

## Supplementary Materials

### X-ray Diffraction Samples and Measurements

X-ray diffraction analysis of the Rocknest scoop sample is described in (23); similar analyses were performed for John Klein and Cumberland. John Klein and Cumberland were the first two drill samples collected by *Curiosity*. All scooped or drilled samples pass through the Collection and Handling for In situ Martian Rock Analysis (CHIMRA) sample collection and processing system (10). All powders for X-ray diffraction are processed through a 150- $\mu\text{m}$  sieve before delivering a portion to the CheMin inlet funnel.

The sieved drill powders were placed into sample cells with 6  $\mu\text{m}$  thick Mylar® windows. Mylar® contributes a minor, broad scattering signature in diffraction patterns that is generally “swamped” by diffraction from the loaded sample. In addition, an aluminized light shield also contributes “peaks” to the observed diffraction patterns. Only  $\sim 10 \text{ mm}^3$  of material is required to fill the active volume of the sample cell, which is a disc-shaped volume 8 mm in diameter and 175  $\mu\text{m}$  thick. A collimated  $\sim 70 \mu\text{m}$  diameter X-ray beam illuminates the center of the sample cell. A piezoelectric vibration system on each cell pair shakes the material during analysis, causing grains in the cell to pass through the X-ray beam in random orientations.

CheMin measures XRD and XRF data simultaneously using Co radiation in transmission geometry (11). The instrument operates in single-photon counting mode so that between each readout the majority of CCD pixels are struck by either a single X-ray photon or by no photons. In this way, the system can determine both the energy of the photons striking the CCD (XRF) and the two-dimensional (2-D) position of each photon (XRD). The energy and positional information of detected photons in each frame are summed over repeated 10-sec measurements into a “minor frame” of 30 min of data (180 frames). The 2-D distribution of Co  $K\alpha$  X-ray intensity represents the XRD pattern of the sample. Circumferential integration of these rings, corrected for arc length, produces a conventional 1-D XRD pattern. For conversion of the 2-D CCD pattern to a 1-D pattern we have used FilmScan® software from Materials Data, Inc.

CheMin generally operates for only a few hours each night, when the CCD can be cooled to its lowest temperature, collecting as many minor frames as possible for the available analysis time, usually five to seven per night. XRD data were acquired over multiple nights for the John Klein and Cumberland drill samples to provide acceptable counting statistics. Total data collection times were 33.9 hr for John Klein and 20.2 hr for Cumberland. The data for individual minor frames and for each night’s analysis were examined separately, and there was no evidence of any changes in instrumental parameters as a function of time over the duration of these analyses. Before sample delivery and analysis, the empty cell was analyzed to confirm that it was indeed empty before receiving the sample. The flight instrument was calibrated on the ground before flight using a quartz-beryl standard, and measurement of this standard on Mars showed no changes in instrument geometry or dimensions.

**Crystalline Components.** All XRD data were first evaluated by comparisons and searches of the International Centre for Diffraction Data (ICDD) Powder Diffraction File using Bruker AXS DIFFRAC.EVA (©2000, Bruker AXS, Karlsruhe, Germany) and MDI Jade® (Materials Data Incorporated, Livermore, CA) software packages, which revealed the presence of plagioclase, forsterite, magnetite, augite, pigeonite, orthopyroxene, akaganeite, bassanite, and anhydrite. John

Klein was the first drill sample analyzed and there was immediate evidence of a phyllosilicate, represented by a broad diffraction peak at  $8.5\text{-}11^\circ 2\theta$  Co  $K\alpha$ . The comparatively large instrumental peak width for the CheMin instrument ( $\sim 0.3^\circ 2\theta$  full-width at half-maximum at  $25^\circ 2\theta$ ) limits our ability to determine accurately the presence of some minor crystalline phases ( $< 2$  wt. %). The data were analyzed further via Rietveld methods, using Topas ( $^\circ 2000$ , Bruker AXS, Karlsruhe, Germany). We used the fundamental-parameters approach within Topas, along with additional convolutions, to model the experimental profiles. We also used an emission spectrum including Co  $K\alpha$  with a refinable Co  $K\beta$  component. The Rietveld method involves constructing a model consisting of the crystal structures of all component phases, and the differences between the observed and simulated diffraction patterns are minimized by varying components of the model, including scale factors (related to phase abundance), unit-cell parameters, and crystallite-size and strain broadening parameters for each phase. Atomic positions and site occupancies were generally not varied, although octahedral site occupancies were varied for forsteritic olivine, augite, and pigeonite, and Na-Ca occupancies were varied for the plagioclase component. This method thus provides information on all well-ordered phases (*i.e.*, crystalline), but it is not directly applicable to disordered phases such as clay minerals or amorphous components.

