Approximate 3D Body-Wave Synthetics for Tomographic Models

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Abstract We present a new method of generating analytical synthetics for tomographic-style models. These models are perturbations to a 1D layered model involving changes in block velocities producing 3D images. The procedure is broken into three steps: (1) construction of ray paths for the reference 1D layered model, (2) generation of perturbed paths and the construction of 2D synthetics in the plane containing the source and receiver, and (3) addition of out-of-plane contributions (2D) from virtual receivers weighted by diffraction operators. In step 1, the ray paths reflecting from the various interfaces are established with ray parameter ($p_o$) and travel time ($t_o$). Next, these values are corrected after adding the velocity perturbations where ray segments in faster blocks grow relative to slower blocks. This new set of ray parameters can be used to generate 2D Cagniard-deHoop synthetics or WKM synthetics. Contributions from virtual receivers at neighboring azimuths are added by convolving with diffraction operators that are defined by the source duration and travel time to the 3D structure. We suggest a particularly simple approximation based on four virtual receivers which produces synthetics in agreement with 3D numerical synthetics.

Introduction

The largest low-velocity structures in the lower mantle occur beneath southern Africa and the mid-Pacific. These low shear-wave velocity structures are correlated with hotspots (Williams et al., 1998), suggesting that the decrease in velocity is associated with an increase in temperature. The positive geoid anomaly and high topography over Africa (Hager et al., 1985), and the broad-scale Cenozoic uplift (Gurnis et al., 2000), are all consistent with warm, rising mantle beneath Africa. However, recent tomographic imaging of the whole mantle suggests that bulk sound velocity ($V_s$) and shear velocity ($V_p$) are negatively correlated within the African and Pacific anomalies (Masters et al., 2000), suggesting that the anomalies are chemical in origin, not thermal. The chemical hypothesis is supported by an inversion of normal modes (Ishii and Tromp, 1999), which indicates that the density of the lower mantle may increase within the two low $V_s$ anomalies. However, if high-density chemical anomalies are embedded within thermal upwellings, we would predict that there should be sharp jumps in seismic velocity, either radially or laterally as found in dynamic models (Tackley, 2000). Thus, the sharpness of structures becomes a key issue in distinguishing between temperatures versus chemistry as the proper explanation of these anomalous structures.

A particularly effective means of determining lower mantle structure is through the study of differential travel times between ($S-S_c$) and (SKS-S) (Ni and Helmberger, 2003a). Anomalous patterns in South African data required enhancing and sharpening of existing tomographic models to fit such data resulting in a ridge-like structure extending upward from the core-mantle-boundary (CMB) with a 3% drop in shear velocity (see Fig. 1). Note that the phase SKS is nearly parallel to the eastern boundary, which predicts about a 6-s decrease in travel times between 96° and 99° (Fig. 1e). This jump occurs in less than a degree (100 km) or 50 km at the CMB in many data profiles (Ni and Helmberger, 2003a). The SKS waveforms appear complex near this crossover, suggesting multipathing, which can be addressed with 2D WKM theory (Ni et al., 2002). We will briefly review this approach before introducing 3D effects in the next section, but first we will examine some observations sampling the ridge structure displayed in Figure 2b for paths along the wall, at right angles to the paths in Figure 1b.

Observations recorded by the South African Array of deep Fiji events are particularly interesting as reported by Wen (2001). The $S_{diff}$ paths from one of the events (Western Pacific, 971222 at a depth of 180 km) he used is displayed in Figure 2a. Note that some of the paths sample the northern dark-edge boundary. The waveform data are displayed in two formats, one in a conventional record section (Fig. 2b) and one as a “fan-shot” or as a function of azimuth. Normal observations should start at $t = 0$. When plotted against azimuth, we see a systematic delay of data at 230° (paths inside the structure) relative to paths near the edge, 246°. Wen (2001) modeled these waveforms very well by dividing
up the data into sectors (narrow windows of azimuth) with separate 2D models for each sector. Although some of these variations could well be 2D, as he modeled it, some of it must be multipathing in azimuth (3D effects) as demonstrated in this study.

