

Higher-order defect-mode laser in an optically thick photonic crystal slab

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Received October 26, 2012; revised November 29, 2012; accepted December 3, 2012;
posted December 6, 2012 (Doc. ID 178784); published January 7, 2013

The use of an optically thick slab may provide versatile solutions for the realization of a current injection-type laser using photonic crystals. Here, we show that a transversely higher-order defect mode can be designed to be confined by a photonic bandgap in such a thick slab. Using simulations, we show that a high Q of $>10^5$ is possible from a finely tuned second-order hexapole mode (2h). Experimentally, we achieve optically pumped pulsed lasing at 1347 nm from the 2h with a peak threshold pump power of 88 μ W. © 2013 Optical Society of America

OCIS codes: 230.5298, 250.5960.

Two-dimensional (2-D) photonic crystal (PhC) slab structures have, so far, been in the form of a thin dielectric slab whose thickness T is often chosen to be ~ 200 nm for an operational wavelength of ~ 1.3 μ m. This thickness consideration is to maximize the size of the photonic bandgap (PBG) in the in-plane direction (x - y plane) [1], which has unfortunately placed a severe constraint on the design of a current-injection type laser. Pulsed lasing operation has been demonstrated using a vertically varying p - i - n doping structure within the thin PhC slab, for which a submicrometer-size dielectric post placed directly underneath the laser cavity serves as a current path [2]. Recent efforts have moved toward a *laterally* varying p - i - n structure, and a few successful results were already reported by groups in both Stanford [3] and Nippon Telegraph and Telephone Corporation (NTT) [4]. However, there are still favorable reasons for using a vertically varying doped structure because such a design allows a monolithic growth of all of the epitaxial layers that are almost free of crystal defects.

Recently, we have shown that even a very thick slab can support sufficiently high- Q (few thousands) cavity modes for lasing [5]. In our previous result, however, the dipole mode formed in a triangular-lattice air-hole PhC slab was emitting more photons into the in-plane directions than into the vertical direction (z) for efficient photon emission and collection. Moreover, Q could not exceed 3000 with $T = 606$ nm. It would seem, at first, that we have no other options for further improvement in Q because the poor horizontal confinement appears inevitable due to the absence of a PBG. It is our purpose in this Letter to rebut this first intuition and show that the thick slab can be used to achieve an efficient vertical emitter with a surprisingly high Q of over 10^5 .

To start, we perform numerical simulations using both the plane-wave-expansion method [6] and the finite-difference time-domain (FDTD) method to investigate how a PBG evolves as we change the air-hole radius (r) and the slab thickness (T) [Fig. 1(a)]. Note that r and T are represented in the unit of the lattice constant (a). In the case of a triangular-lattice air-hole PhC, $\{r = 0.40a, T = 0.6a\}$ gives the widest gap centered at $\omega_c \approx 0.38$, which agrees with earlier work by Johnson *et al.* [1]. Also

note that there exists a broad region of $\{r, T\}$ that gives a wide gap-to-midgap ratio [1] $\widetilde{\Delta\omega} > 30\%$. This is why r and T are often chosen to be $\sim 0.35a$ and $0.5a$, respectively.

We also find that a tiny PBG (usually $\widetilde{\Delta\omega} \sim 1\%$) exists up to $T = 1.25a$.

The dipole mode discussed in our previous work [5] ($T = 1.86a$) is marked as “1d” in the gap map. Now, we pose the question of whether we can design a certain resonant mode emitting at ~ 1.3 μ m that is confined by a PBG in a slab with $T = 606$ nm. From the gap map diagram, the only possibility appears to be increasing a in order to bring down $T(a)$ below $1.25a$. However, keeping the same 1d mode, larger a usually results in longer λ because $\omega = a/\lambda$ is rather fixed by the in-plane modal structure of a resonant mode [7]. Therefore, we should look instead into other resonant modes that do not resemble the dipole mode.