**Clay Mineral and Amorphous-component Abundances.** Neither smectites nor X-ray amorphous samples are amenable to Rietveld analysis. Instead, the FULLPAT full-pattern fitting method was used (22). FULLPAT operates on the principle that diffraction and scattering patterns for all phases in a sample are additive. By fitting full diffraction patterns, including the background, which contains important information on sample composition and matrix effects, explicit analysis of amorphous or partially ordered materials can be accomplished if the amorphous/disordered phases are included in the analyses as distinct phases. Thus, FULLPAT allows direct analysis of the abundance of clay minerals and amorphous components, rather than determining them as the difference from 100% in an internal-standard quantitative analysis. Like all full-pattern fitting methods, accurate analysis requires representative standards or structure models. A large variety of pure mineral standards, disordered materials (allophanes, ferrihydrite, aluminosilicate gels), and a synthetic glass of Gusev basaltic composition were measured. Each of these was run as a pure phase and was also mixed with a beryl standard in 50:50 wt. ratio to determine a Reference Intensity Ratio (RIR) for subsequent use in FULLPAT. All standard data were measured on a CheMin IV instrument at the NASA Johnson Space Center; the CheMin IV instrument geometry is very similar to the instrument on MSL and is considered a good proxy for the flight instrument. Peak areas for each phase were compared against the intensity of the beryl 100 peak, and the measured beryl RIR of 1.70 relative to corundum (measured on a laboratory instrument) was used to convert the RIR(beryl) to the conventional RIR(corundum) value. During FULLPAT analysis, the intensity of each standard pattern was normalized to the intensity of a pure pattern of corundum used as datum. Thus, using the corundum datum 113 reflection intensity and the measured RIR for each standard phase, the pattern of each disordered phase could be normalized to the appropriate overall intensity based on its measured intensity area used for the RIR determination.

Because few standard data for pure phases have been measured on the CheMin flight instrument, an alternate method for calculating standard data representative of the MSL CheMin instrument was also employed. This process involved first determining instrumental peak shapes and widths as a function of  $2\theta$  using the beryl standard measured on the MSL instrument. We

then calculated diffraction patterns for each standard using the appropriate crystal structure information and the instrumental profiles determined above for Co K $\alpha$  radiation. The final step in calculation of standard data for FULLPAT is to normalize the intensity of the calculated pattern to the corundum datum pattern using the calculated RIR as outlined above. The scaled measured and calculated library patterns, for both ordered and amorphous phases, were then used with FULLPAT.

### **Estimating Compositions and Abundances of Clay Minerals and Amorphous Components from XRD and APXS data.**

The relative proportions of crystalline and amorphous plus smectite components and their respective bulk compositions were estimated by combining the APXS chemical compositions of the mudstone samples, and the chemical composition of crystalline components including Fe oxidation state (from stoichiometry or XRD unit-cell parameters) weighted by their CheMin XRD abundance (phases from plagioclase to pyrrhotite in Table 1 in this paper). To estimate the chemical composition of the amorphous material relative to that of the total amorphous plus smectite component, the chemical compositions (H<sub>2</sub>O/OH-free basis) of two saponites were assumed for the trioctahedral smectite: griffithite and Clay Minerals Society saponite SapCa-1. Among the clay minerals analyzed in the laboratory, griffithite has an 02 $l$  diffraction band similar to the smectite component of both John Klein and Cumberland. The proportion of each smectite, calculated by increasing the smectite concentration until the MgO concentration in the amorphous component was ~0 wt.%, is an upper limit for its concentration.

Table S-1. Chemical composition of John Klein drill fines from APXS and CheMin measurements, calculated chemical compositions of crystalline and combined amorphous and smectite components, and calculated chemical compositions of amorphous components assuming griffithite and saponite SapCa-1 as trioctahedral smectites.

