

A Procedure to Estimate the Absorption Rate of Sound Propagating Through High Temperature Gas

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Abstract

A procedure to estimate the absorption rate of small disturbance acoustic waves propagating through high temperature gas due to relaxation is outlined. The procedure considers more than one relaxation mode, such as vibration modes and chemical reactions. It contains the known results for one relaxation mode as a special case. In the relaxation process, it is assumed that rotation and translation are in equilibrium and that vibration and chemistry may proceed at finite rates, while electronic excitation is assumed to be frozen in the equilibrium state. Some calculations are made as example cases with undisturbed base state in equilibrium for air, carbon dioxide and pure nitrogen in the temperature range from 1000K to 6000K. According to the results, carbon dioxide and air can have strong sound absorption due to vibrational relaxation at a frequency of around 1MHz and at a density ranging between $0.1\text{kg/m}^3 \sim 1.0\text{kg/m}^3$, which are typical conditions of boundary layer transition experiments in the T5 hypervelocity shock tunnel. On the other hand, nitrogen does not have a strong absorption effect even at a very high temperature of 5000K.

Nomenclature

Symbols

A	Matrix for reciprocal of relaxation time constant, 1/s
a	speed of sound, m/s
a_e	equilibrium speed of sound, m/s
a_f	frozen speed of sound, m/s
C	Constant of integration in Equation 16
C_f	Coefficient in Equation 27
\hat{C}_v	specific heat at constant volume per mole, kJ/K mole
D	Absorption parameter, defined by Equation 16
e	energy per unit mass of gas, J/kg, or logarithmic constant
\hat{e}	energy per mole, J/mole
f	Vector of spacial distribution function of disturbance, defined by Equation 12
f	frequency of disturbance, Hz, or arbitrary function of N_j in Equation 29
g	Spacial distribution function for potential ψ , defined in Equation 17
g_e	Degeneracy of electronic excitation of partition function, Q
g_v	Degeneracy of vibrational excitation of partition function, Q
h	Enthalpy per unit mass of gas, J/kg, or Planck constant, $= 6.6256 \times 10^{-34}$, Js
I	Unit matrix
i	Imaginary unit, or index
K	Equilibrium constant
k	Boltzmann constant, $= 1.38054 \times 10^{-23}$ J/K
k_f	Forward reaction rate coefficient, Equation 26
\bar{M}	Averaged molecular weight, kg/mole
M_w	Molecular weight, kg/mole
N	Mole concentration per unit mass of mixture, mole/kg
N_A	Avogadro's number, $= 6.02252 \times 10^{23}$, 1/mole
n_r	Number of reactions
n_{re}	Number of linearly independent reactions
n_s	Number of species
p	Pressure, Pa
p'	Disturbance pressure, Pa
Q	Partition function
q	Vector of nonequilibrium variables measured per unit mass, defined by Equation 21
R	Matrix defined by Equation 23
R'	Matrix defined by Equation 22
R	Universal gas constant, $= 8.31433$ J/K mole
T	Temperature, K
t	Time, s
u	Velocity, m/s
V	Volume, m ³
X	Square of the ratio of the frozen speed of sound and equilibrium speed of sound
x	Coordinate
α	Vector of degrees of reactions per unit mass
η	Coefficient in Equation 27
Θ	Characteristic temperature (rotational, vibrational, or electronic)
Θ_f	Characteristic temperature in forward reaction rate equation (27)

λ	Wave length of disturbance
μ_{sr}	Equivalent molecular weight of species s and r , defined by, $= \frac{Mw_s Mw_r}{Mw_s + Mw_r}$
ν_{ij}	Stoichiometric coefficient of j th species of the i th reaction, defined by, $\nu_{ij} = \nu''_{ij} - \nu'_{ij}$
ν'_{ij}	Stoichiometric coefficient of j th species on the reactants side of the i th reaction
ν''_{ij}	Stoichiometric coefficient of j th species on the products side of the i th reaction
ρ	Density, kg/m ³
σ	Symmetry factor
τ	Relaxation time, s
ψ	Potential function defined by Equation 8
ω	Angular frequency of disturbance wave, 1/s

Subscripts

o	Undisturbed value
el	electronic contribution
$imag.$	Imaginary part
$real$	Real part
rot	Rotational contribution
tr	Transitional contribution
v , or vib	Vibrational contribution

Superscripts

$*$	Undisturbed equilibrium condition
l	Disturbance value

1 Introduction

It is known that the propagation of acoustic waves can be affected significantly by relaxation of thermal vibrational excitation and/or chemical reactions in gases at high temperature. Although a weak relaxation effect of thermal vibrational modes at room temperature can be interpreted as a bulk viscosity, more careful considerations are required when the effect is larger, as has been pointed out by Lighthill¹. Since such absorption phenomena can affect boundary layer transition in hypersonic flow²⁻⁴, estimation of absorption due to relaxation in actual gas composition is important. For a simple case where only one relaxation mode exists, such as in the case of vibrational relaxation, or in an ideal dissociating gas, there are good text books on this phenomenon^{5,6}. Generally speaking, the speed of sound depends on its frequency in relaxing gas, *i.e.*, ranging from the frozen sound speed at high frequency to the equilibrium sound speed at low frequency. For relaxation due to dissociation and/or vibration, the frozen sound speed is larger than the equilibrium sound speed.

In such case, sound wave is always damped by relaxation. This damping rate is a function of its frequency, which has a peak around a frequency of reciprocal of relaxation time (Figure 1, reproduction from Clarke *et. al.*⁵). Maximum damping rate depends on a ratio between the two sound speeds, a_f/a_e . This results is for an ideal dissociating gas of sound speed ratio, a_f/a_e , of approximately 1.18. This figure shows that sound at right frequency can be attenuated to 60% in magnitude per wave length.

However, in high enthalpy flow, such as are produced in the T5 hypervelocity shock tunnel, relaxation of both thermal vibrational modes and chemical reactions can occur simultaneously. The sound speed ratio can change depending on the mole fraction of the species of interest, as well as temperature. Also, several chemical reactions can affect each other so that the situation may be more complicated than a simple sum of the individual damping effects taken separately. In this report, the damping rate will be estimated in such situations where each species may have more than one vibrational mode with different relaxation times, and where several reactions each with a different relaxation time can take place. The procedure here is basically following the method described in Chap. VIII, "Introduction to physical gas dynamics", Vincenti & Kruger⁶. The difference from the text book is that more than two relaxation effects are considered here. In the relaxation process, it is assumed that rotation and translation are in equilibrium, and that vibration and chemistry may proceed at finite rates, while electronic excitation is assumed to be frozen in the equilibrium state.

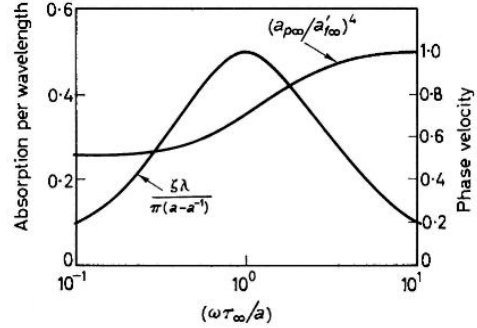


Figure 1: Absorption rate and speed of sound which propagate in ideal dissociating gas. $a_f/a_e \approx 1.183$. Reproduced from Clarke *et. al.*⁵

2 Procedure

Estimation of sound attenuation rate for equilibrium gas at rest

Let \mathbf{q} be a vector of non-equilibrium variables measured per unit mass (for example, these could

include e_v for vibrational non-equilibrium and/or α for ideal dissociating gas). When the disturbance quantities are denoted with $'$, the governing equations for a small disturbance propagating through gas in equilibrium can be written as,

$$\frac{\partial \rho'}{\partial t} + \rho_o \frac{\partial u'_i}{\partial x_i} = 0, \quad (1)$$

$$\rho_o \frac{\partial u_i}{\partial t} + \frac{\partial p'}{\partial x_i} = 0, \quad (2)$$

$$\rho_o \frac{\partial h'}{\partial t} - \frac{\partial p'}{\partial t} = 0, \quad (3)$$

$$h' = h_{p_o} p' + h_{\rho_o} \rho' + \frac{\partial h}{\partial \mathbf{q}} \mathbf{q}', \quad (4)$$

$$\frac{\partial \mathbf{q}'}{\partial t} = \mathbf{A}(\mathbf{q}^* - \mathbf{q}'), \quad (5)$$

$$\mathbf{q}^* = \mathbf{q}^*_{p_o} p' + \mathbf{q}^*_{\rho_o} \rho', \quad (6)$$

where $*$ denotes equilibrium value under the given pressure and density. And \mathbf{A} is a matrix related with the inverse of relaxation time, defined as,

$$\mathbf{A} \equiv -\frac{\partial}{\partial \mathbf{q}} \left(\frac{\partial \mathbf{q}}{\partial t} \right) \quad \left(\sim \frac{1}{\tau} \right). \quad (7)$$

We restrict the discussion to one-dimensional sound propagation. In order to eliminate p' and u' , introduce a function ψ from Equation 2 as follows:

$$p' = -\rho_o \psi_t, \quad u' = \psi_x. \quad (8)$$

Thus, Equation 1 becomes

$$\frac{\partial \rho'}{\partial t} = -\rho_o \psi_{xx}.$$

Substituting into Equation 4, we can get

$$-\psi_{tt} = -\rho_o h_{p_o} \psi_{tt} - \rho_o h_{\rho_o} \psi_{xx} + \frac{\partial h}{\partial \mathbf{q}} \frac{\partial \mathbf{q}'}{\partial t}. \quad (9)$$

Differentiating Equation 5 with respect to time, t , and substituting Equation 6 to eliminate virtual fluctuation of \mathbf{q}^* in the equilibrium state, we get

$$\frac{\partial}{\partial t} \left(\frac{\partial \mathbf{q}'}{\partial t} \right) = \mathbf{A} \left\{ -\rho_o \mathbf{q}^*_{p_o} \psi_{tt} - \rho_o \mathbf{q}^*_{\rho_o} \psi_{xx} - \frac{\partial \mathbf{q}'}{\partial t} \right\}, \quad (10)$$

$$\frac{1 - \rho_o h_{p_o}}{\rho_o h_{\rho_o}} \psi_{tt} - \psi_{xx} + \frac{1}{\rho_o h_{\rho_o}} \frac{\partial h}{\partial \mathbf{q}} \frac{\partial \mathbf{q}'}{\partial t} = 0. \quad (11)$$

Assuming the frequencies for the fluctuation vector \mathbf{q}' and ψ to be identical, *i.e.*,

$$\frac{\partial \mathbf{q}'}{\partial t} = \mathbf{f}(x) e^{i\omega t} \quad (12)$$

$$\psi = g(x) e^{i\omega t}. \quad (13)$$

Then the equations become

$$\frac{1 - \rho_o h_{p_o}}{\rho_o h_{\rho_o}} \omega^2 g - g'' + \frac{1}{\rho h_{\rho_o}} \frac{\partial h}{\partial \mathbf{q}} \mathbf{f} = 0 \quad (14)$$

$$(i\omega \mathbf{I} + \mathbf{A}) \mathbf{f} = \mathbf{A} (\rho_o \omega^2 g \mathbf{q}_{p_o}^* - \rho_o g'' \mathbf{q}_{\rho_o}^*). \quad (15)$$

Solving the above equations, the function g can be written in the form

$$g = C e^{Dx} \quad (16)$$

or,

$$\psi = g e^{i\omega t} = C e^{-\left(\frac{2\pi D_{real}}{D_{imag.}}\right) \frac{x}{\lambda}} e^{i\omega \left(t + \frac{D_{imag.} x}{\omega}\right)}, \quad (17)$$

where

$$D = \pm \sqrt{\frac{-\omega^2 \left(\frac{1}{a_{f_o}^2} - \frac{1}{h_{\rho_o}} \left(\frac{\partial h}{\partial \mathbf{q}} \right) (i\omega \mathbf{I} + \mathbf{A})^{-1} \mathbf{A} \mathbf{q}_{p_o}^* \right)}{1 + \frac{1}{h_{\rho_o}} \left(\frac{\partial h}{\partial \mathbf{q}} \right) (i\omega \mathbf{I} + \mathbf{A})^{-1} \mathbf{A} \mathbf{q}_{\rho_o}^*}}, \quad (18)$$

$$a_{f_o}^2 = \frac{h_{\rho_o}}{\frac{1}{\rho_o} - h_{p_o}},$$

$$\lambda = \frac{a}{f} = -\frac{2\pi(\omega/D_{imag.})}{\omega}.$$

Both for waves propagating in the positive direction ($-\frac{\omega}{D_{imag.}} > 0$) and in the negative direction ($-\frac{\omega}{D_{imag.}} < 0$), positive $\frac{D_{real}}{D_{imag.}}$ means damping. To confirm that this result contains the case of a single relaxation mode as a special case, consider the matrix \mathbf{A} to be reduced to $\frac{1}{\tau}$, where τ is the relaxation time. Introducing another relaxation time, τ^+ ,

$$\tau^+ = \frac{\tau (h_p - 1/\rho)}{h_p + h_q q_p^* - 1/\rho},$$

the absorption parameter, D , can be reduced to

$$D^2 = -\frac{\omega^2 (i\omega \tau^+ + 1)}{i\omega \tau^+ a_f^2 + a_e^2} \quad (19)$$

$$= -\frac{\omega^2}{a_e^2} \left[\frac{1 + X(\omega \tau^+)^2}{1 + X^2(\omega \tau^+)^2} + i \frac{(1 - X)\omega \tau^+}{1 + X^2(\omega \tau^+)^2} \right],$$

where a_e is the equilibrium speed of sound, which can be written as

$$a_e^2 = -\frac{h_\rho + h_q q_\rho^*}{h_p + h_q q_p^* - 1/\rho},$$

and X is defined as the square of the ratio of the frozen to the equilibrium speed of sound,

$$X \equiv (a_f/a_e)^2.$$

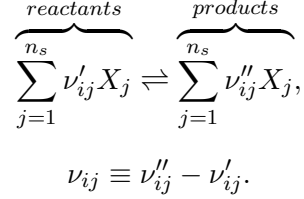
Equation 19 is identical to well-known result for the ideal dissociating gas case^{5,6}. It should be noted that the sign of $\frac{D_{real}}{D_{imag.}}$, which determines whether relaxation acts as damping or amplifying

force, depends on the sign of $1 - X$, *i.e.*, $a_e - a_f$, as can be seen from the sign of the imaginary part of D^2 shown in Equation 19:

$$\frac{D_{real}}{D_{imag.}} \begin{cases} > 0 & (a_f > a_e) : \text{damping} \\ < 0 & (a_f < a_e) : \text{amplifying} \end{cases}.$$