It is well known that even a single-defect resonator supports multiple resonances such as the quadrupole, the hexapole, and the monopole modes [8]. These higher-order modes are pulled down from the conduction-band edge of the photonic band structure [7]. Further tuning the defect region can get more higher-order modes pulled down into the gap. One possible route from the (first-order) dipole mode (1d) to the second-order hexapole mode (“2h”) is drawn by an arrow in the gap map diagram. The 2h mode is designed to be resonant at a wavelength close to that of 1d (Structural parameters for this second hexapole mode are as follows: $K_1 = 1.07a$, $K_2 = 0.99a$, $R_1 = 0.28a$, $R_{\text{bg}} = 0.46a$, $R = 0.46a$. For definitions of these parameters, see Fig. 2.) even though it has quite a large a of 500 nm (thus, $T \approx 1.21a$). As a quantitative measure showing how well the PhC layers work as a mirror, we calculate the vertical extraction efficiency η_{vert} defined by $\eta_{\text{vert}} \equiv (1/Q_{\text{vert}})/(1/Q_{\text{horz}} + 1/Q_{\text{vert}}) = (1/Q_{\text{vert}})/(1/Q_{\text{tot}})$ [5]. We find that η_{vert} of 2h shown in Fig. 1(c) is 0.954 ($Q_{\text{horz}} = 3.3 \times 10^5$) with the same number of air-hole barriers shown in Fig. 2(b). We believe this η_{vert} (or Q_{horz}) has not yet been saturated due to the small gap size, expecting further improvement by increasing the number of barriers. Probably, in applying the idea of a higher-order resonant mode, T of 606 nm would be

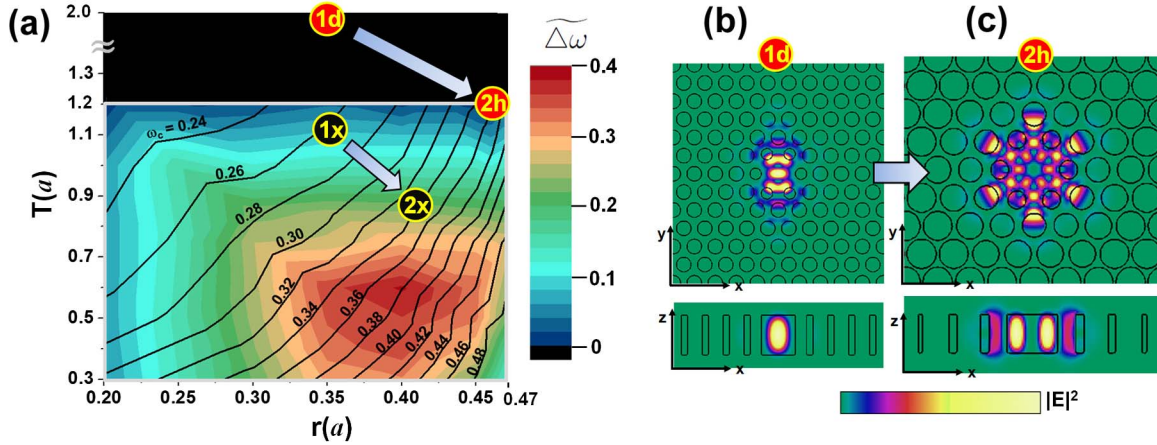


Fig. 1. (Color online) (a) 2-D map of a PBG for a triangular-lattice air-hole (radius = r) PhC in a dielectric slab ($n_{\text{slab}} = 3.4$) with a thickness of T . The 2-D color scale map represents the size of the PBG in terms of the gap-to-midgap ratio defined by $\widetilde{\Delta\omega} \equiv \Delta\omega/\omega_c$, where ω_c is the center frequency of a PBG. The contour curves of ω_c are overlaid on the 2-D map. Note that throughout the Letter, all frequencies are normalized by $2\pi c/a$; hence $\omega = a/\lambda$ (dimensionless). (b) First-order dipole mode (1d) [$Q = 2600$ and $V = 0.82(\lambda/n_{\text{slab}})^3$] oscillating at $\lambda = 1341$ nm with $a = 325$ nm. (c) Second-order hexapole mode (2h) [$Q = 15,200$ and $V = 2.23(\lambda/n_{\text{slab}})^3$] oscillating at $\lambda = 1365$ nm with $a = 500$ nm. Both modes are formed in a slab with $T = 606$ nm.