(wt.%)	APXS		XRD	Smectite+	Griffithite Model <sup>e</sup>		SapCa-1 Model <sup>f</sup>	
	APXS <sup>a</sup>	+CHMN <sup>b</sup>	Crystalline <sup>c</sup>	Amorphous <sup>d</sup>	Griffithite	Amorphous	SapCa-1	Amorphous
SiO <sub>2</sub>	42.07	42.03	42.65	41.76	49.71	32.94	57.60	30.10
TiO <sub>2</sub>	0.97	0.97	-0.02	1.41	-0.01	2.98	0.56	2.03
Al <sub>2</sub> O <sub>3</sub>	8.67	8.66	12.48	6.97	9.52	4.14	4.11	9.08
Cr <sub>2</sub> O <sub>3</sub>	0.42	0.42	-0.01	0.61	-0.01	1.30	-0.02	1.07
FeO+Fe <sub>2</sub> O <sub>3</sub>	19.86	13.51	-0.23	19.59	16.48	23.04	0.74	33.46
Fe-Cryst	0.00	0.47	1.51	0.00	0.00	0.01	0.00	0.01
FeO-Cryst	0.00	3.24	10.53	0.00	0.00	0.00	0.00	0.00
Fe <sub>2</sub> O <sub>3</sub> -Cryst	0.00	2.06	6.71	0.00	0.00	0.00	0.00	0.00
Fe <sub>2</sub> O <sub>3</sub> -npOx	0.00	0.58	1.87	0.00	0.00	0.00	0.00	0.00
MnO	0.27	0.27	0.00	0.39	0.07	0.75	0.03	0.66
MgO	9.06	9.05	4.88	10.90	20.66	0.07	25.70	0.01
CaO	7.76	7.75	9.47	6.99	2.83	11.61	7.72	6.46
Na <sub>2</sub> O	3.01	2.90	2.98	2.86	0.05	5.98	1.75	3.68
Na-Cryst	0.00	0.04	0.13	0.00	0.00	0.00	0.00	0.00
K <sub>2</sub> O	0.57	0.57	0.30	0.69	0.01	1.44	0.87	0.56
P <sub>2</sub> O <sub>5</sub>	0.93	0.93	-0.02	1.35	-0.02	2.87	0.09	2.28
SO <sub>3</sub>	5.61	3.83	1.07	5.05	-0.09	10.76	0.07	8.72
S-Cryst	0.00	0.33	1.07	0.00	0.00	0.01	0.00	0.01
SO <sub>3</sub> -Cryst	0.00	0.95	3.10	0.00	0.00	-0.01	0.00	-0.01
Cl	0.56	0.53	0.33	0.62	-0.01	1.31	-0.02	1.08
H <sub>2</sub> O-Cyst	0.00	0.12	0.40	0.00	0.00	-0.01	0.00	0.00
Sum	99.76	99.20	99.20	99.20	99.19	99.19	99.20	99.19
Relative to Whole Sample			30.7	69.3	36.4	32.8	29.4	39.9

<sup>a</sup>Composition of drill fines. <sup>b</sup>Composition of drill fines modified according to chemical composition of XRD crystalline phases (excluding smectite). <sup>c</sup>Composition of XRD crystalline component calculated from compositions of individual crystalline components and their relative proportions from Table 1. <sup>d</sup>Composition of amorphous plus smectite component. Cr<sub>2</sub>O<sub>3</sub>, MnO, and P<sub>2</sub>O<sub>5</sub> were modeled with the amorphous component. <sup>e</sup>Composition of griffithite (H<sub>2</sub>O/OH-free basis) and the amorphous phase calculated assuming griffithite is the smectite and MgO ~0 wt.% in the amorphous phase. <sup>f</sup>Composition of SapCa-1 (H<sub>2</sub>O/OH-free basis) and the amorphous phase calculated assuming SapCa-1 is the smectite and MgO ~0 wt.% in the amorphous phase.

Table S-2. Chemical composition of Cumberland drill fines from APXS and CheMin measurements, calculated chemical compositions of crystalline and combined amorphous and smectite components, and calculated chemical compositions of amorphous components assuming griffithite and saponite SapCa-1 as trioctahedral smectites.