Definition of variables and description of the system

The linearly independent set of chemical reactions can be represented as



Defining a vector α , which represents the degree of advancement of the reactions per unit mass (mole/kg), each species concentration, N_j , moles per unit mass of mixture, can be written by α as

$$N_j = \sum_{i=1}^{n_{r_e}} \alpha_i \nu_{ij} + N_{0j}. \quad (20)$$

The vector of non-equilibrium variables, \mathbf{q} , can be defined as a combination of α and the vibrational energies per unit mass for the molecular species:

$$\mathbf{q} \equiv \begin{pmatrix} \alpha \\ e_v(1) \\ \vdots \\ e_v(n_s) \end{pmatrix}. \quad (21)$$

Since it is necessary to take account of several reaction paths to evaluate the non-equilibrium rate processes properly, a matrix, \mathbf{R}' , which represents the relation between the set of linearly independent reactions (n_{r_e}) and the remaining reactions ($n_r > n_{r_e}$) can be introduced:

$$\boldsymbol{\nu}^* = \begin{pmatrix} \mathbf{I} \\ \mathbf{R}' \end{pmatrix} \boldsymbol{\nu}. \quad (22)$$

where $\boldsymbol{\nu}^*$ is a $n_r \times n_s$ coefficient matrix for all reactions, and \mathbf{R}' is $n_r - n_{r_e} \times n_{r_e}$ matrix. Then, letting α' express the degrees of advancement of reactions $\boldsymbol{\nu}^*$,

$$\alpha = (\mathbf{I} \quad \mathbf{R}') \alpha' \equiv \mathbf{R} \alpha'. \quad (23)$$

Calculation of derivative values

The pressure and density dependence of the \mathbf{q} in equilibrium can be calculated as follows: In the equilibrium state,

$$K_i(T) = \rho^{\sum_j \nu_{ij}} \prod_j N_j^{*\nu_{ij}}, \quad (24)$$

must be satisfied. Using the following form of the equation of state,

$$\frac{dT}{T} = \frac{1}{p} dp - \frac{1}{\rho} d\rho - \overline{M} \sum_i \left(\sum_j \nu_{ij} \right) d\alpha_i, \quad (25)$$

and differentiating the law of mass action (Equation 24) with respect to T , the following equation can be derived

$$\mathbf{A}_p dp + \mathbf{A}_\rho d\rho - \mathbf{A}_\alpha d\boldsymbol{\alpha}^* = 0,$$

where

$$\begin{aligned} \mathbf{A}_{pi} &\equiv \frac{T}{K_i} \frac{dK_i}{dT} \left(\frac{1}{p} \right) \\ \mathbf{A}_{\rho i} &\equiv \left[\frac{T}{K_i} \frac{dK_i}{dT} \left(\frac{1}{\rho} \right) + \frac{\sum_j \nu_{ij}}{\rho} \right] \\ \mathbf{A}_{\alpha ij} &\equiv \left[\frac{T}{K_i} \frac{dK_i}{dT} \bar{M} \sum_k \nu_{jk} + \sum_k \frac{\nu_{ik} \nu_{jk}}{N_k} \right]. \end{aligned}$$

Then, the equilibrium change of the vector $\boldsymbol{\alpha}$ corresponding to given changes in pressure and density can be calculated as follows,

$$\begin{aligned} d\boldsymbol{\alpha}^* &= \mathbf{A}_\alpha^{-1} \mathbf{A}_p dp + \mathbf{A}_\alpha^{-1} \mathbf{A}_\rho d\rho, \\ \left(\frac{\partial \boldsymbol{\alpha}^*}{\partial p} \right) &= \mathbf{A}_\alpha^{-1} \mathbf{A}_p, \\ \left(\frac{\partial \boldsymbol{\alpha}^*}{\partial \rho} \right) &= \mathbf{A}_\alpha^{-1} \mathbf{A}_\rho. \end{aligned}$$

Similarly, the change in vibrational energy, assuming a harmonic oscillator model is

$$de_{v_i}^* = \frac{de_{v_i}^*}{dT} dT = e_{v_i}^* \frac{\left(\frac{\Theta_{v_i}}{T^2} \right) e^{-\frac{\Theta_{v_i}}{T}}}{e^{-\frac{\Theta_{v_i}}{T}} - 1} \left\{ \left(\frac{T}{p} + \frac{\partial T}{\partial \boldsymbol{\alpha}} \frac{\partial \boldsymbol{\alpha}^*}{\partial p} \right) dp + \left(-\frac{T}{\rho} + \frac{\partial T}{\partial \boldsymbol{\alpha}} \frac{\partial \boldsymbol{\alpha}^*}{\partial \rho} \right) d\rho \right\},$$

since

$$dT = \frac{T}{p} dp + \frac{T}{\rho} d\rho + \frac{\partial T}{\partial \boldsymbol{\alpha}} d\boldsymbol{\alpha},$$

where, from Equation 25,

$$\left(\frac{\partial T}{\partial \alpha_i} \right) = -\bar{M} T \sum_k \nu_{ik}.$$

In Equation 18, $\frac{\partial h}{\partial \mathbf{q}}$ as well as h_{ρ_0} and h_{p_0} need to be known. They are calculated under the assumption mentioned before, as,

$$\frac{\partial h}{\partial \rho} = - \sum_{s=1}^{n_s} N_s \frac{T}{\rho} \hat{C}_{v,t+r} - \frac{p}{\rho^2},$$

$$\frac{\partial h}{\partial p} = \sum_{s=1}^{n_s} N_s \frac{T}{p} \hat{C}_{v,t+r} + \frac{1}{\rho},$$

$$\frac{\partial h}{\partial e_{v_i}} = M_i N_i,$$

$$\frac{\partial h}{\partial \alpha_i} = \sum_{j=1}^{n_s} \left[\nu_{ij} (\hat{e}_j + \hat{e}_{0j}) - N_j \bar{M} T \sum_j \nu_{ij} \hat{C}_{v,t+r} \right].$$

The first two equations indicate our assumption of “thermal equilibrium in translation and rotation” and “frozen electronic excitation” in the disturbance wave.

Relaxation time

The relaxation time of chemical reaction is related to reaction rate, $\frac{d\alpha'}{dt}$, each of which can be estimated by

$$\rho \frac{d\alpha'_i}{dt} = k_{f_i} \left[\prod_s (\rho N_s)^{\nu'_{i,s}} - \frac{1}{K_i} \prod_s (\rho N_s)^{\nu''_{i,s}} \right], \quad (26)$$

where, k_{f_j} is the forward reaction rate coefficient of the form

$$k_{f_j} = C_{f_j} T^{\eta_{f_j}} e^{\frac{\Theta_{f_j}}{T}}. \quad (27)$$

The reaction rates for the linearly independent reactions are then derived using Equation 23, *i.e.*,

$$\frac{d\alpha}{dt} = (\mathbf{I} \quad \mathbf{tR}') \frac{d\alpha'}{dt} = \mathbf{R} \frac{d\alpha'}{dt}. \quad (28)$$

In order to differentiate an arbitrary function (say, f) of species concentration, N_j , with respect to α_i , we can use the following relation from Equation 20. The reaction rates for the linearly independent reactions are then derived using

$$\begin{aligned} \frac{\partial f}{\partial \alpha_i} &= \sum_j \frac{\partial f}{\partial N_j} \frac{\partial N_j}{\partial \alpha_i} \\ &= \sum_j \nu_{ij} \frac{\partial f}{\partial N_j}. \end{aligned} \quad (29)$$

Differentiate Equation 28 with respect to α_j , using Equation 29,

$$\frac{\partial}{\partial \alpha_j} \left(\frac{d\alpha_i}{dt} \right) = \sum_k R_{ik} \frac{k_{f_k}}{\rho} \left[\sum_l \left(\frac{\nu'_{kl} \nu_{jl}}{N_l} \right) \prod_s (\rho N_s)^{\nu'_{ks}} - \frac{1}{K_k} \sum_l \left(\frac{\nu''_{kl} \nu_{jl}}{N_l} \right) \prod_s (\rho N_s)^{\nu''_{ks}} \right].$$

When the undisturbed condition is in equilibrium, the above equation can be reduced to

$$\frac{\partial}{\partial \alpha_j} \left(\frac{d\alpha_i}{dt} \right) = - \sum_k R_{ik} \frac{k_{f_k}}{\rho} \left[\sum_l \left(\frac{\nu_{kl} \nu_{jl}}{N_l} \right) \right] \prod_s (\rho N_s)^{\nu'_{ks}}.$$

In the above equation, changes in k_{f_j} and K_k in accordance with temperature changes resulting from $\delta\alpha_i$, *i.e.*, $(\partial K_k / \partial T)(\partial T / \partial \alpha_i)$, are ignored.

The vibrational energy relaxation for species s due to collisions with species r is determined from the expression given by Millikan and White⁷,

$$\ln A_1 \tau_{sr} p = A_2 \mu_{sr}^{0.5} \Theta_{v_s}^{4/3} \left(T^{-1/3} - A_3 \mu_{sr}^{1/4} \right),$$

where μ_{sr} is the equivalent molecular weight between the two species. Constants, A_1 , A_2 and A_3 are,

$$A_1 = 9.8625 \times 10^2 \text{ Pa}^{-1} \text{ s}^{-1} \quad A_2 = 0.0367 \text{ kg}^{-1/2} \text{ mol}^{1/2} \text{ K}^{-5/3} \quad A_3 = 0.08435 \text{ K}^{1/3} \text{ mol}^{1/4} \text{ kg}^{-1/4}.$$

The relaxation time of species s is determined by taking the number-weighted average of τ_{sr} :

$$\tau_s = \frac{\sum_r N_r}{\sum_r \frac{N_r}{\tau_{sr}}} \quad (30)$$

For CO₂, however, since it has four vibrational modes that relax at the same rate according to Camac's experiments⁸, the following formula proposed by him is used here, instead:

$$\ln A_4 \tau_{CO_2} p = A_5 T^{-1/3},$$

where constants A_4 and A_5 are

$$A_4 = 4.8488 \times 10^2 \text{ Pa}^{-1} \text{ s}^{-1} \quad A_5 = 36.5 \text{ K}^{1/3}.$$

Strictly speaking, the vibrational relaxation time might be a function of concentration. However, it is assumed that this effect of the disturbance wave is small. (Vibrational relaxation time is assumed constant through the disturbance wave at a value evaluated with the undisturbed equilibrium concentration.) Then the matrix \mathbf{A} in equation 7 becomes

$$\mathbf{A}_{ij} = \frac{\partial}{\partial \alpha_j} \left(\frac{d\alpha_i}{dt} \right) \quad i, j < n_{re},$$

for chemical relaxation, and

$$\mathbf{A}_{ij} = \begin{cases} 0 & i \neq j \\ \frac{1}{\tau_s} & i = j \end{cases}.$$

for vibrational relaxation.

3 Example cases

This procedure for the absorption rate calculation can be easily applied to various gases, which may have several reactions and vibrational modes. Here, results of some example cases, which are typical boundary layer reference conditions of T5 hypervelocity shock tunnel experiments²⁻⁴.