**Brief Review of Ray Theory Methods**

One of the most useful methods for generating 1D synthetics is called the WKBJ method developed by Chapman (1976). Results produced by this method are compared with reflectivity synthetics in Chapman and Orcutt (1985), where the various methods of computing synthetics are discussed in detail. Similar results involving generalized ray solutions are given in Burdick and Orcutt (1979) since these solutions have been well developed. We will start with the latter method where the wave field can be approximated by

$$V(r,z,t) = \frac{d}{dt} \left[ D(t) \ast \phi(r,z,t) \right], \quad (1)$$

where $V$ is the displacement for a flattened earth with $r$ the horizontal coordinate, $z$ the depth (Gilbert and Helmberger, 1972; Helmberger, 1973), where

$$\phi(r,z,t) = \sqrt{\frac{2}{r}} \frac{1}{\pi} \left[ \frac{1}{t} \ast \psi(t) \right], \quad (2)$$

with

$$\psi = \text{Im} \sum_{i=1}^{n} SR_i(p) \frac{\sqrt{P}}{\eta_i} R(p) \Pi_i(p) \left( \frac{dp_i}{dt} \right), \quad (3)$$

and where $p =$ ray parameter and $SR_i(p)$ is the vertical radiation pattern; $\eta_i = (1/\beta_i^2 - p^2)^{1/2}$; $\beta_i =$ shear velocity (km/s); $R(p) =$ receiver function; and $D(t)$ is the far-field dislocation time history. The generalized rays are summed over $i$ with $\Pi_i(p)$ containing the product of transmission coefficients and the reflection coefficient at the reflected interface $(i)$. Equation (3) is essentially the line-source solution, whereas the convolution and distance correction of equation (2) transform it into a point-source solution. It is relatively easy to add shear dislocations to this formalism in the generation of synthetics (i.e., Helmberger, 1983).

The travel time associated with each ray has a simple form:

$$t_i = p_i r + \sum T h_k \eta_k \quad (4)$$
Figure 2. Panel (a) displays the ray paths encountering the 3D structure proposed by Ni et al. (2005). The light shading indicates the bottom D' structure and the dark shading indicates the uppermost structure, extending upward, 1200 km above the CMB. The entire structure has a uniform 3% drop in shear velocity relative to PREM. The structure outside is Grand’s tomographic model. Panels (b) and (c) display the S_d observations recorded by the array. Panel (b) displays observations recorded at the South African Array plotted in a record section, relative to PREM travel-time predictions. A plot of these data as a function of azimuth (c) reveals a strong case for azimuthal multipathing.

where the summation is over the layers (thickness, \(T_{hi}\)) along the ray paths. The derivative \(\left(\frac{dt_i}{dp_i} = 0\right)\) at the stationary points where the rays satisfy Fermat’s principle and obey Snell’s law. This \(p\) is labeled \(p_0\) and the corresponding time \((t_0)\).

An example of such paths is displayed in Figure 1a where the phase SKS for the reference 1D model PREM is presented. The factor \(dp_i/dt_i\) is the complex derivative of the ray parameter against time along the Cagniard-deHoop contours.