(wt.%)	APXS		XRD	Smectite+	Griffithite Model <sup>e</sup>		SapCa-1 Model <sup>f</sup>	
	APXS <sup>a</sup>	+CHMN <sup>b</sup>	Crystalline <sup>c</sup>	Amorphous <sup>d</sup>	Griffithite	Amorphous	SapCa-1	Amorphous
SiO <sub>2</sub>	43.02	43.33	43.72	43.15	49.71	34.98	57.59	31.54
TiO <sub>2</sub>	0.97	0.98	0.57	1.16	-0.01	2.62	0.57	1.64
Al <sub>2</sub> O <sub>3</sub>	8.57	8.63	12.38	6.96	9.53	3.75	4.11	9.25
Cr <sub>2</sub> O <sub>3</sub>	0.43	0.43	-0.01	0.63	-0.01	1.43	-0.02	1.15
FeO+Fe <sub>2</sub> O <sub>3</sub>	22.35	15.27	-0.25	22.21	16.43	29.39	0.66	39.54
Fe-Cryst	0.00	0.38	1.23	0.00	0.00	0.00	0.00	0.00
FeO-Cryst	0.00	3.63	11.74	0.00	0.00	0.00	0.00	0.00
Fe <sub>2</sub> O <sub>3</sub> -Cryst	0.00	2.37	7.65	0.01	0.00	0.02	0.00	0.01
Fe <sub>2</sub> O <sub>3</sub> -npOx	0.00	0.86	2.79	0.00	0.00	0.00	0.00	0.00
MnO	0.27	0.27	0.00	0.40	0.07	0.80	0.03	0.69
MgO	9.41	9.48	5.00	11.48	20.66	0.02	25.70	0.03
CaO	6.29	6.34	7.91	5.63	2.86	9.09	7.75	3.92
Na <sub>2</sub> O	2.98	2.87	2.86	2.97	0.05	6.60	1.74	3.95
Na-Cryst	0.00	0.05	0.08	0.00	0.00	0.00	0.00	0.00
K <sub>2</sub> O	0.50	0.50	0.39	0.55	0.01	1.23	0.88	0.30
P <sub>2</sub> O <sub>5</sub>	0.95	0.96	-0.02	1.39	-0.02	3.16	0.08	2.44
SO <sub>3</sub>	2.57	1.61	0.73	2.00	-0.04	4.55	0.15	3.50
S-Cryst	0.00	0.28	0.74	0.07	0.00	0.17	0.00	0.13
SO <sub>3</sub> -Cryst	0.00	0.28	0.91	0.00	0.00	-0.01	0.00	-0.01
Cl	1.39	0.53	0.32	0.63	-0.01	1.43	-0.02	1.15
H <sub>2</sub> O-Cyst	0.00	0.15	0.49	0.00	0.00	0.00	0.00	0.00
Sum	99.70	99.20	99.24	99.24	99.23	99.23	99.23	99.23
Relative to Whole Sample			30.9	69.1	38.4	30.7	30.8	38.3

<sup>a</sup>Composition of drill fines. <sup>b</sup>Composition of drill fines modified according to chemical composition of XRD crystalline phases (excluding smectite). <sup>c</sup>Composition of XRD crystalline component calculated from compositions of individual crystalline components and their relative proportions from Table 1. <sup>d</sup>Composition of amorphous plus smectite component. Cr<sub>2</sub>O<sub>3</sub>, MnO, and P<sub>2</sub>O<sub>5</sub> are modeled with the amorphous component. <sup>e</sup>Composition of griffithite (H<sub>2</sub>O/OH-free basis) and the amorphous phase calculated assuming griffithite is the smectite and MgO ~0 wt.% in the amorphous phase. <sup>f</sup>Composition of SapCa-1 (H<sub>2</sub>O/OH-free basis) and the amorphous phase calculated assuming SapCa-1 is the smectite and MgO ~0 wt.% in the amorphous phase.

### **Mastcam Hydration Signatures**

The Mastcam instrument is a pair of CCD cameras with fixed focal lengths (34-mm and 100-mm) mounted roughly 2-m above the surface on the rover's mast (14). Each camera obtains images through a Bayer pattern of RGB filters and telecentric microlenses bonded onto the CCD and an 8-position narrowband filter wheel that provides the ability to obtain spectra in 12 unique wavelengths (41). These multispectral observations have been calibrated to radiance ( $I$ ) using pre-flight calibration coefficients, to radiance factor ( $I/F$ , where  $\pi F$  is the solar irradiance at the top of the Martian atmosphere at the time of the observation) using associated observations of the Mastcam calibration target, and to relative reflectance ( $R^*$ ) by dividing  $I/F$  by the cosine of

the solar incidence angle (a similar procedure was used to calibrate Mars Exploration Rover (MER) Pancam images to  $I/F$  and  $R^*$ ; (66, 67)).