the upper limit for $\lambda \sim 1300$ nm, as 2h can only be made barely located at the top-right corner of the gap map diagram. We would like to note that the same strategy can be applied more effectively to the case of an intermediate thickness range of $400 \text{ nm} < T < 600$ nm. Imagine a first-order resonant mode (“1x”) oscillating at $\omega \approx 0.26$ within a slab with $T = 1.1a$. At this region, $\widetilde{\Delta\omega}$ is only about 5%. We can bring it down deep into the bandgap by utilizing its second-order resonant mode (“2x”). If 2x oscillates at $\omega \approx 0.33$, then, without altering λ , 2x can be formed in a slab with $T \approx 0.87a$, at which $\widetilde{\Delta\omega}$ is as large as 20%.

Note that when choosing structural parameters for 2h we intend to obtain higher ω rather than higher Q . This is to minimize $T(a)$ so as to create a PBG. However, 2h requires the large air holes of $R = 0.46a$ to locate its resonance at the center of the tiny bandgap, which is not advantageous for the device’s mechanical robustness. Therefore, we proceed to study if the background air-hole radii (R_{bg}) can be substantially reduced without

sacrificing Q too much. $R_1 = 0.26a$, $K_1 = 1.07a$, and $K_2 = 1.04a$ [See Fig. 2(a)] have been chosen to optimize Q . As a result, ω decreases by about 10% in comparison with the case shown in Fig. 1(c). Several representative cases of fine-tuned air holes are shown in Fig. 2 and Table 1. The outskirts region from R_4 is intended as a mirror. Air-hole radii before and after R_4 are designed to vary gradually to minimize unintentional scattering losses at the crystal dislocations. Because R_1 , K_1 , and K_2 are fixed, all the resonant wavelengths tend to stay near 1323 nm. $a = 450$ nm for all those cases, thus $T = 1.35a$ and there exists no PBG.

Contrary to the initial expectation, Q can be made higher even in the absence of a rigorous PBG. In Case II, we find that Q_{vert} can be greatly improved by more than a factor of 10, and thereby Q_{tot} can reach over 10^5 . It is interesting to observe that, comparing cases I and II, air holes located far from the mode’s energy ($R_{>6}$) can affect Q_{vert} . It should also be noted that just one layer of $R_4 = 0.45a$ effectively blocks the horizontal photon leakage. As we progressively reduce R , both Q_{vert} and Q_{horz} decrease somewhat. However, all cases show quite high $\eta_{\text{vert}} > \sim 0.8$ even in the absence of a PBG, which seems to imply that a careful engineering of the background air holes (such as hole-size chirping) can reduce the coupling loss between the defect mode and the in-plane Bloch modes [9].

In experiment, we intend to fabricate a structurally more robust design similar to case VI rather than the

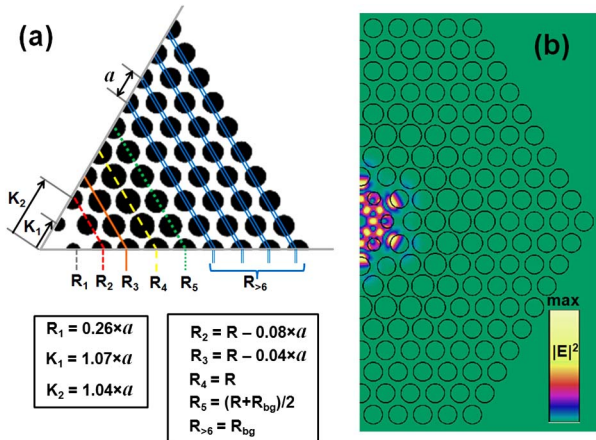


Fig. 2. (Color online) (a) Schematic diagram shows how we finely tune air-hole sizes and locations to optimize Q . (b) Electric-field intensity distribution ($|E|^2$) of the highest- Q mode (case II in Table 1).