However, for simple core velocities, this method can be greatly simplified by examining

\[
\frac{\delta(p_{oi} - p_{oi-1})}{\delta(t_{oi} - t_{oi-1})} = \left(\frac{\delta p_i}{\delta t_i}\right) \quad (5)
\]

for various \(i\)’s which has a square-root singularity at layer \(i\) nearest the geometric ray stationary point (Chapman, 1976). The \((p-t)\) curves in Figure 1c and d (PREM) display this feature as a function of epicentral distances, and allow equation (4) to be approximated by

\[
\Psi = SR_i(p)R(p)\left(\frac{\delta p}{\delta t}\right)(T_{SP} \cdot T_{PS}) \quad (6)
\]

where the first-order transmission coefficients for the CMB are retained. If one allows the velocities in equation (4) to vary (tomographic approximation), the \(p-t\) curves do not change appreciably. However, if one allows the ray parameter to be adjusted to obey Snell’s law (Fig. 1b), the paths will flatten for segments with fast velocities and produce sharp features in the \((p-t)\) curves as for model LVZ3 displayed in Figure 1c and d (see Ni et al., 2000). Thus, we obtain two pulses with the most favorable geometry with the fast path producing the first pulse and the second pulse following the slow path. If we add a transition zone (second column) along the boundary, we no longer produce multipathing because of the smoothness of the \((p-t)\) curves (Ni et al., 2002). These features can also be seen in 2D numerical
synthetics generated for tomographic models (Ni et al., 2003a, 2003b). Note that the $y$ function is nearly the line-source solution except for the inclusion of the $(\tilde{p})$ factor. This feature is exploited in developing 2D numerical simulation of earthquake (dislocation) sources (Helmberger and Vidale, 1988; Wen and Helmberger, 1998). To produce a point-source solution, we simply perform the operations in equation (2) which involves a convolution with $1/\tilde{t}$. This operation creates a step-function-like response and is appropriate for models containing azimuthal uniformity. If the ray paths are traveling along a boundary (in or out of the paper in Fig. 1), this assumption fails. Thus, we will modify equations (2) and (3) to include effects of off-great-circle paths treated as diffractions.

**Diffraction Theory and Interfacing Wave Fields**

Interfacing numerical and integral techniques allows flexibility in seismic modeling and is becoming a part of the standard tools discussed in textbooks. Some recent applications involve 2D deep-earth models (Wen and Helmberger, 1998), and mapping abrupt jumps in crustal thickness (Zhu and Helmberger, 1998). Although there are many possible modifications (Frazer and Sen, 1985), the approach followed here is commonly referred to as the Kirchhoff-Helmholtz integral equation (Born and Wolf, 1964), with $\phi_p$ the potential at position $r$.

$$\phi_p (r,t) = \frac{1}{4\pi} \left\{ -\frac{1}{r} \frac{\partial u}{\partial n} + \frac{u \cdot \partial r}{r \partial n} + \frac{1}{\alpha \partial n \partial t} \right\} ds$$  \hspace{1cm} (7)$$

where $u$ is the wave field (potential) on the surface ($S$) retarded by $\tau = t - t_p$, with $t_p$ the travel time from each element to the receiver. A unit vector "$n$" denotes the direction perpendicular to the local surface. The integration is over the surface $S$ with elements $dS$.

This integral is simply a formal description of Huygen’s principle, which states that the disturbance at some later time ($t_p$) can be obtained by summing secondary sources on a surface ($S$). To demonstrate its use, we will consider a simple application in a situation where the answer is known. The model setup is displayed in the upper panel of Figure 3 involving deep ocean sediments with a source in the ocean and receiver below the water-mud interface. The generalized ray solution in equation (2) for element points along the interface ($r$) are displayed on the left in Figure 3, and are a function of depth ($h$) on the right. The lowermost pair of traces displays the comparison of a summation (640 elements) at a depth of 125 m with the analytical solution. Note that this smooth looking response was produced by summing spike-like pulses properly lagged and weighted by $(\partial u / \partial n)$, cosines from equation (7). The response becomes rough when adding fine-scale variation (Scott, 1985). As the depth grows, the head wave evolves into a step and the tunneled direct wave disappears. This allows idealized solutions (geometric rays) without the need of generating the full Cagniard-deHoop Green’s functions. An example of this type of solution is displayed in Figure 4 involving a step along an interface; see Scott and Helmberger (1985) for an assortment of structural shapes. The split of the responses for paths along the step corresponds to the classical result (half of response) and easily derived in both 2D and 3D.