Mastcam's longest wavelength filters have some sensitivity to hydrated and/or hydroxylated minerals (27). Specifically, the 1013 nm near-IR filters (referred to as filters L6 and R6 (41)) can detect an absorption due to the  $2\nu_1 + \nu_3$  H<sub>2</sub>O combination band and/or the  $3\nu$  OH overtone when this band minimum occurs longward of roughly 980 nm (*e.g.*, as in water ice, some carbonates, and hydrated sulfates). This narrow hydration band leads to a Mastcam spectral profile that is "flat" in the near-IR, with a sharp downturn at the longest Mastcam wavelength (Fig. 4C) that can be used as a "hydration signature." This profile is distinguishable from spectra of iron-bearing minerals with broad absorptions near 1000-nm, which have an overall negative spectral slope in the near-IR.

The Mastcam hydration signature can be used to remotely identify and map candidate hydrated surface materials in Mastcam near-IR filter images based on the technique developed for the MER Pancam instruments (16, 68) and applied to images acquired along the Spirit (16, 69) and Opportunity (38, 70) traverses. Mastcam spectra exhibiting a hydration signature are defined as those with a spectral slope ( $\Delta R^*/\Delta\lambda$ ) in calibrated  $R^*$  data from 937 to 1013 nm less than  $-4.0 \times 10^{-4} \text{ nm}^{-1}$  and a nearly-flat  $R^*$  spectral profile between 805 and 937 nm (with absolute slope values less than  $2.0 \times 10^{-4} \text{ nm}^{-1}$ ). Slope thresholds were modified slightly from those used for the Pancam hydration signature (16) in order to minimize noise in the Mastcam hydration maps.

It is important to note that the absence of a hydration signature in Mastcam data does not necessarily indicate an absence of hydrated minerals; in the spectra of many H<sub>2</sub>O and/or OH bearing minerals, including phyllosilicates such as saponite (Fig. 4C), the hydration band is centered closer to 950 nm and cannot be detected by Mastcam's longest wavelength filter. Of the various hydration states of Ca-sulfate (gypsum, bassanite and anhydrite), only gypsum (CaSO<sub>4</sub>•2H<sub>2</sub>O) is detectable to Mastcam (and also to MER Pancam (38)). Anhydrite (CaSO<sub>4</sub>) lacks a hydration band, and the weak hydration band in bassanite (CaSO<sub>4</sub>•0.5H<sub>2</sub>O) is centered near 950 nm (Fig. 4C).

## **Mapping of Light-toned Veins and Nodules in Borehole Walls**

Light-toned veins and nodules are visible in both the John Klein and Cumberland borehole walls. Analyses by LIBS and APXS indicate that these late-diagenetic features are associated with Ca-sulfate; in contrast the mudstone matrix is relatively sulfate-poor (8, 19). Sulfate minerals detected by CheMin in the borehole samples include anhydrite and bassanite. An initial ChemCam RMI image taken to support localization of the LIBS analysis spots also showed a striking distribution of veins and nodules in the John Klein drill hole. Subsequently, to better understand the distribution of late-diagenetic veins and nodules, several off-axis images of both boreholes were taken using the Mars Hand Lens Imager (MAHLI) to get relatively complete coverage of the borehole walls to the full visible depth. Some images were acquired at night using MAHLI white light LED illumination. The images were processed to compare the light-toned vein and nodule abundances between John Klein and Cumberland, and to compare sulfate mineral abundances determined by CheMin with mapped abundances of light-toned fillings.