Estimation of the equilibrium state

The equilibrium condition, including energy, $e_{tr}, e_{rot}, e_{vib}, e_{el}$, pressure and partition functions for each species and for each excitation mode, $Q_{tr}, Q_{rot}, Q_{vib}, Q_{el}$ are required for the sound absorption calculation as an initial undisturbed state. The equilibrium constant of the i -th reaction is determined from the relation below by definition,

$$K_i = \prod \left[\left(\frac{Q_j}{N_A V} \right) e^{-\frac{\epsilon_j}{kT}} \right]^{\nu_{ij}},$$

where, Q_j is the partition function of the j -th species which, for a harmonic oscillator model, can be written as

$$\begin{aligned} \frac{Q_j}{N_A V} &= \frac{Q_{jtr}}{N_A V} Q_{jrot} Q_{jvib} Q_{jel} \\ &= (2\pi M_w T)^{3/2} \left(\frac{k^{3/2}}{N_A^{5/2} h^3} \right) \frac{1}{\sigma} \left(\frac{T}{\Theta_{rot}} \right) \prod \left[\left(1 - e^{-\frac{\Theta_{v_i}}{T}} \right)^{g_{v_i}} \right] \sum g_{e_i} e^{-\frac{\Theta_{e_i}}{T}}. \end{aligned}$$

By substituting these into Equation 24, the mole fraction of each species can be obtained. For nonlinear polyatomic molecules, the rotational partition function should be replaced by

$$\frac{\sqrt{\pi}}{\sigma} \left(\frac{T^3}{\Theta_{rot,A} \Theta_{rot,B} \Theta_{rot,C}} \right)^{1/2}.$$

The energy of each excitation mode is calculated directly from partition functions:

$$e_i = RT^2 \frac{\partial \log Q_i}{\partial T}.$$

Results of some examples with the gases air, carbon dioxide and pure nitrogen are calculated from property data of species (shown in Table 2) and reactions (shown in Table 3) and are compared with a STANJAN⁹ calculation, which is based on JANAF table¹⁰, in Figure 2,3. STANJAN results are indicated by the symbols with circle at each 1000K, while results from the harmonic oscillator model are shown with lines and symbols at each 500K. They show good agreement throughout the temperature range, indicating validity of the harmonic oscillator model at the conditions calculated here.

Air

Using the data shown in Tables 2,3, sound absorption rates per wavelength, as defined by $\frac{2\pi D_{real}}{D_{imag}}$, are calculated and are shown in Figure 4 as functions of disturbance frequency. Since there are a lot of chemical reactions and vibrational modes in the air case, the resultant curves appear quite complicated. However, for sufficiently low temperature, there should be only one relaxation process, *i.e.*, vibration of oxygen molecule. Actually, we can see a weak absorption peak at a temperature below 2000K which corresponds to this mode. Disturbance frequencies lower than the peak absorption frequency behave, in general, like equilibrium disturbances, while much higher frequencies are frozen. As temperature increases, generally speaking, the relaxation time decreases. This means that the peak absorption frequency increases with increasing temperature, as can be seen in the figures. At sufficiently high density, and as the temperature is increased, another and stronger absorption peak, whose frequency is lower, appears and then merges with the first peak. It corresponds to relaxation due to vibration of the nitrogen molecule and to dissociation of oxygen.

For boundary layer transition experiments in the T5 hypervelocity shock tunnel, the frequency range of interest is typically around 1MHz at a density of approximately 0.1kg/m³. In this region, it can be seen that both temperature and density increase cause stronger relaxation effects. At sufficiently high density, considerable absorption can be expected at a temperature of 4000K~5000K.

At $T=2000K$, and $\rho=1.0kg/m^3$, where only vibrational relaxation of oxygen takes place, the minimum value of the ratio of sound speeds a/a_f , is approximately 0.98, so that a strong relaxation effect cannot be expected as is seen in the sound absorption results. Higher temperature cases this ratio reaches values as low as approximately 0.9. This corresponds to vibration of nitrogen and dissociation of oxygen as noted above.

Carbon Dioxide

Estimations of the absorption rate in carbon dioxide are shown in Figure 5. Since all vibrational relaxation times are assumed identical here, the absorption curves have two humps at most, one is for absorption due to this vibration and the other for that due to dissociation of the carbon dioxide molecule. The higher-frequency absorption peaks, which corresponds to vibration, decrease with increasing temperature. This is because the mole fraction of carbon dioxide molecule decreases with increasing temperature due to dissociation. This effect can be seen also in the plots of sound

speed ratio. The first plateau part increases from approximately 0.9 to 0.98 as temperature increase from 1000K to 5000K.

Due to the rich vibrational modes of carbon dioxide molecule and their relatively low characteristic vibrational temperature, absorption at a frequency of around 1MHz is quite strong even at a temperature below 3000K. Also, the sound speed ratio, a/a_f , due to vibration is as low as 0.9, which leads to high sound absorption rate even at relatively low temperature.

Nitrogen

Results for pure nitrogen are shown in Figure 6. Since there are only two relaxation modes, they look quite simple. Due to higher characteristic vibrational temperature and to higher dissociation energy than those of oxygen or carbon dioxide, relaxation gives much lower absorption rate and lower peak frequency than the above two examples. In order to obtain a large absorption effect at a frequency of approximately 1MHz, the temperature has to be even higher than 5000K for a density of 0.1kg/m^3 .

4 Conclusion

A procedure to calculate absorption rates for sound propagating through high temperature gas is extended to conditions where more than two relaxation mechanisms may exist. It contains the known results for one relaxation mode as a special case.

Using the procedure, absorption rates in the gases air, carbon dioxide and pure nitrogen are calculated under several conditions with equilibrium species concentration. According to the results, carbon dioxide and air can have strong sound absorption due to vibrational relaxation at a frequency of around 1MHz and at a density ranging between $0.1\text{kg/m}^3 \sim 1.0\text{kg/m}^3$, which are typical conditions of boundary layer transition experiments in the T5 hypervelocity shock tunnel. On the other hand, nitrogen does not have a strong absorption effect at condition even at a very high temperature of 5000K.

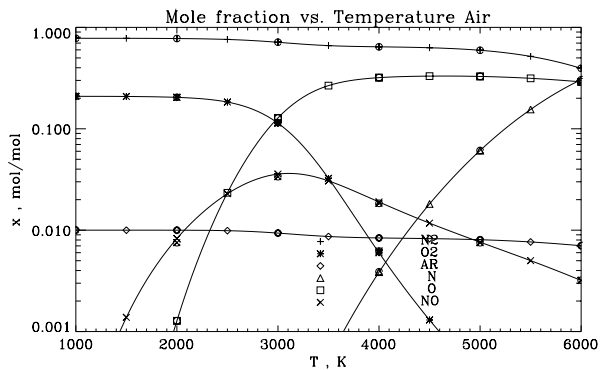
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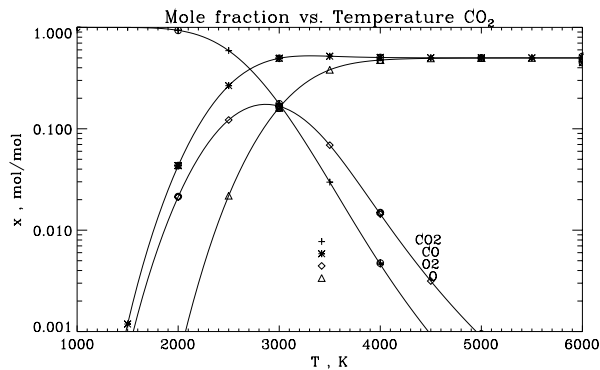
Table 2: Properties used in the calculations

species	M_w g/mol	$\sigma\Theta_{rot}$ K	h_f^o J/mol	g_v	Θ_v K	g_{e_o}	g_{e_i}	ϵ_e J/mol
N ₂	28.016	5.79	0.0	1	3353.2	1	3	6.015×10^5
							6	7.136×10^5
							1	7.342×10^5
O ₂	32.000	4.16	0.0	1	2239.0	3	2	9.225×10^4
							1	1.579×10^5
							3	4.320×10^5
							3	5.960×10^5
Ar	39.944	–	0.0	–	–	1	5	1.115×10^6
							3	1.122×10^6
N	14.008	–	4.713×10^5	–	–	4	6	2.301×10^5
							4	2.308×10^5
							6	3.452×10^5
							12	9.971×10^5
O	16.000	–	2.468×10^5	–	–	5	3	1.903×10^3
							1	2.717×10^3
							5	1.899×10^5
							1	4.044×10^5
							5	8.829×10^5
NO	30.008	2.45	8.990×10^4	1	2699.2	4	2	5.262×10^5
							4	5.496×10^5
C	12.011	–	7.116×10^5	–	–	1	3	1.962×10^2
							5	5.204×10^2
							5	1.219×10^5
							1	2.590×10^5
							5	4.036×10^5
CO ₂	44.011	1.13	-3.933×10^5	2	960.1	1		
				1	1992.5			
				1	3380.2			
CO	28.011	2.78	-1.139×10^5	1	3082.0	1	6	5.824×10^5
							3	6.687×10^5
							6	7.453×10^5
							2	7.785×10^5
H ₂	2.016	175.09	0.0	1	6100.0	1	1	1.097×10^6
							2	1.196×10^6
							3	1.352×10^6
H	1.008	–	2.110×10^5	–	–	1	3	9.839×10^5
							4	1.166×10^6
							5	1.230×10^6

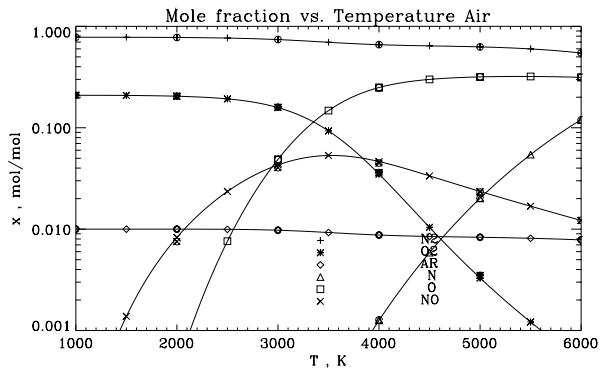
Table 3: Chemical rate coefficients			
Third body	C_f m ³ /mole·s	η_f	Θ_f K
pure N ₂ case			
	N ₂ ⇌ 2N		
N ₂	2.30 × 10 ²³	-3.5	113261.
N	8.50 × 10 ¹⁹	-2.5	113261.
Air case			
	N ₂ ⇌ 2N		
N ₂	2.30 × 10 ²³	-3.5	113261.
N	8.50 × 10 ¹⁹	-2.5	113261.
the others	9.90 × 10 ¹⁴	-1.5	113260.
	O ₂ ⇌ 2O		
O ₂	3.60 × 10 ¹⁵	-1.5	59390.
O	2.10 × 10 ¹²	-0.5	59390.
the others	1.20 × 10 ¹⁵	-1.5	59390.
	NO ⇌ N + O		
all species	5.20 × 10 ¹⁵	-1.5	75500.
	O ₂ + N ⇌ O + NO		
none	1.00 × 10 ⁶	0.5	3625.
	N ₂ + O ⇌ N + NO		
none	5.00 × 10 ⁷	0.0	38020.
	N ₂ + O ₂ ⇌ 2NO		
none	9.10 × 10 ¹⁸	-2.5	65010.
CO ₂ case			
	CO ₂ ⇌ CO + O		
all species	2.88 × 10 ⁵	0.5	37655.
	2CO ⇌ CO ₂ + C		
none	2.33 × 10 ³	0.5	65694.
	CO + O ₂ ⇌ CO ₂ + O		
none	1.60 × 10 ⁷	0.0	20640.
	CO ⇌ C + O		
CO	1.76 × 10 ²⁴	-3.52	128751.
O	1.29 × 10 ²⁵	-3.52	128751.
the others	8.79 × 10 ²³	-3.52	128751.
	O ₂ ⇌ 2O		
O ₂	2.75 × 10 ¹³	-1.0	59754.
O	2.10 × 10 ¹²	-0.5	59382.
the others	2.55 × 10 ¹²	-1.0	59754.
	CO + O ⇌ O ₂ + C		
none	2.73 × 10 ⁵	0.5	69520.