First, we rewrite equation (7) in Laplace transform space,

$$\tilde{\phi}_p (r,s) = \frac{1}{4\pi} \left\{ -\frac{1}{s} \frac{\partial u}{\partial n} + \frac{\tilde{u} \cdot \partial r}{r \partial n} + \frac{1}{\alpha \partial n s} \right\} ds$$  \hspace{1cm} (8)$$

with $s$ the transform variable. We assume a symmetric point source (Fig. 5) which lights up the interface.
Figure 4. Generation of the transmitted response below a faulted-Moho with two pulses formed along the azimuth of the fault and larger single pulses at right-angle positions.

Figure 5. Geometry for 3D analytic evaluation of the Kirchhoff integral in (a). The interface surface is $S$, with solid angle $\Omega$ tracing out $dS$. The normal to the surface is $\hat{n}$. The source, at distance $r_o$ from $S$, generates potential $\phi$ which produces $\phi (S)$ on the surface. Kirchhoff integration gives the result $\phi (P)$ at point $P$, at a distance $r$ from $S$. Geometry for analytic evaluation of the 2D Kirchhoff integral in the lower panel (b). The line interface is $\Gamma$, with angle $\theta$ tracing out $dl$. The normal to the contour is $\hat{n}$. The source, at distance $r_o$ from $\Gamma$, generates potential $\phi$, which produces signal $\phi (\Gamma)$ on the surface. 2D Kirchhoff integration gives the result $\phi (P)$ at point $P$, at a distance $r$ from $\Gamma$. 
\[
\tilde{u}(s) = \frac{1}{r_0} e^{-\frac{s}{r_0}} \tilde{f}(s)
\]

and assume \(|r| = r_0\) and \(\partial r/\partial \mathbf{n} = -\delta r/\delta \mathbf{n}\). We also suppose that near-field terms can be dropped or travel time is large compared with source duration. Note that

\[
d\Omega = \frac{1}{r^2} \frac{\partial r}{\partial \mathbf{n}} dS, \text{ where } \Omega \text{ is the solid angle.} \tag{10}
\]

Then

\[
\tilde{\phi}_p(r) = \tilde{f}(s) \frac{1}{2\pi} \int \frac{e^{-2\frac{s}{r_0}} \frac{s}{r}}{r} d\Omega
\]

Letting

\[
t = \frac{2r}{\alpha} \text{ and } d\Omega = \frac{d\Omega}{dt} dt
\]

we obtain

\[
\phi_p(r) = \frac{d}{dt} \left[ f(t) \ast \frac{1}{2\pi} \frac{1}{\alpha} d\Omega/dt \right] = \left[ f(t) \ast \frac{1}{2\pi} \frac{1}{\alpha} \frac{d^2\Omega}{dt^2} \right] \tag{11}
\]

where \(\Omega(t)\) is the solid angle swept out over the surface (Hilterman, 1975).

\[
\Omega(t) = 2\pi \left( 1 - \frac{t_0}{t} \right) H(t - t_0)
\]

where \(t_0\) is the first arrival (geometric). Note that \(\Omega(t) = 0\), \(t = t_0\) and equal to \(2\pi\) as \(t \to \infty\), and that

\[
\frac{d\Omega^2}{dt^2} = 2\pi \frac{t_0}{t} \delta(t - t_0)
\]

and

\[
\phi_p(r) = \frac{1}{R} f(t - t_0), \text{ since } \alpha = R.
\]

If the left plane is shifted up or down relative to the right plane, we get two pulses with a small timing offset as in Figure 4. Note that the amplitude is strongly controlled by the \((d\Omega/dt)\) which is always large for direct arrivals (stationary). Sharp changes in the interface or in the wave-field timing introduce complexity as discussed in Scott and Helmberger (1985).

