



Fig. 5. Double bistability,  $T_1/T_2 = 10$ ,  $C = 20$ ,  $\Omega = 24$ ,  $\Phi = 8$ , (a)  $\delta = -0.1$ , (b)  $\delta = 0.1$ .

stability. The optical multistability may be useful for multi-logic computers and signal processing.

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## On the High Power Limit of the Laser Linewidth

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**Abstract**—The quantum mechanical limit of the laser linewidth is shown to imply a residual constant linewidth rather than obey an inverse power dependence as is usually assumed.

THE question of the limiting spectral linewidth of the field of a single mode laser was addressed in the early stages of the laser's development. Schawlow and Townes, the first to concern themselves with this problem, obtained [1]

$$(\Delta\nu)_{\text{laser}} = \frac{2\pi\hbar\nu(\Delta\nu_{1/2})^2}{P} \quad (1)$$

Equation (1) was subsequently modified to [2]

$$(\Delta\nu)_{\text{laser}} = \frac{2\pi\hbar\nu(\Delta\nu_{1/2})^2}{P} \frac{N_2}{[N_2 - N_1(g_2/g_1)]_{\text{th}}} \quad (2)$$

where the factor

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$$\mu = \frac{N_2}{[N_2 - N_1(g_2/g_1)]_{\text{th}}} \quad (3)$$

accounts for the fact that when  $t_1 \neq 0$ , the finite population  $N_1$  of the lower laser level requires a corresponding increase in  $N_2$  in order for the gain to remain equal to the loss. This increases the spontaneous emission noise power, which is proportional to  $N_2$ , and hence  $(\Delta\nu)_{\text{laser}}$ .

The common interpretation of (2) is that it predicts an inverse dependence of  $(\Delta\nu)_{\text{laser}}$  on the power output  $P$ .

It is the purpose of this letter to point out that, according to (2), there should remain a residual laser linewidth, even as  $P \rightarrow \infty$ . This is due to the fact that, unless  $t_1$  is zero, as  $P$  increases,  $N_1$  must increase since the increased net-induced transition rate into level 1 must equal in steady state  $N_1/t_1$  the rate of emptying of level 1. This causes the population  $N_2$  to increase in order to keep  $N_2 - N_1(g_2/g_1)$ , and thus the gain, a constant. At sufficiently high values of  $P$ ,  $N_2$  becomes and stays proportional to  $P$  and the ratio  $N_2/P$  in (2) approaches a constant value, thus leading to a residual power independent linewidth.

To obtain the power ( $P$ ) dependence of  $\mu$ , we solve the conventional laser rate equations

$$\begin{aligned}\frac{dN_2}{dt} &= R - \frac{N_2}{t_2} - \left[ N_2 - N_1 \frac{g_2}{g_1} \right] W_i \\ \frac{dN_1}{dt} &= -\frac{N_1}{t_1} + \left[ N_2 - N_1 \frac{g_2}{g_1} \right] W_i + \frac{N_2}{t_2} \\ \frac{dp}{dt} &= \left[ N_2 - N_1 \frac{g_2}{g_1} \right] W_i - \frac{p}{t_c}\end{aligned}\quad (4)$$

where  $N_2$  and  $N_1$  are the level populations,  $g_{1,2}$  are their degeneracies,  $t_1$  and  $t_2 = t_{\text{spont}}$  are the lifetimes,  $t_c$  is the passive resonator photon lifetime,  $R$  is the pumping rate into level 2,  $W_i$  is the induced transition rate, and  $p$  is the number of photons in the oscillating mode.

At equilibrium,  $d/dt = 0$ , we can solve (4) to obtain

$$\begin{aligned}N_2 - N_1 \frac{g_2}{g_1} &= \frac{R[t_2 - t_1(g_2/g_1)]}{1 + W_i t_2} \\ N_2 &= \frac{R t_2 [1 + W_i t_1 (g_2/g_1)]}{(1 + W_i t_2)}\end{aligned}\quad (5)$$

so that

$$\mu = \frac{N_2}{[N_2 - N_1 (g_2/g_1)]_{\text{th}}} = \frac{t_2}{t_2 - t_1 (g_2/g_1)} \left( 1 + W_i \frac{g_2}{g_1} t_1 \right)\quad (6)$$

where the subscript "th" indicates the value at threshold. The power output, including "wall losses" of the laser, is

$$P = \left[ N_2 - N_1 \frac{g_2}{g_1} \right]_{\text{th}} W_i h\nu\quad (7)$$

which, when used together with (6) in (2), gives

$$\begin{aligned}(\Delta\nu)_{\text{laser}} &= \frac{2\pi h\nu (\Delta\nu_{1/2})^2}{P} \left[ \frac{t_2}{t_2 - t_1 (g_2/g_1)} \right] \\ &+ \frac{c\Delta\nu_{1/2} \lambda_0^2}{8\pi n^3 (\Delta\nu)_{\text{gain}} V} \left[ \frac{t_1}{t_2 (g_1/g_2) - t_1} \right]\end{aligned}\quad (8)$$

where  $\Delta\nu_{1/2} \equiv 1/2\pi t_c$  and  $(\Delta\nu)_{\text{gain}}$  is the linewidth of atomic transition responsible for the laser gain.  $V$  is the mode volume. In obtaining (8), we use

$$\left[ N_2 - N_1 \frac{g_2}{g_1} \right]_{\text{th}} = \frac{8\pi\nu^2 n^3 (\Delta\nu)_{\text{gain}} V t_2}{c^3 t_c} \quad (t_2 = t_{\text{spont}}).\quad (9)$$

The first term on the right-hand side of (8) is the conventional Schawlow-Townes expression containing the inverse  $P$  dependence. The second term is *power independent* and corresponds to a residual linewidth as  $P \rightarrow \infty$ .

To get an idea of the magnitudes involved, we consider the case of a 0.6328  $\mu\text{m}$  HeNe laser with mirror reflectivities of  $R = 0.99$ , a resonator length of  $l = 30$  cm, and take  $t_1/t_2 = 0.1$ . We obtain

$$\Delta\nu_{1/2}(\text{Hz}) = \frac{(1-R)c}{2\pi n l} = 1.6 \times 10^6$$

and

$$\Delta\nu_{\text{laser}}(\text{Hz}) \simeq \frac{10^{-3}}{P(m\omega)} + 3.8 \times 10^{-4}.$$

The residual linewidth thus dominates at power levels exceeding a few milliwatts.

In a semiconductor laser the situation is more complicated. The dynamics of pumping are fundamentally different from those in a simple atomic laser. Charge neutrality will dictate that each injected electron is accompanied by the injection of a hole which would tend to clamp  $N_2$  above threshold. For this reason we expect the above-described linewidth mechanism, if at all present, to have a negligible effect on the linewidth of a semiconductor laser.

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