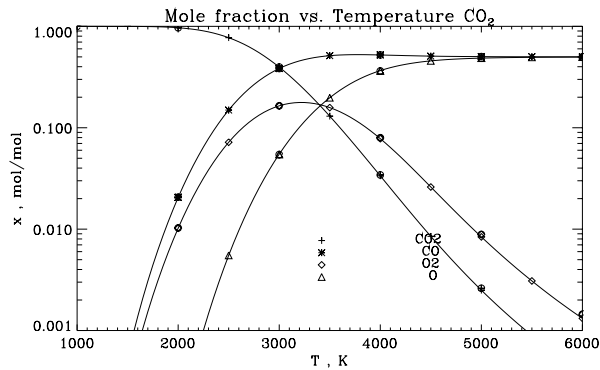
Air, $\rho = 0.01\text{kg/m}^3$



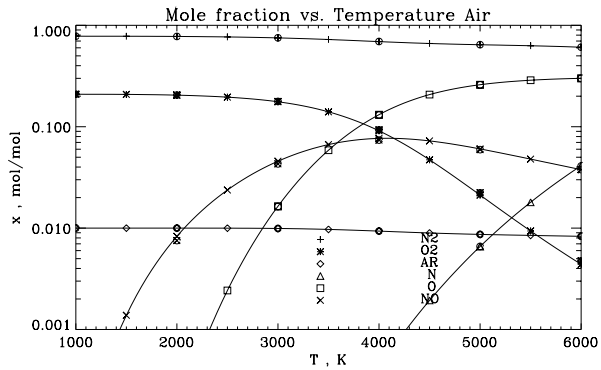
CO₂, $\rho = 0.01\text{kg/m}^3$



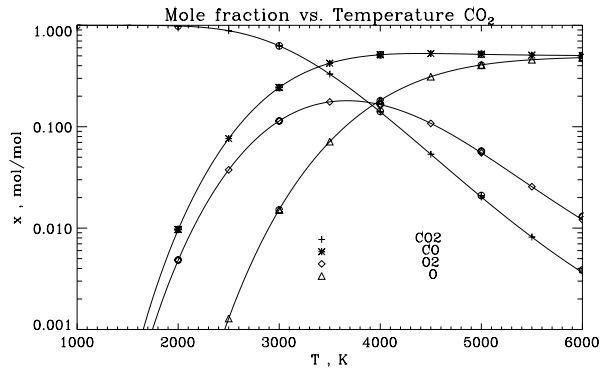
Air, $\rho = 0.10\text{kg/m}^3$



CO₂, $\rho = 0.10\text{kg/m}^3$

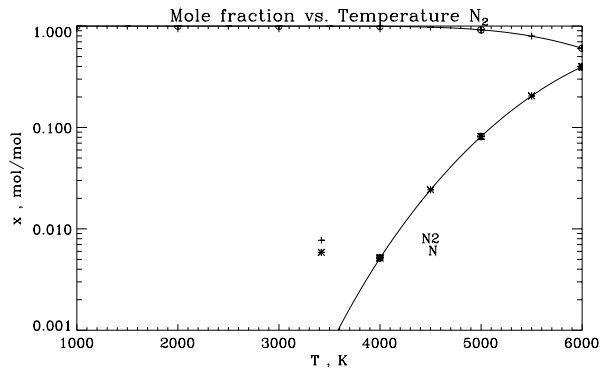


Air, $\rho = 1.0\text{kg/m}^3$

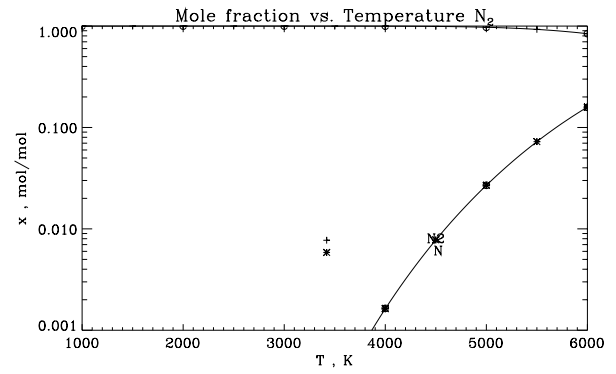


CO₂, $\rho = 1.0\text{kg/m}^3$

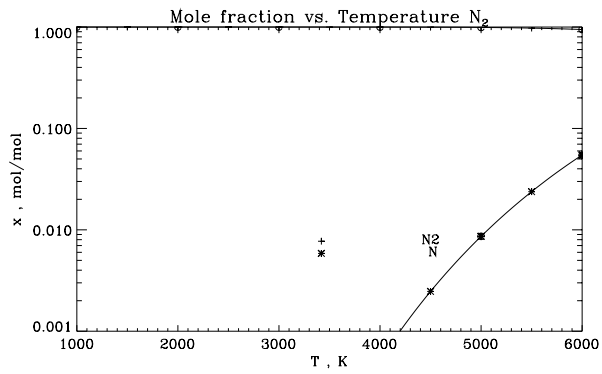
Figure 2: Comparisons of estimated mole concentrations with STANJAN results , symbols with circle, at constant density in equilibrium state



$N_2, \rho = 0.01\text{kg/m}^3$

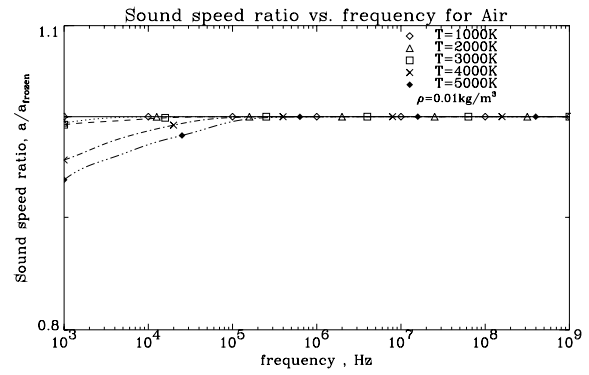
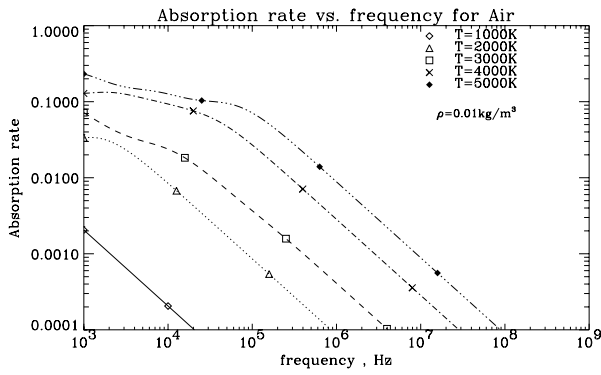


$N_2, \rho = 0.10\text{kg/m}^3$



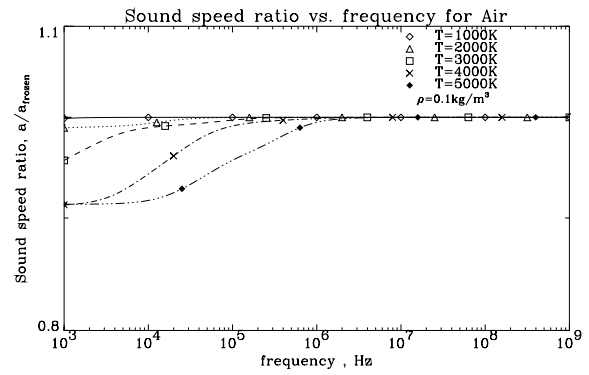
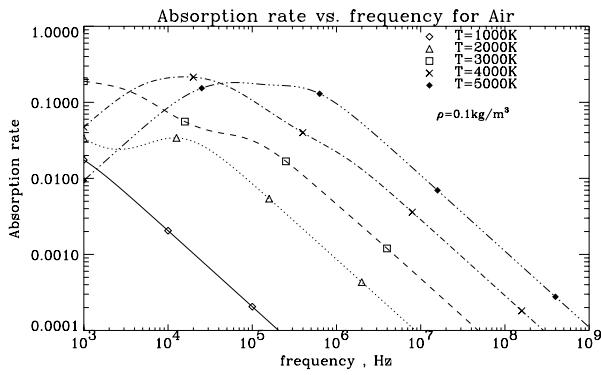
$N_2, \rho = 1.0\text{kg/m}^3$

Figure 3: Comparisons of estimated mole concentrations with STANJAN results, symbols with circle, at constant density in equilibrium state



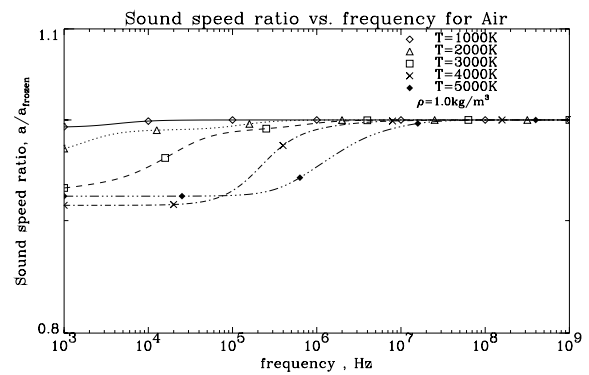
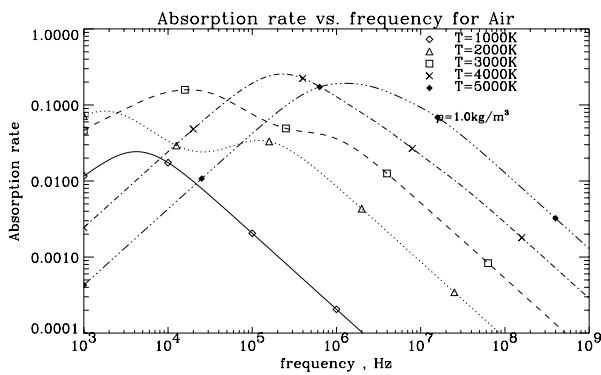
Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 0.01\text{kg/m}^3$, Air

Ratio of sound speeds, a/a_f



Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 0.1\text{kg/m}^3$, Air

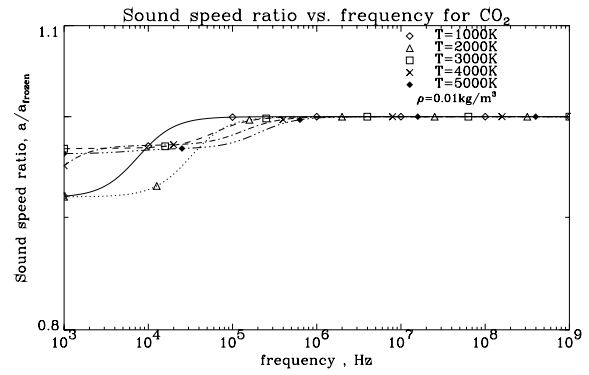
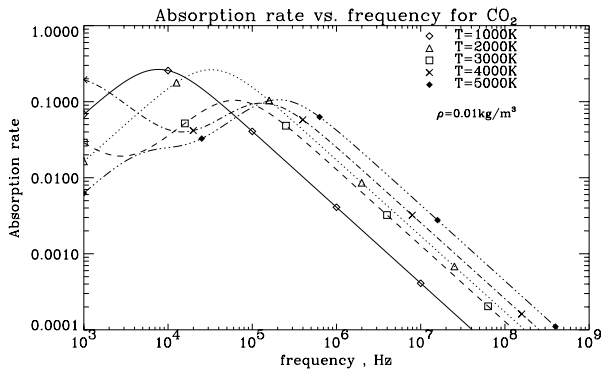
Ratio of sound speeds, a/a_f



Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 1.0\text{kg/m}^3$, Air

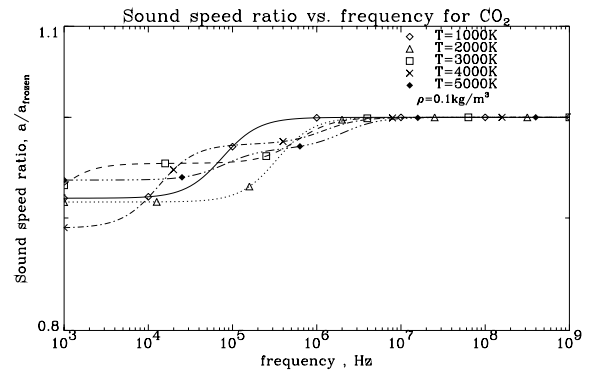
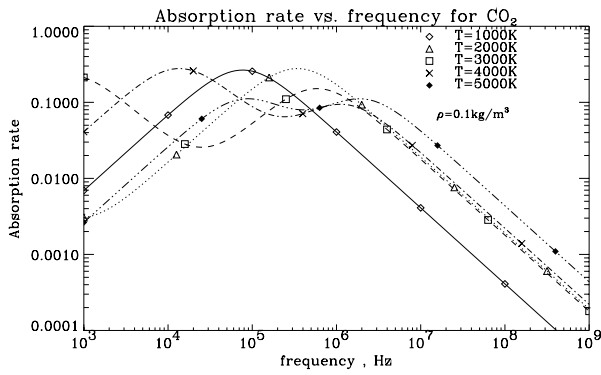
Ratio of sound speeds, a/a_f

Figure 4: Estimated sound absorption rate and sound speeds ratio at constant density versus frequency for air.
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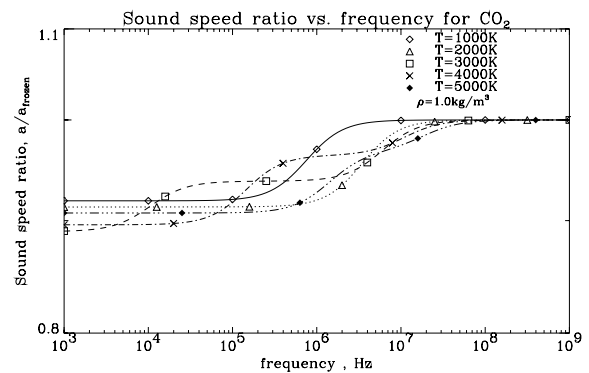
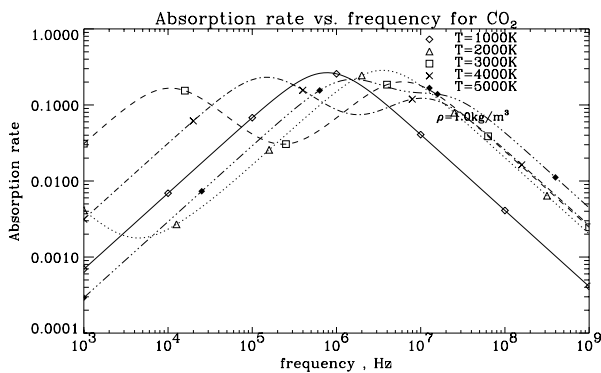
Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 0.01\text{kg/m}^3$, Carbon dioxide