A similar result can be derived from line-source theory as discussed by Stead and Helmberger (1988),

\[
\tilde{\phi}_L(r,s) = \tilde{f}(s) \frac{1}{4} \int e^{-2\frac{s}{r_0}} \frac{1}{r} \frac{\partial r}{\partial \mathbf{n}} dl
\]

their equation 47. This integral is over the line with \(dl\) the line element and \((\partial r/\partial \mathbf{n})\) the gradient direction. Now, from the geometry displayed in Figure 5, we can express

\[
d\theta = \frac{1}{r} \frac{\partial r}{\partial \mathbf{n}} dl
\]

and

\[
\phi_L(r,t) = f(t) \ast \frac{1}{2} \frac{d\theta}{dt}
\]

where

\[
\frac{d\theta}{dt} = \frac{2}{t_0} \frac{H(t - t_0)}{(t^2 - t_0^2)^{3/2}}.
\]

Note that if the right or left side of the interface were opaque, we would obtain only half the response. If the opaque region is extended, we lose the singularity and produce a shadow zone.

\[
\phi_L(r,t) = f(t) \ast \frac{1}{2} \frac{H(t - t_0)}{(t^2 - t_0^2)^{3/2}}.
\]

since \(H(t - t_0)\) does not turn on until \(t_0\). Thus we have a simple way of weighting 2D diffractions as their distance away from a square-root singularity, which can be used to approximate the contributions from non-great-circle paths.

We construct a reference plane at a constant depth just above the 3D structure of interest. Note that we could compute the response lighting up this surface from below using the WKV code and then sum these secondary sources by approximating the contributions from non-great-circle paths.

If the left plane is shifted up or down relative to the right plane, we get two pulses with a small timing offset as in Figure 4. Note that the amplitude is strongly controlled by the \((d\Omega/dt)\) which is always large for direct arrivals (stationary). Sharp changes in the interface or in the wave-field timing introduce complexity as discussed in Scott and Helmberger (1985).

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\]
Figure 6. Construction of a reference plane (a) along the horizontal, essentially parallel to the Earth’s surface. The ray path connecting the source with the receiver (Δg) is arriving along the great circle line. A line along the azimuthal arc is included as well as a plot of the Fresnel zone. The position Δ is the location of a virtual receiver. The filled dots are the locations of spatial offsets from the piercing point (1) of the geometric ray specified by equal Δ delays. The lower panel (b) displays the graphical operation of the convolution of with a square-root singularity representing the ψj(t) operator located at to. Thus, the virtual receivers (j’s) nearest (1), the geometric ray, produce the sharpest and strongest contributions.

the pulses will simply average as well known (i.e., Červeny and Soares, 1992). Thus, one can define a Fresnel zone where differential arrivals are confined to be less than (T/2) and the Fresnel boundary becomes

\[ X = \sqrt{2h} \]

or

\[ X = \frac{\sqrt{2h}}{λ} \text{ with } λ \text{ the wavelength.} \]  

(15)

Returning to our general formalism, we define the differential times

\[ Δt_j = δt_{j+1} - δt_j \]

and obtain

\[ δX_j = \sqrt{2hΔt_j} \]

We then compute the wave field \( Ψ_j \) at the various virtual receivers (Xj) and replace \( \left[ 1/r * ψ(r,z,t) \right] \) in equation (2) with

\[ \frac{1}{2} \sum_{i=1}^{n} \left[ \frac{H(t - t_i)}{\sqrt{t + Δt_i}} * ψ_j(t) - \frac{H(t - t_{i+1})}{\sqrt{t + Δt_{i+1}}} * ψ_j(t) \right] \]  