Table 1. Examples of the Second-Order Hexapole Mode in a $T = 606$ nm Slab

Case	$R(a)$	$R_{\text{bg}}(a)$	Q_{tot}	Q_{vert}	η_{vert}
I	0.45	0.45	55,400	58,500	0.947
II	0.45	0.38	105,100	146,200	0.719
III	0.44	0.38	50,400	63,900	0.789
IV	0.43	0.38	27,900	34,400	0.811
V	0.42	0.38	17,800	21,800	0.813
VI	0.41	0.38	12,400	15,300	0.807

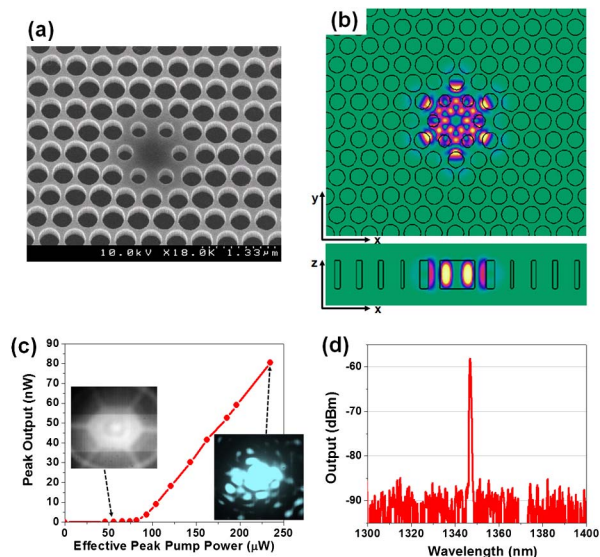


Fig. 3. (Color online) (a) SEM image taken at a tilt of about 10° . Note that $T = 606$ nm. (b) FDTD simulated mode profile. (c) Light-in versus light-out ($L-L$) curve. Insets show near-infrared camera images taken before and after the lasing. (d) Lasing spectrum measured at a peak pump power of $200 \mu\text{W}$.

Q -optimized design of case II. We use the same InGaAsP wafer containing seven InGaAsP quantum wells emitting near 1325 nm used in our previous work [5]. To define high-aspect-ratio air holes, we use chemically assisted ion-beam etching with Ar and Cl_2 [5]. The fabricated devices are optically pumped at room temperature with a 830 nm laser diode driven by a pulse generator at 1 MHz with a duty cycle of 2.5% . A $100\times$ objective lens is used to focus the pump laser on the center of the resonator (pump spot size $\sim 3.5 \mu\text{m}$). The $L-L$ curve in Fig. 3(c) clearly shows a threshold, estimated to be $88 \mu\text{W}$ in terms of peak pump power, where we have assumed about 20% of actual incident pump power is absorbed by the slab. In Fig. 3(d), we verify single-mode lasing operation over a wide spectral range (1300 – 1400 nm) with a side-mode suppression ratio of ~ 30 dB. To confirm if the measured laser peak truly originates from the $2h$ mode, we perform

FDTD simulation using a contour input for actual fabricated air holes from the scanning-electron microscopy (SEM) image [see Fig. 3(b)]. The FDTD expects that the designed $2h$ mode should locate at a wavelength of 1340 nm, which agrees very well with the experimental result. However, the FDTD expects somewhat lower Q of ~ 3000 , which could be due to the slightly broken six-fold symmetry in the six nearest neighboring holes (R_1).

Finally, one feasible design for the realization of a current-injection laser is to insert a thin sacrificial layer in the middle of the thick slab, which is to be wet-chemically removed to form a current aperture. The thick slab enables a mechanically robust double slab in the form of a vertically varying $p-i-n$ structure [10].

This work was supported by DARPA under NACHOS (W911NF-07-1-0277) and by the National Science Foundation under NSF CIAN ERC (EEC-0812072).

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