Ratio of sound speeds, a/a_f



Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 0.1\text{kg/m}^3$, Carbon dioxide

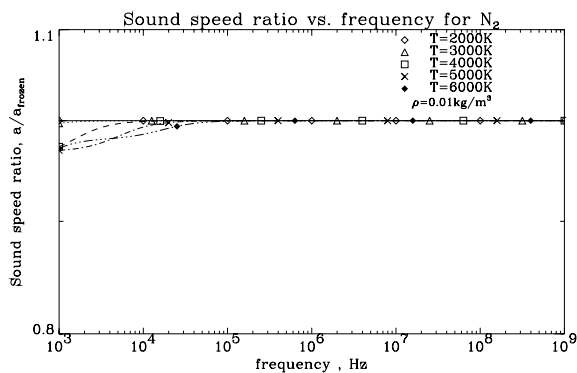
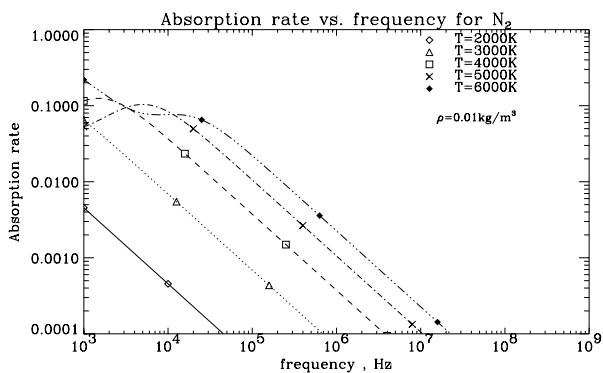
Ratio of sound speeds, a/a_f



Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 1.0\text{kg/m}^3$, Carbon dioxide

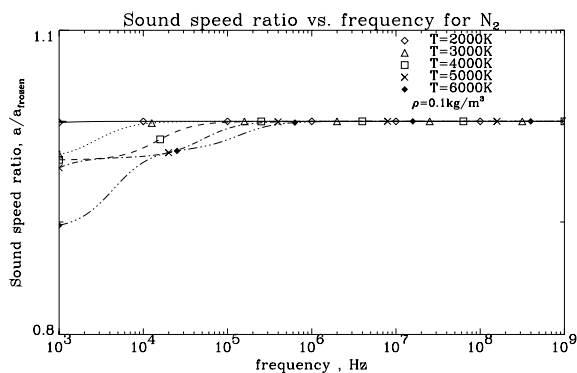
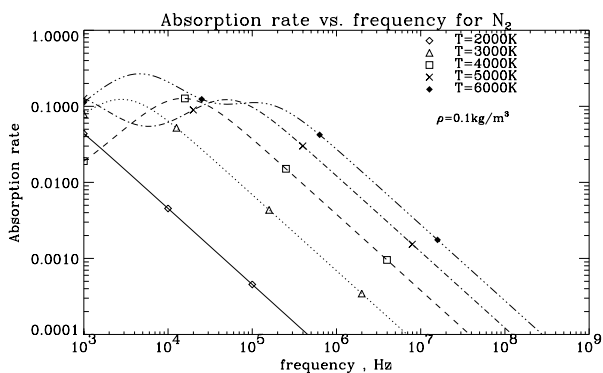
Ratio of sound speeds, a/a_f

Figure 5: Estimated sound absorption rate and sound speeds ratio at constant density versus frequency for carbon dioxide.



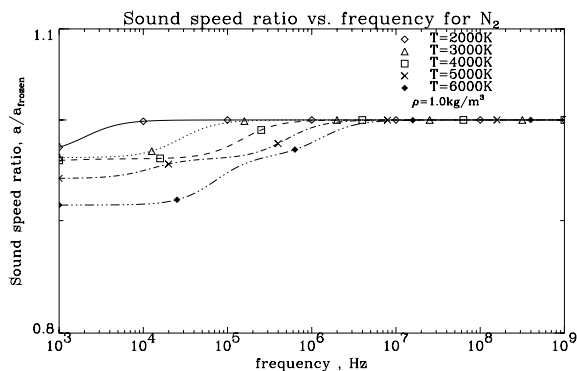
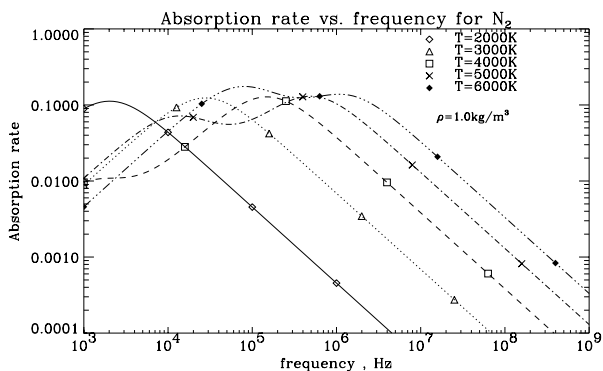
Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 0.01\text{kg/m}^3$, Nitrogen

Ratio of sound speeds, a/a_f



Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 0.1\text{kg/m}^3$, Nitrogen

Ratio of sound speeds, a/a_f



Sound absorption rate per wave length, $\frac{2\pi D_{real}}{D_{imag}}$
 $\rho = 1.0\text{kg/m}^3$, Nitrogen

Ratio of sound speeds, a/a_f

Figure 6: Estimated sound absorption rate and sound speeds ratio at constant density versus frequency for nitrogen.

Appendix

Source programs and an example input file for calculating sound absorption are presented here. “sprg.cpp” is a main program to output sound absorption rate per wave length and sound speed ratio as functions of frequency. “SRP_datd.cpp” is the library program for the procedure described in this memorandum. “SRP_datd.h” is the header file for “SRP_datd.cpp”. “mathfj3.cpp” contains mathematical functions including inverse of matrix and complex operations. Only header file for it appears here.

1. Main program : sprg.cpp

```
//      program sprg.cpp (Sound Propagation in Relaxing Gases)
/* This program is to calculate the effect of relaxing gas effect on the
sound propagation at a rest equilibrium condition.
To compile, type "g++ -o sprg sprg.cpp SRP_datd.cpp ../mathfj3.cpp"
at "/home/keisuke/programs/Processing" directory.
*/
#include <stdio.h>
#include <string.h>
#include <iostream>
#include "SRP_datd.h"

void main() {
    int    ifs;
    float  w,af0,ae0,factau,dwe,freq0;
    vector<float> x0;
    int    i,j,k,stau,iwend;
    RP_dat rp;
    FP_dat fi;
    string fnm;
    char   Path[200],fmo0[200],fmo[200];
    FILE   *fpo;
    printf("select gas propertoes file.\n");
    printf("0:CO2(1ow T)\n1:CO2(n2:N2\n3:Air\n");
    scanf("%d",&ifs);
    strcpy(Path,"/home/keisuke/data/");
    if (ifs==0) {
        fnm   = "/home/keisuke/data/co2lowT.dat";
        stau  = 1; // 1 for CO2, 0 for the others
    } else if (ifs==1) {
        fnm   = "/home/keisuke/data/co2.dat";
        stau  = 1; // 1 for CO2, 0 for the others
    } else if (ifs==2) {
        fnm   = "/home/keisuke/data/n2.dat";
        stau  = 0; // 1 for CO2, 0 for the others
    } else if (ifs==3) {
        fnm   = "/home/keisuke/data/air.dat";
        stau  = 0; // 1 for CO2, 0 for the others
    }
    rp.readReact(fnm,fi.sp);
    printf("# of species = %d\n# of reactions = %d\n",
           ,fi.sp.size(),rp.nr);

    printf("Temperature..(K) ? "); scanf("%f",&fi.T);
    printf("Density..(kg/m3) ? "); scanf("%f",&fi.rhot);

    fi.De0 = 0.;
    fi.SetInit(rp);
    x0.resize(fi.ns);
    for (i=0; i<fi.ns; i++) x0[i] = 0.;
    if (ifs<3) {
        x0[0] = 1.;
    } else if (ifs==3) {
        x0[0] = 0.781;
        x0[1] = 0.209;
        x0[2] = 1.-x0[0]-x0[1];
    }
    fi.N0 = fi.InitN0(1,x0);
    fi.SetEq(rp);
    printf("Mw0=%f\n",fi.Mw0);
    for (i=0; i<fi.ns; i++)
        printf("%s : C[%d]=%f\n",fi.sp[i].HP,i,fi.C[i]);
    for (i=0; i<fi.ns; i++)
        printf("%s : Q[%d]=%e, lQ[%d]=%e, d1Q[%d]=%e\n",fi.sp[i].HP
               ,i,fi.sp[i].Q,i,fi.sp[i].lQ
               ,i,fi.sp[i].d1Q);

    for (i=0; i<rp.nr; i++)
        printf("Keq[%d]=%f, lKeq[%d]=%f, dlKeq[%d]=%f\n",
               ,i,rp.Keq[i],i,rp.dlKeq[i]);
    fi.CalPropfrmQPRT(2,rp);
    rp.Rate(fi.T,fi.rhot,fi.N);
    for (i=0; i<rp.nr; i++) printf("kf[%d]=%e\n",i,rp.kf[i]);
    fi.CalDqEq(rp,stau);
    af0 = sqrt(fi.afz2);
    ae0 = sqrt( (fi.dhdr +fi.dhdq*fi.dqdrE)
                /(1./fi.rhot -fi.dhdq -fi.dhdq*fi.dqdpE) );
    printf("ae0/af0=%e, ae0=%e, af0=%e\n",ae0/af0,ae0,af0);
    printf("dhdr=%e, rest num.=%e\n1./r=%e, -dhdq=%e, rest den.=%e\n",
           ,fi.dhdr,fi.dhdq*fi.dqdrE
           ,1./fi.rhot,-fi.dhdq,-1.*fi.dhdq*fi.dqdpE);
    for (i=0; i<fi.nq; i++)
        printf("q[%d]=%e, dh/dq=%e, dq/dp=%e, dq/drho=%e\n",
               ,i,fi.q[i],fi.dhdq[i],fi.dqdpE[i],fi.dqdrE[i]);
    printf("\n");
    for (i=0; i<rp.nre; i++)
        for (j=0; j<rp.nre; j++)
            printf("dqqa[%d][%d]=%e\n",i,j,fi.dqqa[i][j]);
    for (i=0; i<fi.nv; i++)
        printf("dqqv[%d]=%e\n",i,1./fi.tauv[i]);
    factau = 1 + (fi.dhdq*fi.dqdrE)/fi.dhdr;
    printf("fac-tau-i=%f\n",factau);
    for (i=0; i<fi.nq; i++) {
        for (j=0; j<fi.nq; j++)
            printf("%10.2e",fi.atauv[i][j]);
        printf("\n");
    }

    printf("factau = %e, denomi = %e, af0=%e, "
           ,1. + (1./fi.dhdr)*(fi.dhdq*fi.dqdrE)
           ,1./fi.afz2 - (1./fi.dhdr)*(fi.dhdq*fi.dqdpE)
           ,af0 );
    printf("a[0]/af0=%e\n",
           ,sqrt( ( 1. + (1./fi.dhdr)*(fi.dhdq*fi.dqdrE) )
                /( 1./fi.afz2 - (1./fi.dhdr)*(fi.dhdq*fi.dqdpE) ) )
           /af0 );
    printf("\n");

    printf("frequency to start at..(Hz) ");
    scanf("%f",&freq0);
    printf("Total number of calculation points.. ");
    scanf("%d",&iwend);
    printf("# of points per decade.. ");
    scanf("%f",&dwe);    dwe = 1./dwe;
    printf("Output filename.. ");
    scanf("%s",fmo0);
    sprintf(fmo,"%s%s",Path,fmo0);
    fpo = fopen(fmo,"w");
    printf("%13e%14s%14s\n","freq.,"abs. per lamda","a/af0");
    fprintf(fpo,"%13e%14s%14s\n","freq","abslamda","aaf0");
    for (int iw=0; iw<iwend; iw++) {
        w = freq0*pow(10.,dwe*iw)*(2.*pi_rC);
        fi.sprg(rp,w);
        printf("%13.6e%14.6e%14.6e\n",
               ,w/(2.*pi_rC),fi.Atper1,fi.RtoAf);
        fprintf(fpo,"%13.6e%14.6e%14.6e\n",
               ,w/(2.*pi_rC),fi.Atper1,fi.RtoAf);
    }
    fclose(fpo);
}
```