(16)

where \( t_i \) is the travel time from each sample to the receiver (\( Δg \)) and \( Δt_i = t_i - t_o \), the difference in timing between the true geometric path and the diffracted path (i). The \( ψ_j(t) \) are
computed at $\Delta X_j$ away from the geometric path. The $\psi_j$ values can be early or late caused by the (2D) structure, but they are all lagged by the $\Delta t_i$ caused by the extra travel path (corrected for being off azimuth) and systematically losing their strengths and high-frequency with separation. A graphical presentation of the convolution operator is displayed in Figure 6b. For the 2D case, all the $\psi_j = \psi$, the response computed at the true receiver and because $\psi$ behaves like a simple square-root singularity for simple situations (Chapman, 1976), we obtain a step-function turning on at $t_0$ (i.e., Helmberger, 1983). But for the 3D case, we integrate in strips weighted relative to the geometric arrival and summing the responses from the right and left. If these two responses are offset in timing, such as in Figure 4, we would expect two pulses as displayed after applying equation (1). Thus, we can greatly simplify the planar grid summation as discussed in Figures 3 and 4. Still further approximations can be applied based on the Fresnel zone ideas as discussed in the next section.

Application to the African Plume Structure

In this section, we will apply the combination of WKM and diffraction (referred to as DWKM) to approximate synthetics for a 3D model. Thus we will attempt to predict some of the strong azimuthal effects discussed earlier in Figure 2. The edge and sharpness of this boundary were determined by mapping the jumps in SKS as observed on the African Array for a large number of earthquakes at all azimuths (Ni et al., 2003b). The first column in Figure 7 displays the 2D synthetics where only the in-plane motions are included. Note the jump in timing that occurs at the top edge of the figure when the ray paths first sample the slow plume structure. To include the out-of-plane contribution, we apply the

![Figure 7](image-url)
diffractions along an arc at constant epicentral distance as displayed in Figure 8.

We construct a reference plane at a constant depth just above the 3D structure of interest. We could compute the response lighting up this surface from below using the WKM code and then sum these secondary sources by performing a surface integral as discussed earlier. However, we simplify this procedure by replacing this integral with a line integral as displayed in Figure 8a and apply the weighting suggested by equation (16) in the preceding section.

However, this formalism can be made still simpler by adding some more approximations. Let the depth of the reference plane be \( h \) and \( \alpha \) be the average velocity along the path to the surface. Let \( \Delta X \) be the horizontal distance associated with the diffracted paths (i.e., \( \Delta x = \Delta t \)) then

\[
\Delta X \approx \sqrt{2 \alpha \tau h}
\]  

(17)

where \( \tau \) is the differential time (\( \Delta t_i \)) between the geometric time and the path arriving \( \Delta x_i \) away, assuming \( \tau \ll \) total travel time, as in the preceding section. We suggest that, instead of integrating along the arc displayed in Figure 8a, we approximate it based on \( T, h, \) and our level of model definition. Essentially, \( \Delta x \) values must be larger than our tomographic block sizes to warrant consideration, which means that we can approximate the square-root singularity.

We define four times; \( t_g \) the geometric time at the receiver, \( t_f = T/2 \), the Fresnel zone limit, \( t_l = T/8 \), the time defining the average area under the square-root singularity between \( t_f \) and \( t_g \),

\[
t_d = \left( \frac{\sqrt{2}}{4} + 1 \right) T
\]

the time position defining the average area beyond \( t_f \). These times can be substituted into equation (17) to estimate

\[
X_f = \sqrt{\alpha h T}
\]

\[
X_l = \sqrt{\alpha h T/4}
\]

(18)

\[
X_d = \left( \frac{\sqrt{2}}{4} + 1 \right) X_l
\]

If we assume the reference plane situated at a depth of 1500 km, an average shear velocity of 6 km/s, and source duration of 12 s, we obtain \( X_f = 164 \) km and \( X_d = 396 \) km. The synthetic at \( \Delta x \) is then estimated by convolving the four WKM responses at the virtual receivers with the two operators \( O_L \) and \( O_D \) for the right and left positions. These operations are defined by:

![Figure 8](image-url)

Figure 8. A surface of constant depth serving as a reference plane for interfacing Kirchhoff solutions is presented in panel (a). To shorten the calculation, we assume 2D geometry and integrate along the arc (heavy line) which corresponds to constant epicentral distance with variable azimuth. The other dotted lines correspond to other neighboring distances. Four locations are indicated corresponding to projections to the surface of the geometric arrival (\( V_g \)), the Fresnel boundary (\( V_f \)) and two virtual stations \( V_l \) and \( V_d \), representing the lit region and the diffracted region. The lower diagram (b) displays the time corresponding to the above four positions relative to the square-root weighting.