*Drill hole depth and wall visibility* - Both the John Klein and Cumberland holes were drilled to a depth of about 6.5 cm. Autofocused MAHLI image sub-frames covering only the floor of each hole—acquired shortly after drilling was completed on the same sol that the rock was drilled—provided a measure of the distance between the camera lens and the bottom of the hole. Similar autofocused sub-frames acquired outside the hole permitted subtraction of one from the other to estimate hole depth. In both cases, the hole was measured to be about  $3.2 \pm 0.3$  cm deep. While the drill penetrated to 6.5 cm, drill cuttings/debris filled the lower half of each after the drill bit was withdrawn. These ranges, relative to the MAHLI lens, were estimated from its focus motor count position ( $m$ ), which, when the dust cover is open and the range is between 2.1 and 210 cm, relates to range ( $r$ , in cm) between lens and target by  $r = ((0.576786m^{-1}) + (-11.8479) + (2.80153 \times 10^{-3}m) + (-2.266488 \times 10^{-7}m^2) + (6.26666 \times 10^{-12}m^3))^{-1}$ . Thus, for the drill hole wall analysis presented here, only half of the depth and half of the surface area of each wall was observed.

*Processing* - Of the focus stack images acquired at each drill hole, those that were in best focus on the drill hole walls were chosen to accurately represent the entire surface area of the drill hole. Both the John Klein and Cumberland drill holes have MAHLI images from four map directions (approximately S, W, N, E). Some of the MAHLI nighttime LED-illuminated images show more detail of the vein material than do the day, solar-illuminated, images, such as the W, N and E images for Cumberland. Images with the least compression and best focus and contrast were selected and each was cropped in Adobe Photoshop© to 1903 pixels wide and 1847 pixels high, or 6.343 inches wide and 6.157 inches high, at 300 dpi. The width is slightly larger than the height due to the ellipsoid shape of the drill hole as viewed from off-axis angles. A master image was created to hold all the images. The master image is 3805 pixels wide and 3693 pixels high, or 25.543 inches wide and 24.597 inches high, at 300 dpi. Drill hole images were aligned from left to right in order S, W, N, E with the long axis of the drill hole ellipse oriented left-right. Some of the images were tilted and/or had different image scales. In order to correct this, one drill hole image was selected to be the template orientation (long axis left-right) and size. A new layer was created so that an ellipse template could be created to correctly align and size the other images. In the new layer the elliptical marquee tool was used to trace out an ellipse that exactly fit the image that was selected as the base image. That layer was copied and pasted to cover all four images. Each drill hole image was then aligned with the transformation tool to best fit the

ellipse template and the opacity of the ellipse templates was adjusted to 50%. The drill hole ellipse template was used as the surface area marker for mapping. Some of the images overlapped, in which case the image with the best representation of the vein was used.

Easily identifiable marks in the images were used to end one image and start another, so that the entire surface was represented with no overlap. The ellipses were then cut with the polygonal lasso tool to represent the mapping area. The regular lasso tool was used to remove from the image any drill cuttings or debris visible on the bottom of the drill hole. All four images were then converted to greyscale (second row of images in Figs. S-1 and S-2). The bottom row of images was processed to enhance contrast to better show the veins. Next, the previously created surface area marker layers were copied and placed over the bottom row of high contrast images. These were used to cut out un-mapped areas of the drill holes. Each drill-hole image was cut and copied into a new layer. Surface-area marker layers were processed one at a time by using the color range tool to select light-toned vein material. The vein representation was increased to include different shades by selecting additional vein colors until a good representation of the veins was obtained. The selected area was added or removed with the lasso tool. After this was done, the actual drill hole image was deselected and the surface area marker was selected to create a simple representation of the vein in the mapping area.

The vein-to-total surface area percentage was derived from this final representation. The surface area marker was selected with the magic wand tool and the expanded view of the histogram window. With the full area minus the vein area, the histogram window was refreshed to give a pixel amount. This was repeated for every surface area marker and the results were used to calculate  $\text{vein}/(\text{vein} + \text{surface} - \text{vein}) = \text{percent vein per total surface area}$ .