2.Header file : SRP_datd.h

```

//program SRP_datd.h
#include <stdio.h>
#include <string.h>
#include <math.h>
#include <algorithm>
#include <vector>
#include <string>
#include "/home/keisuke/programs/mathfj3.h"
// using std::string;
// using std::vector;
const double R_Univ = 8.31433; // = k_Boltz x N_Avog
const double k_Boltz = 1.38054e-23;
const double N_Avog = 6.02252e23;
const double h_Planck = 6.6256e-34;
const double khN = 6.26545e5;
// khN actually means (k_Boltz^-1.5)*(h_Planck^-3)*(N_Avog^-2.5)
const double eVtoJ = 1.602e-19;
const double pi_rC = 3.141592654;

class SP_dat { // class for species properties
public:
double T,p,rhs,s,Rgas,thr // entropy is for per mole.
,e,et,er,ee,es // es : formation energy, per mole
,de // de = de/dT
,em // em : energy per unit mass
,Cvt,Cvr,Mw,Avis,Bvis,Cvis,mu
,Q,lQ,dlQ,d2lQ;
int nvmd,nelv,nofa; // # of vib. and elect. mods
vector<double> thv,the,ev,svm; // characteristic temperatures
vector<int> vdg,edg; // degeneracies
char* HP;
double evmEq(double); //!calculate equilibrium vibrational energies
// // from temperature.
// double Tv(); //!calculate vibrational temperature using vib.
// // energy in the member
SP_dat& CalEqProp(double); //!calculate energies in each modes and
// // entropy using partition functions. temperature as the input.
// // " calPartFunc" will be called in this procedure.
private:
SP_dat& CalPartFunc(double);
double QT,QR,QE,lQT,lQR,lQE
,d1lQT,d1lQR,d1lQE
,d2lQT,d2lQR,d2lQE;
vector<double> QV,lQV,d1QV,d2lQV;
// !! This QT is not actually the partition function, but that
// // multiplied by rho/(Mw*n*N_Avog)
// // !! Consequently, for the calculation of entropy etc., log(QT)
// // should be replaced by lQT -ln(rho / Mw), where Mw is molecular
// // weight of the species and rho is density of the species. Though,
// // rho(i)/Mw(i)=rho(mix)*n(i), where n(i) is mole per unit mass of
// // mixture
};

class RP_dat { // class for reactions properties
public:
int nr,nre; // nr:# of reactions
vector<int> s3; // s3:# of subreactions, dim=nr
vector<double> Keq,kf,lKeq,dlKeq; // dim=nr
vector<vector<int>> n0,n1,n2,n3; // n3:species' index of 3rd body
vector<vector<double>> C fj,nfj,thfj; // React. rate param.s for subr.
vector<vector<double>> na;

RP_dat& readGasProp(vector<SP_dat>&);
//!read gas properties from the file of "/home/keisuke/programs/
// // Processing/gasesEqProp.dat" for each species.

RP_dat& readReact(string&,vector<SP_dat>&);
//!read reactions informations. It will call the above procedure
// // of "readGasProp".

RP_dat& CalKeq(double,const vector<SP_dat>&);
//!calculate equilibrium constants from partition function of each
// // species. It is necessary to call "sp.CalPartFunc" procedure
// // before this is called.

RP_dat& Rate(double,double,const vector<double> &);
// // input (Temperature, density, N:mole/kg)
// //!calculate rate coefficients for each reactions. mole
// // concentrations per unit mass, N, is supposed.
};

class FP_dat { // class for flow or mixture properties
public:
int ns,nq,nv; // nq=mv+nre ns:# of species, nv:of v.mode
vector<SP_dat> sp; // dim=ns
vector<int> idxv1,idxv2; // vib. index 1:species, 2:mode
vector<double> C,x,N,N0; // dim=rp.ns
vector<double> q,dhdq,dqdpE,dqdrE,tauv; // dim=nr+ns
vector<vector<double>> atau,dqqa; // dim(atau)=(nre+nv)*(nre+nv)
double p,rhot,T,u,M,s,h,e,de,De0,mu,gam,Cpfc
,T0,P0,h0,Mw0,Rmix,afz2,dhdp,dhdr
,Atperl // attenuation per wave length
,RtoAf; // Ratio to frozen speed of sound

FP_dat& SetInit(const RP_dat&); //!set dimensions of arrays
// // "RP_dat.readReact" is supposed to be called in advance.
// // De0 is the energy to adjust the zero point. It should be
// // determined before "CalPropfrmPRQ" is called.

FP_dat& CalPropfrmQPRQ(int, const RP_dat&);
// // calculates N,C,x,Mw0,Rmix,T,energies,dhdp,dhdr
// // and frozen sound of speed. This procedure is assuming
// // equilibrium condition except vibrational thermal modes.
// // This means translational and rotational temperatures are in
// // equilibrium and electronic temperatures is frozen.

FP_dat& CalVISC(); //!calculate viscosities from temperature
// // and mole fractions(x).

FP_dat& SetEq(RP_dat&); //!input:Temperature & density of mixture
// // This procedure uses Temperature and density as input and
// // calculates N (moles per unit mass of mixture), mole
// // fractions, mass fractions, density of each species, pressure
// // and molecular weight of mixture. q-vector is also calculated.

FP_dat& CalDqEq (const RP_dat&, int); // using T,rhot,p,reaction
// // parameters, N and species informations, calculates matrices
// // and vectors of derivatives, time constants. integer stauv is
// // the sign for the tau formula. stauv=1 for CO2 gas and others
// // for the others.
// // RP_dat::Rate(T,rhot,N) is supposed to be called in advance.

FP_dat& CxfrmN(); // using N and density of mixture,
// // calculates Mw0,C,x and densities of each species.

vector<double> InitN0(int, const vector<double>&);
// // calculates N, concentrations in moles
// // per unit mass of mixture
// // is=0 : from mass fractions, C
// // is=1 : from mole fractions, x

FP_dat& FP_dat::sprg(const RP_dat&, double);
// // This is for estimating the effect of relaxing gas on the
// // sound propagation at a rest equilibrium condition.
// // It calculates Atperl and RtoAf. 2nd parameter is radial
// // frequency in unit of rad/s.

private:
FP_dat& Nvm(const RP_dat&); // from q-vector, calculates N and
// // vibrational energies of each species per unit mass.
};

```

3. Library program : SRP_datd.cpp

```

//program SRP_datd.cpp
#include "SRP_datd.h"

double SP_dat::evmEq(double T) {
double fevm;
fevm = 0.;
for (int i=0; i<nvmd; i++)
fevm += vdg[i]*(R_Univ/Mw)*thv[i]/(exp(thv[i]/T)-1);
return fevm;
}
/*
double SP_dat::Tv() {
double Tvs, ev1, dev;
Tvs = T;
do {
ev1 = evmEq(Tvs);
dev = 0.;
for (int i=0; i<nvmd; i++)
dev += vdg[i]*(R_Univ/Mw)*exp(thv[i]/Tvs)
* pow( thv[i]/( Tvs*(exp(thv[i]/Tvs)-1) ), 2 );
Tvs -= (ev1-evm)/dev;
} while ( fabs(1.-ev1/evm)>1.e-4 );
return Tvs;
}
*/
SP_dat& SP_dat::CalPartFunc(double T) {
double QeN, dQeN, d2QeN;
int i;
QT = khN*pow( 2.*pi_rC*Mw*T, 1.5);
lQT = log(QT);
d1QT = 1.5/T; d21QT = -1.5/(T*T);
QV.resize(nvmd); lQV.resize(nvmd);
d1QV.resize(nvmd); d21QV.resize(nvmd);
if ( nofa==1 ) {
if ( nofa==2 ) {
QR = T/thr;
lQR = log(QR);
d1QR = 1./T; d21QR = -1./(T*T);
} else {
QR = pow(T/thr, 1.5);
lQR = 1.5*log(T/thr);
d1QR = 1.5/T; d21QR = -1.5/(T*T);
}
for (int j=0; j<nvmd; j++) {
lQV[j] = -vdg[j]*log(1.-exp(-thv[j]/T));
d1QV[j] = vdg[j]*(thv[j]/(T*T))/(exp(-thv[j]/T)-1.);
d21QV[j] = (d1QV[j]/T)
*(-2. +(thv[j]/T)/(1.-exp(-thv[j]/T)));
QV[j] = exp(lQV[j]);
}
} else {
QR = 1.; lQR = 0.; d1QR = 0.; d21QR = 0.;
for (int j=0; j<nvmd; j++) {
lQV[j] = 0.;
d1QV[j] = 0.;
d21QV[j] = 0.;
QV[j] = 1.;
}
}
QE = edg[0]; dQeN = 0.; d2QeN = 0.;
for (int j=1; j<nelv; j++) {
QeN = edg[j]*exp(-the[j]/T);
QE += QeN;
dQeN += QeN*the[j];
d2QeN += QeN*the[j]*(-2.*T + the[j]);
}
lQE = log(QE);
if (fabs(QE)>1.e-10) {
d1QE = ( dQeN/QE )*( 1./T );
d21QE = -d1QE+d1QE + (d2QeN/(T*T*T))/QE;
} else {
d1QE = 0.;
d21QE = 0.;
}
Q = QT*QR*QE; for (i=0; i<nvmd; i++) Q *= QV[i];
lQ = lQT + lQR + lQE; for (i=0; i<nvmd; i++) lQ += lQV[i];
d1Q = d1QT + d1QR + d1QE; for (i=0; i<nvmd; i++) d1Q += d1QV[i];
d21Q = d21QT + d21QR + d21QE;
for (i=0; i<nvmd; i++) d21Q += d21QV[i];
return *this;
}
}
SP_dat& SP_dat::CalEqProp(double T) {
CalPartFunc(T);
s = R_Univ*(lQ + 1. *T*d1Q - log(rhs/Mw));
// remember, symbol "Q" here is NOT a partition function, Q,
// but Q / N_Avog x V.
e = R_Univ*T*d1Q; de = R_Univ*T*(2.*d1Q +T*d21Q);
et = R_Univ*T*d1QT;
er = R_Univ*T*d1QR;
ee = R_Univ*T*d1QE;
for (int i=0; i<nvmd; i++) {
ev[i] = R_Univ*T*d1QV[i];
evm[i] = ev[i]/Mw;
}
em = e/Mw;
return *this;
}
}
RP_dat& RP_dat::readGasProp(vector<SP_dat>& sp) {
vector<double> At, Bt, Ct, mwt, thrt, shjap;
vector<vector<double>> thvt, Elj;
vector<int> nvmdt, nelvt, nofat;
vector<vector<int>> vdg, edgt;
int i, j, k, n, ns;
char fn[200], dchr;
vector<char*> HPt;
FILE *fp;
ns = sp.size();
strcpy(fn, "/home/keisuke/programs/Processing/gasesEqProp.dat");
fp = fopen(fn, "r");
fscanf(fp, "%d", &n);
for (i=0; i<2; i++) do { fscanf(fp, "%c", &dchr); } while (dchr!='\n');
mwt.resize(n); At.resize(n); Bt.resize(n); Ct.resize(n);
HPt.resize(n); thrt.resize(n); vdg.resize(n); thvt.resize(n);
Elj.resize(n); nvmdt.resize(n); edgt.resize(n);
nofat.resize(n); nelvt.resize(n); shjap.resize(n);
for (i=0; i<n; i++) {
HPt[i] = (char*)malloc(sizeof(char)*5);
fscanf(fp, "%s%lf%d%le%lf%lf%lf%lf"
, HPt[i], &mwt[i], &nofat[i], &thrt[i], &shjap[i],
&At[i], &Bt[i], &Ct[i]);
do { fscanf(fp, "%c", &dchr); } while (dchr!='\n');
fscanf(fp, "%d", &nvmdt[i]);
vdgt[i].resize(nvmdt[i]); thvt[i].resize(nvmdt[i]);
for (k=0; k<nvmdt[i]; k++)
fscanf(fp, "%d %lf", &vdgt[i][k], &thvt[i][k]);
do { fscanf(fp, "%c", &dchr); } while (dchr!='\n');
fscanf(fp, "%c", &dchr); } while (dchr!='\n');
fscanf(fp, "%d", &nelvt[i]);
edgt[i].resize(nelvt[i]); Elj[i].resize(nelvt[i]);
for (k=0; k<nelvt[i]; k++)
fscanf(fp, "%d %lf", &edgt[i][k], &Elj[i][k]);
do { fscanf(fp, "%c", &dchr); } while (dchr!='\n');
}
}
fclose(fp);
for (i=0; i<n; i++) {
for (j=0; j<n; j++)
if ( strcmp(sp[i].HP, HPt[j])==0 ) {
sp[i].Mw = mwt[j]/1.e3;
sp[i].nofa = nofat[j];
sp[i].thr = thrt[j];
sp[i].es = shjap[j];
sp[i].Avis = At[j];
sp[i].Bvis = Bt[j];
sp[i].Cvis = Ct[j];
sp[i].nvmd = nvmdt[j];
sp[i].vdg.resize(sp[i].nvmd);
sp[i].thv.resize(sp[i].nvmd);
sp[i].ev.resize(sp[i].nvmd);
sp[i].evm.resize(sp[i].nvmd);
for (k=0; k<sp[i].nvmd; k++) {
sp[i].vdg[k] = vdgt[j][k];
sp[i].thv[k] = thvt[j][k];
}
sp[i].nelv = nelvt[j];
sp[i].the.resize(sp[i].nelv);
sp[i].edg.resize(sp[i].nelv);
for (k=0; k<sp[i].nelv; k++) {
sp[i].edg[k] = edgt[j][k];
sp[i].the[k] = Elj[j][k]/R_Univ;
}
sp[i].Rgas = R_Univ/sp[i].Mw;
sp[i].Cvt = 1.5*R_Univ;
if (sp[i].nofa>1)
sp[i].Cvr = R_Univ;
else
sp[i].Cvr = 0.;
}
}
return *this;
}
}
RP_dat& RP_dat::readReact(string& fns, vector<SP_dat>& sp) {
int i, j, ns;
const char* fnm = fns.c_str();
FILE *fp;
char dchar;
fp = fopen(fnm, "r");
fscanf(fp, "%d %d", &ns, &nr);
sp.resize(ns);
Keq.resize(nr); lKeq.resize(nr); dlKeq.resize(nr);
kf.resize(nr); s3.resize(nr);
n0.resize(nr); n1.resize(nr); n2.resize(nr); n3.resize(nr);
Cfj.resize(nr); nfj.resize(nr); thfj.resize(nr);
for (i=0; i<ns; i++) {
sp[i].HP = (char*)malloc(sizeof(char)*4);
fscanf(fp, "%s", sp[i].HP);
}
do { fscanf(fp, "%c", &dchar); } while (dchar!='\n');
readGasProp(sp);
for (i=0; i<nr; i++) {
n0[i].resize(ns); n1[i].resize(ns);
n2[i].resize(ns);
for (j=0; j<ns; j++) fscanf(fp, "%d", &n1[i][j]);
for (j=0; j<ns; j++) {
fscanf(fp, "%d", &n2[i][j]);
n0[i][j] = n2[i][j] - n1[i][j];
}
fscanf(fp, "%d", &s3[i]);
n3[i].resize(s3[i]); Cfj[i].resize(s3[i]);
nfj[i].resize(s3[i]); thfj[i].resize(s3[i]);
if (s3[i]>1) for (j=0; j<s3[i]-1; j++)
fscanf(fp, "%d%lf%lf%lf", &n3[i][j], &Cfj[i][j],
&nfj[i][j], &thfj[i][j]);
}
}
}