![Figure 9](image-url)

Figure 9. Operators corresponding to the lit region (light line), the diffracted region (dotted line), and 1D case (heavy line). These operators are convolved with WKM responses (2D) to construct the solution.
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\[ dH(t) \left( \frac{H(t)}{t} \right) \hat{O}(t) \]

for the lit region, and

\[ dH(t) \left( \frac{H(t)}{t} \right) \hat{O}_D(t) \]

for the diffracted zone. Note that the latter is a long-period correction because the singularity has been removed. An example set of these operators is given in Figure 9. Note that \( O_D(t) \) starts later because such diffracted arrivals travel further to get to the true receiver. The synthetics in the second and third columns in Figure 7 were generated in this manner. The longer the source duration, the greater the window sampled by the operators as apparent from examining this figure. Note that in a true diffraction application, we would compute the times \( t_i \) and \( t_d \) at the reference arc. But because the ray paths travel nearly parallel from this position to the surface, we neglect their differential paths above the reference line.

A comparison of these DWKM synthetics against a 3D numerical code is given in Figure 10. The numerical code is called SEM which stands for the spectral-element method (Komatitsch and Tromp, 1999, 2002). The 3D model is discussed in Ni et al. (2005) and contains sharp vertical walls. It proves difficult to exactly match the waveforms produced by the two methods because both contain a series of filters describing attenuation, source description, etc. Because we are interested in waveform changes that occur across the array, we generally pick a particularly simple observation and use it as an effective source or empirical source. In Figure 10, we adopted the record near 230° azimuth (SEM) for normalization. The DWKM synthetics are the same as in Figure 7 (third column) except for the change in this empirical source.

Two important features of the data are captured by these predictions. First, the travel-time delays of up to 10 s are quite apparent in the synthetics. However, they occur abruptly in the synthetics between 246° and 244°, whereas in data, the transition is less sharp. Second, the double pulses near 246° are reasonably well matched except the amplitude of the second arrival seems larger in the data. Both of these features argue for some of mismatch in geometry, that is, actual ray paths are not truly parallel to the structure. However, the most important point is in the interpretation of the second arrival. In 2D models or even 1D models, the only way to produce such a delayed pulse at these distances is by

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Figure 10. Comparison of synthetics generated with the DWKM code (analytical) against those from SEM (numerical). The amplitudes are all normalized to the SEM synthetic at the azimuth of 230°. Note the reduction in amplitude where the phases become multipathed or broadened at the edge position.

\[ O_D(t) = \frac{d}{dt} \left[ \frac{(H(t) - t_d)}{\sqrt{t}} * \hat{D}(t) \right] \]

