

The overall performance of the readout box is robust and reliable. All electronic, mechanical and physics tests performed on the readout box during the beam test periods were successful. The readout box is capable of providing the HF operations in the upgrade era with the desired performance characteristics and the flexibility to extend the readout options.

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