```

```

        j = s3[i]-1;
        fscanf(fp,"%d%lf%lf%lf",&Cfj[i][j],&nfj[i][j],
            &thfj[i][j]);
    }
    n3[i][j] = -1;
}
if (nr>1) {
    fscanf(fp,"%d",&nre);
    na.resize(nre);
    for (i=0; i<nre; i++)
        na[i].resize(nr);
    for (i=0; i<nr; i++)
        for (j=0; j<nre; j++)
            fscanf(fp,"%lf",&na[j][i]);
} else {
    nre = 1;
    na.resize(1);
    na[0].resize(1);
    na[0][0] = 1.;
}
fclose(fp);
return *this;
}

RP_dat& RP_dat::CalKeq(double T, const vector<SP_dat> &sp) {
    int i,j,ns;
    ns = sp.size();
    for (i=0; i<ns; i++) {
        Keq[i] = 1.;
        lKeq[i] = 0.;
        dlKeq[i] = 0.;
        for (j=0; j<ns; j++) {
            Keq[i] *= pow( sp[j].Q*exp(-sp[j].es/(R_Univ*T))
                ,n0[i][j]);

            lKeq[i] += n0[i][j]*( sp[j].lQ
                -sp[j].es/(R_Univ*T) );
            dlKeq[i] += n0[i][j]*( sp[j].dlQ
                +(sp[j].es/(R_Univ*T*T) ) );
        }
    }
    return *this;
}

RP_dat& RP_dat::Rate(double T, double rhot, const vector<double> &N) {
    double sN,sN1;
    int i,j,ns;
    ns = N.size();
    sN = 0.;
    for (i=0; i<ns; i++) sN += N[i];
    for (i=0; i<nr; i++)
        if (s3[i]>1) {
            kf[i] = 0.; sN1 = 0.;
            for (j=0; j<s3[i]-1; j++) {
                kf[i] += Cfj[i][j]*pow(T,nfj[i][j])
                    *exp(-thfj[i][j]/T)
                    *rhot*N[n3[i][j]];
                sN1 += N[n3[i][j]];
            }
            j = s3[i]-1;
            kf[i] += rhot*(sN-sN1)*Cfj[i][j]*pow(T,nfj[i][j])
                *exp(-thfj[i][j]/T);
        } else {
            j = 0;
            kf[i] = Cfj[i][j]*pow(T,nfj[i][j])
                *exp(-thfj[i][j]/T);
        }
    return *this;
}

FP_dat& FP_dat::SetInit(const RP_dat& rp) {
    int i,j,inv;
    ns = sp.size();
    nv = 0;
    for (i=0; i<ns; i++)
        for (j=0; j<sp[i].nvmd; j++)
            nv++;
    idxv1.resize(nv); idxv2.resize(nv); inv = 0;
    for (i=0; i<ns; i++)
        for (j=0; j<sp[i].nvmd; j++) {
            idxv1[inv] = i;
            idxv2[inv] = j;
            inv++;
        }
    nq = rp.nre + nv;
    N.resize(ns); NO.resize(ns); C.resize(ns); x.resize(ns);
    q.resize(nq); dhdq.resize(nq);
    dqdpE.resize(nq); dqdrE.resize(nq);
    atau.resize(nq); for (i=0; i<nq; i++) atau[i].resize(nq);
    return *this;
}

FP_dat& FP_dat::CalPropfrmQPRT(int isp, const RP_dat& rp) {
    int i,j;
    NevM(rp); // N and evm are from q-vector.
    Mw0 = 0.;
    for (i=0; i<ns; i++) Mw0 += N[i];
    Mw0 = 1./Mw0;
    Rmix = R_Univ/Mw0;
    if (isp==0) p = (rhot*Rmix)*T;
    else if (isp==1) rhot = p/(Rmix*T);
    else T = p/(rhot*Rmix);
    for (i=0; i<ns; i++) {
        sp[i].T = T;
        sp[i].p = p;
        sp[i].CalEqProp(T); // !Here, evm is overwritten to
            // equilibrium values.
    }
    NevM(rp); // Replace evm again. Usually it is not needed.
    e = De0; de = 0.;
}

for (i=0; i<ns; i++) {
    C[i] = sp[i].Mw*N[i];
    x[i] = Mw0*N[i];
    sp[i].rhs = rhot*C[i];
    for (j=0; j<sp[i].nvmd; j++)
        sp[i].ev[j] = sp[i].evm[j] *sp[i].Mw;
    sp[i].e = sp[i].et +sp[i].er +sp[i].ee;
    for (j=0; j<sp[i].nvmd; j++)
        sp[i].e += sp[i].ev[j];
    sp[i].em = sp[i].e /sp[i].Mw;
    e += N[i]*( sp[i].e + sp[i].es );
    de += N[i]*sp[i].de;
}
h = e +p/rhot;
Cpfz = de +Rmix;
dhdr = -p/(rhot*rhot);
dhdp = 1./rhot;
for (i=0; i<ns; i++) {
    dhdr -= N[i]*(sp[i].Cvt+sp[i].Cvr)*T/rhot;
    dhdp += N[i]*(sp[i].Cvt+sp[i].Cvr)*T/p;
}
afz2 = dhdr/(1./rhot -dhdp);
gam = 1. +Rmix/de;
return *this;
}

FP_dat& FP_dat::CalVISC() {
    double phi;
    int k;
    for (k=0; k<ns; k++)
        sp[k].mu = 0.1*exp( ( sp[k].Avis*log(T)
            +sp[k].Bvis)*log(T)
            +sp[k].Cvis );
    mu = 0.;
    for (k=0; k<ns; k++) {
        phi = 0.;
        for (int l=0; l<ns; l++) {
            phi += x[l]*pow( 1.+sqrt(sp[k].mu/sp[l].mu)
                *pow(sp[l].Mw/sp[k].Mw,0.25),2.0)
                /sqrt( 8.*(1.+sp[k].Mw/sp[l].Mw) );
        }
        mu += x[k]*sp[k].mu/phi;
    }
    return *this;
}

FP_dat& FP_dat::SetEq(RP_dat& rp) {
    vector<vector<double>> df,idf;
    vector<double> f,a,da;
    vector<double> Nt;
    double det;
    double fda,dis0,dif0;
    int k,ni,nj,nre,mi,nofi;
    nre = rp.nre;
    df.resize(nre); for (ni=0; ni<nre; ni++) df[ni].resize(nre);
    f.resize(nre); da.resize(nre); a.resize(nre);
    Nt.resize(ns);
    for (ni=0; ni<ns; ni++)
        sp[ni].CalEqProp(T);
    rp.CalKeq(T,sp);
    for (ni=0; ni<nre; ni++) {
        a[ni] = 0.;
        da[ni] = 0.;
    }
    nofi = 0;
    do {
        N = NO;
        for (k=0; k<ns; k++)
            for (ni=0; ni<nre; ni++)
                N[k] += rp.n0[ni][k]*a[ni];
        for (k=0; k<ns; k++)
            printf("N[%d]=%e, ",k,N[k]);
        printf("\n");
        for (ni=0; ni<nre; ni++) {
            for (nj=0; nj<nre; nj++) {
                df[ni][nj] = 0.;
                for (k=0; k<ns; k++)
                    if (rp.n0[ni][k]*rp.n0[nj][k]!=0)
                        df[ni][nj] += rp.n0[ni][k]
                            *rp.n0[nj][k]/N[k];
            }
            f[ni] = 0.;
            for (k=0; k<ns; k++)
                f[ni] += rp.n0[ni][k]*log(rhot*N[k]);
            f[ni] -= rp.lKeq[ni];
        }
        InvMtx(df,idf,det);
        printf("det=%e\n\n",det);
        da = -1.*(idf*f);
        fda = 0.5;
        Nt = NO;
        for (k=0; k<ns; k++) for (ni=0; ni<nre; ni++)
            Nt[k] += rp.n0[ni][k]*(a+fda*da)[ni];
        while ( Minelement(Nt,&mi)<0. ) {
            fda *= 0.5;
            Nt = NO;
            for (k=0; k<ns; k++) for (ni=0; ni<nre; ni++)
                Nt[k] += rp.n0[ni][k]*(a+fda*da)[ni];
        }
        dif0 = vabs(da);
        a = a +fda*da;
        dis0 = 0.;
        for (ni=0; ni<nre; ni++)
            dis0 += pow( f[ni]/rp.lKeq[ni],2 );
        dis0 = sqrt(dis0);
        for (int i=0; i<ns; i++) printf("%f ",Nt[i]);
        printf("dis0=%e, dif0=%e, fda=%e\n",dis0,dif0,fda);
    }
}