(Komatitsch and Tromp, 1999, 2002). The 3D model is discussed in Ni et al. (2005) and contains sharp vertical walls. It proves difficult to exactly match the waveforms produced by the two methods because both contain a series of filters describing attenuation, source description, etc. Because we are interested in waveform changes that occur across the array, we generally pick a particularly simple observation and use it as an effective source or empirical source. In Figure 10, we adopted the record near 230° azimuth (SEM) for normalization. The DWKM synthetics are the same as in Figure 7 (third column) except for the change in this empirical source.
Figure 11. Boundary layer sensitivity testing for the 2D model presented in Figure 1. Great-circle paths are displayed in map view in panel (a) with some examples of observed SKS waveforms in panel (b). The arrivals are aligned on PREM for event 941020 and on observed SH_d for event 950214. Note that the SKS is elongated relative to SH_d and shows a 5-s offset between 98° and 101°. (c) Model N has a thermal boundary 60 km wide with a 1.5% velocity reduction. Model A has a 6% reduction instead, corresponding to a "plume-type layer." The 3D synthetics are computed by summing the weighted average of these 2D models. The two inside letters correspond to the "lit zone." 2D synthetics are generated for two simple cases in column one (NNNN) and column two (AAAA) for the phase SKS as it samples the eastern edge. The third column contains a 3D model where the model is N into the paper (north) and A out of the paper (south). The synthetics are simulated from four 2D sections, hence the four letters. The fourth column has only the more distant anomaly (200 km off the Great Circle). The column on the right contains observed waveforms from the Tanzania Array (data taken from Ni et al., 2002, displaying considerable variability).
slowing down $S_S$ or by introducing a ULVZ (see, for example, Ni and Helmberger, 2001). Thus, sharp structures require special consideration in waveform modeling. It is difficult to locate complex boundary structure from paths traveling large distances along the edge. A more direct approach is examining the edge along perpendicular paths as introduced in Figure 1. Thus, we choose such a path setup for a second application, Figure 11. Data from three events recorded by the Tanzania Array (Fig. 11b) display complexity near the SKS crossover from slow (inside structure $<96^\circ$) to fast (outside $<102^\circ$) (Ni et al., 2002). The array has an extended cross alignment so that there is some mixing in azimuth and distance. Moreover, the edge is sampled at slightly different locations for each event (Fig. 11a). We again placed a horizontal reference plane directly above the 3D structure and added non-great-circle paths (in and out of the paper). Four strips containing velocity anomalies were placed in the two lit and differential zones for various combinations. Because the velocity contrast reaches 6% for the plume-style strip, the synthetics for the (AAAA) produce very strong diffractions. These data do not support such strong features, although elongated pulses are commonly observed as displayed and some datasets display such trailing-off features (Ni et al., 2005). Discussion and Conclusion

Whereas global tomographic models display considerable variation, they tend to be quite smooth. Hence, the generation of 3D synthetics remains PREM-like (Ni et al., 2005). However, broadband observations from arrays are displaying considerable evidence for multipathing (i.e., Ni et al., 2005). To explain such data, one can suppose that tomographic models have been overly smoothed because of the present methodology of determining both the source location and structure simultaneously. To sharpen features, we can perform mapping procedures based on imposing functional rules (i.e., Sidorin et al., 1999). Because $S_S$ is not observed globally, it is not included in such datasets nor is it produced by global models. It can be produced by adding sharpness as demonstrated in the previous study. Thus, new models can be created and easily tested against auxiliary waveform data by applying DWKM.

In the previous examples, the reference plane was inserted just above a particular strong structural feature, but a more general procedure would be to place it at the bottoming position or halfway between the source and receiver, as suggested in Burdick and Salvado (1986). The applicability of DWKM to such a problem needs to be established and will be pursued in future efforts.

In summary, we introduced a new approach in simulating 3D synthetics called the DWKM method. Instead of tracing rays through 3D structures, we treat the simpler problem of generating 2D synthetics (WKM) for azimuths near the receiver. The positions of these non-great-circle paths at virtual receivers are controlled by the source duration and the distance to the 3D target structure, essentially the Fresnel zone, $X = \sqrt{\delta hT}$. We refer to the interior region as the “Lit” zone and exterior region as the “Diffracted” zone. The 2D WKM responses at these four virtual receivers are weighted and delayed relative to a square-root singularity centered on the true receiver. Results from these approximations are compared with the 3D numerical synthetics (SEM) with satisfactory results. Thus, we have developed a new tool for investigating 3D earth structure which is particularly useful for modeling broadband array data.

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