```

```

//      scanf("%*c");
//      } while ( ( dis0>1.e-6 )&&(dif0>1.e-6) );
//      } while ( ( dis0>1.e-6 )&&(nofi<500 ) );
//      if (dis0>1.e-6) printf("Disagreement (ratio) is %f\n",dis0);
//      } while ( dif0>1.e-8 );
for (ni=0; ni<rp.nre; ni++)
    q[ni] = 0.;
for (ni=0; ni<nre; ni++)
    q[ni] = a[ni];
for (ni=0; ni<nv; ni++)
    q[nre+ni] = sp[idxv1[ni]].evm[idxv2[ni]];
N = Nt;
CxfrmN();
p = rhot*(R_Univ/Mw0)*T;
return *this;
}

FP_dat& FP_dat::CalDqEq (const RP_dat& rp, int stauv) {
    int i,j,s,nr,nre;
    double det,devT,redM,sNtvs,tauv,thvT,ata,bta;
    vector<vector<double>> taa,aa,iaa,snn0n,dqqan;
    vector<double> ap,ar,sn0,dap,dar,dTa,devr,devr,pini;
    atau.resize(nq);
    for (i=0; i<nq; i++) {
        atau[i].resize(nq);
        for (j=0; j<nq; j++) atau[i][j] = 0.;
    }
    nr = rp.nr; nre = rp.nre;
    sn0.resize(nr); snn0n.resize(nr); taa.resize(nre);
    dqqan.resize(nr); pini.resize(nr); aa.resize(nre);
    ap.resize(nre); ar.resize(nre); aa.resize(nre);
    dap.resize(nre); dar.resize(nre); dqa.resize(nre);
    for (i=0; i<nr; i++) {
        snn0n[i].resize(nr);
        dqqan[i].resize(nr);
    }
    for (i=0; i<nre; i++) {
        dqa[i].resize(nre);
        aa[i].resize(nre);
        taa[i].resize(ns);
    }
    devp.resize(nv); devr.resize(nv); tauv.resize(nv);
    for (i=0; i<nr; i++) {
        sn0[i] = 0.; pini[i] = 1.;
        for (s=0; s<ns; s++) {
            sn0[i] += rp.n0[i][s];
            pini[i] *= pow(rhot*N[s],rp.n1[i][s]);
        }
        for (j=0; j<nr; j++) {
            snn0n[i][j] = 0.;
            for (s=0; s<ns; s++)
                if ( rp.n0[i][s]*rp.n0[j][s]!=0 )
                    snn0n[i][j] += rp.n0[j][s]
                        *rp.n0[i][s]/N[s];
        }
    }
    for (i=0; i<nre; i++) {
        ap[i] = T*rp.dlKqEq[i]/p;
        ar[i] = -(T*rp.dlKqEq[i]+sn0[i])/rhot;
        for (j=0; j<ns; j++) {
            if (rp.n0[i][j]==0)
                taa[i][j] = T*rp.dlKqEq[i]*Mw0;
            else
                taa[i][j] = T*rp.dlKqEq[i]*Mw0
                    *rp.n0[i][j]/N[j];
        }
    }
    for (i=0; i<nre; i++) for (j=0; j<nre; j++) {
        aa[i][j] = 0.;
        for (int k=0; k<ns; k++) aa[i][j] += taa[i][k]*rp.n0[j][k];
    }
    InvMtx(aa,iaa,det);
    dap = iaa*ap;
    dar = iaa*ar;
    for (i=0; i<nre; i++)
        for (j=0; j<nre; j++) {
            dqa[i][j] = 0.;
            for (int k=0; k<ns; k++)
                dqa[i][j] += rp.na[i][k]*(rp.kf[k]/rhot)
                    *snn0n[k][j]*pini[k];
        }
    for (i=0; i<nre; i++) {
        dqpE[i] = dap[i];
        dqrE[i] = dar[i];
        dhdq[i] = 0.;
        for (j=0; j<ns; j++)
            dhdq[i] += rp.n0[i][j]*( sp[j].e +sp[j].es )
                -N[j]*sn0[i]*(sp[j].Cvt+sp[j].Cvr)*Mw0*T;
        for (j=0; j<nre; j++)
            atau[j][i] = dqa[j][i];
    }
    for (i=0; i<nv; i++) {
        thvT = sp[idxv1[i]].thv[idxv2[i]]/T;
        devT = q[nre+i]*thvT/(1-exp(-thvT));
        devp[i] = 1./p; devr[i] = -1./rhot;
        for (j=0; j<nre; j++) {
            devp[i] -= Mw0*snn0[j]*dap[j];
            devr[i] -= Mw0*snn0[j]*dar[j];
        }
        devp[i] += devT; devr[i] += devT;
        dqpE[nre+i] = devp[i];
        dqrE[nre+i] = devr[i];
        dhdq[nre+i] = sp[idxv1[i]].Mw*N[idxv1[i]];
        sNtvs = 0.;
        for (j=0; j<ns; j++) {
            if (stauv==1) {
                ata = 36.5;
                bta = -0.0193;
            } else {
                redM = sp[idxv1[i]].Mw*sp[j].Mw
                    / ( sp[idxv1[i]].Mw*sp[j].Mw );
                ata = 0.0367*sqrt(redM)
                    *pow(sp[idxv1[i]].thv[idxv2[i]],4./3.);
                bta = 0.08435*pow( redM,0.25 );
            }
            tauvs = (1./(p*9.86923e-6))
                *exp(ata*(pow(T,-1./3.)-bta) -18.42 );
            sNtvs += N[j]/tauvs;
        }
        tauv[i] = 1./(Mw0*sNtvs);
        atau[nre+i][nre+i] = 1./tauv[i];
        printf("tau-v[i]=%13.4e\n",tauv[i]);
    }
    return *this;
}

FP_dat& FP_dat::CxfrmN() {
    int i;
    double iMw0;
    iMw0 = 0.;
    for (i=0; i<ns; i++)
        iMw0 += N[i];
    Mw0 = 1./iMw0;
    for (i=0; i<ns; i++) {
        C[i] = sp[i].Mw*N[i];
        x[i] = Mw0*N[i];
        sp[i].rhs = rhot*C[i];
    }
    return *this;
}

FP_dat& FP_dat::Nevm(const RP_dat& rp) {
    int i,j,nr;
    nr = q.size() -nv;
    for (j=0; j<ns; j++) {
        N[j] = N0[j];
        for (i=0; i<nr; i++)
            N[j] += q[i]*rp.n0[i][j];
    }
    for (i=0; i<nv; i++)
        sp[idxv1[i]].evm[idxv2[i]] = q[nre+i];
    return *this;
}

vector<double> FP_dat::InitN0(int is, const vector<double>& COi) {
    vector<double> Not,CO;
    double minN = 1.e-10;
    double sc,npM;
    int i;
    if (COi.size()<ns)
        printf("INPUT CO size is not appropriate!\n");
    Not.resize(ns); CO.resize(CO.size());
    sc = 0.;
    for (i=0; i<min(ns,(int)COi.size()); i++) sc += COi[i];
    for (i=0; i<min(ns,(int)COi.size()); i++) CO[i] = COi[i]/sc;
    if (COi.size()<ns)
        for (i=0; i<ns; i++) CO[i] = 1.e-30;
    if (is==0) {
        npM = 0.;
        for (i=0; i<ns-1; i++) {
            Not[i] = CO[i]/sp[i].Mw;
            if (minN>Not[i]) Not[i] = minN;
            npM += Not[i];
        }
        Mw0 = 1./npM;
    } else {
        Mw0 = 0.;
        for (i=0; i<ns; i++) Mw0 += COi[i]*sp[i].Mw;
        for (i=0; i<ns; i++) {
            Not[i] = COi[i]/Mw0;
            if (minN>Not[i]) Not[i] = minN;
        }
        if (minN>Not[ns-1]) Not[ns-1] = minN;
        return Not;
    }
}

FP_dat& FP_dat::sprg(const RP_dat &rp, double w) {
    double af0;
    vector<vector<complex<double>>> iwIAa,iwIAai,iwIAi,B
        ,dhdqB,Mnum,Mden;
    complex<double> Num1,Den1,D,cdet;
    int i,j;
    af0 = sqrt(afz2);
    iwIAa.resize(rp.nre);
    for (i=0; i<rp.nre; i++) {
        iwIAa[i].resize(rp.nre);
        for (j=0; j<rp.nre; j++)
            if (i==j)
                iwIAa[i][j] = c.i*w +dqa[i][j];
            else
                iwIAa[i][j] = dqa[i][j];
    }
    InvMtx(iwIAa,iwIAai,cdet);
    printf("det= %e + (%e)i, ",cdet.real(),cdet.imag());
    iwIAi.resize(nq);
    for (i=0; i<nq; i++) {
        iwIAi[i].resize(nq);
        for (j=0; j<nq; j++) {
            iwIAi[i][j] = 0.;
            if ( (i<rp.nre)&&(j<rp.nre) )
                iwIAi[i][j] = iwIAai[i][j];
        }
    }
}

```

```

        else if (i==j)
            iwIAi[i][j] = 1./(c_i*w
                +1./tauv[i-rp.nre]);
    }
B = iwIAi*((complex<double>)1.)*atau;
dhdqB = (cd_1*Tmat(dhdq))*B;

Mnum = dhdqB*(cd_1*VtoM(dqdpE));
Mden = dhdqB*(cd_1*VtoM(dqdrE));
Num1 = -w*w*( 1./afz2 -(1./dhdr)*Mnum[0][0] );
Den1 = 1. +(1./dhdr)*Mden[0][0];
D = sqrt( Num1/Den1 );
Atper1 = 2.*pi_rC*D.real()/D.imag();
RtoAf = w/(af0*D.imag());
return *this;
}

```


5. Input file for equilibrium properties : gasesEqProp.dat

24													
name	Mol.Weight	#	SxTHERT	SHAJP(J/mol)	A_visc	B_visc	C_visc						
N2	28.01600000	2	5.79	0.000000E+00	0.0268142	0.3177838	-11.3155513						
		1	1	3353.2400									
		4	1	0.000000E+00	6.014654E+05	7.136084E+05	7.342244E+05						
D2	32.00000000	2	4.16	0.000000E+00	0.044929	-0.0826158	-9.2019475						
		1	1	2238.9700									
		5	3	0.000000E+00	9.224688E+04	1.579169E+05	4.319868E+05						
AR	39.94400000	1	0.00	0.000000E+00	-0.029568	0.244716	-10.638224						
		0	1	0.0000									
		3	1	0.000000E+00	1.114761E+06	1.122024E+06	-12.4327495						
N	14.00800000	1	0.00	4.713043E+05	0.0115572	0.6031679	-11.6031403						
		0	1	0.0000									
		5	4	0.000000E+00	2.301212E+05	4.230753E+05	3.451566E+05						
O	16.00000000	1	0.00	2.467723E+05	0.0203144	0.4294404	-11.6031403						
		0	1	0.0000									
		6	5	0.000000E+00	1.903039E+03	2.716630E+03	1.899104E+05						
NO	30.00800000	2	2.45	8.990272E+04	0.0436378	-0.0335511	-9.576743						
		1	1	2699.1800									
		3	4	0.000000E+00	5.261802E+05	5.495506E+05	-12.7378						
C	12.01100000	1	0.00	7.115781E+05	-0.0083285	0.770324	-12.7378						
		0	1	0.0000									
		6	1	0.000000E+00	1.961851E+02	5.203692E+02	1.219422E+05						
CO2	44.01100000	2	1.13	-3.933329E+05	-0.01952739	1.047818	-14.32212						
		3	2	960.1000	1992.5200	3380.1500							
		1	1	0.000000E+00									
CO	28.01100000	2	2.78	-1.138559E+05	-0.01952739	1.013295	-13.97873						
		1	1	3082.0000									
		5	1	0.000000E+00	5.824246E+05	6.687160E+05	7.452570E+05						
H2	2.01600000	2	175.09	0.000000E+00	-8.3346e-3	0.7815380	-13.5351000						
		1	1	6100.0000									
		4	1	0.000000E+00	1.096736E+06	1.196150E+06	1.351651E+06						
H	1.00800000	1	0.00	2.118807E+05	-8.3912e-3	0.7743270	-13.6653000						
		0	1	0.0000									
		4	1	0.000000E+00	9.839277E+05	1.166148E+06	1.229918E+06						
CH	13.01894000	2	20.80	5.906830E+05	0	0	0						
		1	1	4116.9353									
		6	2	0.000000E+00	2.141299E+02	5.383153E+04	2.769333E+05						
CH2	14.02688000	3	26.42	3.859200E+05	0	0	0						
		3	1	4250.1817	1519.3607	4493.3367							
		1	3	0.000000E+00									
CH2a	14.02688000	3	18.32	3.859200E+05	0	0	0						
		3	1	4353.7742	2011.4264	4422.8361							
		2	0	0.000000E+00	3.110266E+04								
CH3	15.03482000	4	24.66	1.490310E+05	0	0	0						
		4	1	4319.2433	834.4974	4581.1028	1989.8446						
		2	2	0.000000E+00	5.527302E+05								
CH4	16.04276000	5	27.13	-6.691100E+04	0	0	0						
		4	1	4196.2269	2207.1017	4343.2711	1879.0579						
		1	1	0.000000E+00									
C2H	25.02994000	2	2.122	4.739000E+05	0	0	0						
		3	1	2762.4741	920.8247	4632.8992							
		2	2	0.000000E+00	1.076631E+05								
C2H2	26.03788000	2	3.386	2.357550E+05	0	0	0						
		5	1	4854.0410	2839.8809	4721.9602	879.9631						
		1	1	0.000000E+00									
C2H4	28.05376000	6	3.937	6.098600E+04	0	0	0						
		12	1	4354.3497	4463.8416	4468.1579	2335.0100						
		1	1	1365.8420	4300.1074	1471.8807	1356.7776						
		1	1	0.000000E+00									
ND+	30.00745153	2	2.88	9.850914E+05	0	0	0						
		1	1	3372.9500									
		5	1	0.000000E+00	4.823612E+05	7.073796E+05	8.737522E+05						
CD+	28.01045153	2	2.84	1.238976E+06	0	0	0						
		1	1	3082.0000									
		3	2	0.000000E+00	2.480197E+05	5.488001E+05							
O+	15.99945153	1	0.00	1.561248E+06	0.0203144	0.4294404	-11.6031403						
		0	1	0.0000									
		4	4	0.000000E+00	3.208276E+05	3.210788E+05	4.843202E+05						
C+	12.01045153	1	0.54	1.799277E+06	-0.0083285	0.770324	-12.7378						
		0	1	0.0000									
		5	2	0.000000E+00	7.656001E+02	5.143899E+05	5.146486E+05						
E-	0.00054847	1	0.00	0.000000E+00	0	0	0						
		0	1	0.0000									
		1	2	0.000000E+00									

6.Input file for reaction properties : air.dat

```

6      6
N2     O2     AR     N     O     NO     N2     O2     AR     N     O     NO
1      0      0      0      0      0      0      0      0      2      0      0
3
0      2.30e+23     -3.5     113260.
3      8.50e+19     -2.5     113260.
-1     9.90e+14     -1.5     113260.
0      1      0      0      0      0      0      0      0      0      2      0
3
1      3.60e+15     -1.5     59390.
4      2.10e+12     -0.5     59390.
-1     1.20e+15     -1.5     59390.
0      0      0      0      0      1      0      0      0      1      1      0
2
5      5.20e+15     -1.5     75500.
-1     5.20e+15     -1.5     75500.
0      1      0      1      0      0      0      0      0      0      1      1
1
-1     1.00e+6      0.5     3625.
1      0      0      0      1      0      0      0      0      1      0      1
1
-1     5.00e+7      0.0     38020.
1      1      0      0      0      0      0      0      0      0      0      2
1
-1     9.10e+18     -2.5     65010.
3
1.     0.     0.
0.     1.     0.
0.     0.     1.
0.     1.     -1.
1.     0.     -1.
1.     1.     -2.

```