*Results* - The surface area of vein exposure in Cumberland is ~1.7%, very similar to the total sulfate mineral abundance of 1.5% (bassanite plus anhydrite, based on the abundances in Table 1). The surface area of vein exposure in John Klein is ~5.2%, compared with a total sulfate mineral abundance of 3.6% (bassanite plus anhydrite, based on the abundances in Table 1). The apparent excess of mapped vein area compared to sulfate mineral abundance, notably in the John Klein borehole and sample, could be attributed to several factors, including the generally low grain densities of the Ca-sulfates ( $\rho \sim 2.73$  for bassanite to  $\sim 2.97$  for anhydrite, slightly more than andesine at  $\sim 2.67$  but less than the pyroxenes at  $\sim 3.3$ - $3.7$  and much less than magnetite at  $\sim 5.1$ ). However, the greater contributors to the difference are likely to be the inability to map the full borehole depth because of fill (the upper  $\sim 1.5$  cm of the borehole does not make it into the sample processing system (10)), the unknown bulk densities of both the veins and the matrix, the errors in image analysis and quantitative crystalline XRD, and the errors in estimating abundances of the amorphous and clay mineral components from XRD data. Nevertheless, the mapped vein areas in both boreholes are sufficient to account for all of the sulfates detected by XRD.



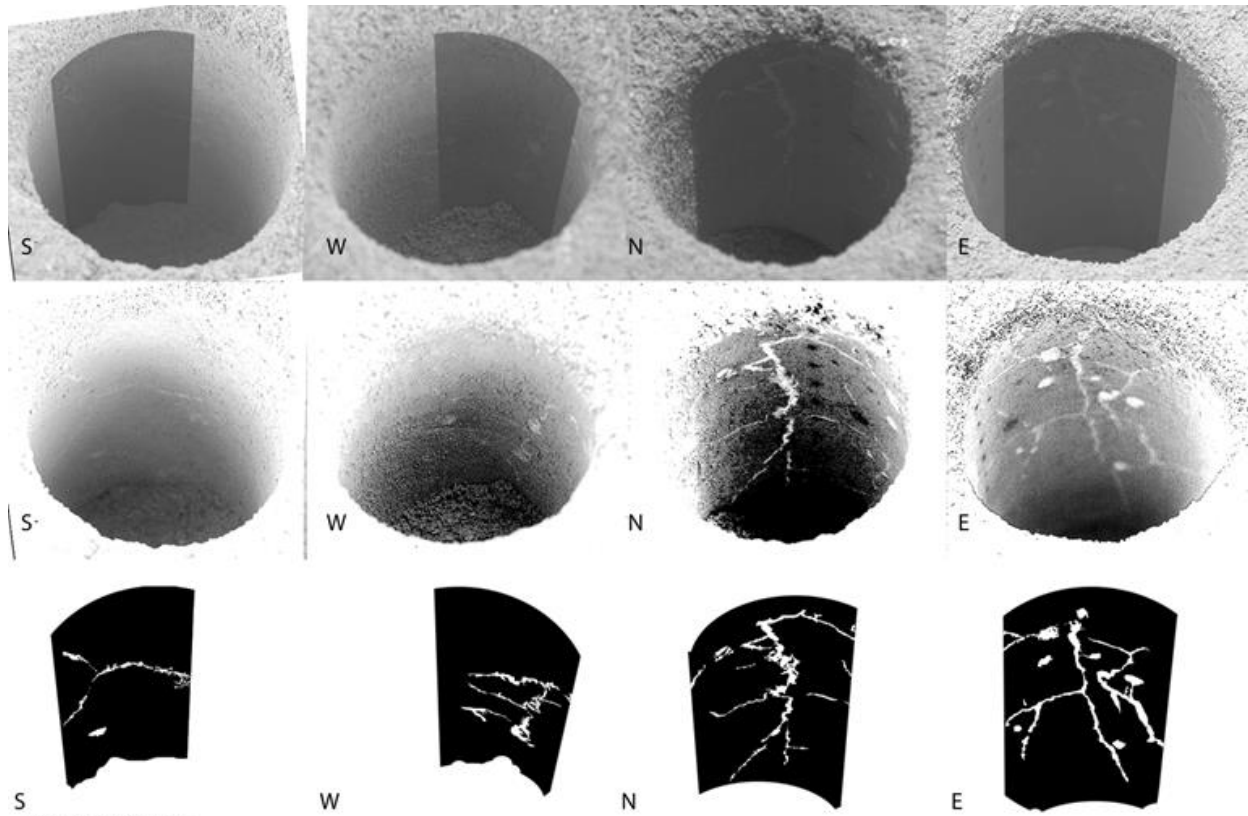


Fig. S-1: Analysis of veins in the John Klein borehole wall. Upper row shows primary images in grayscale with sectors (black) selected for mapping from each MAHLI image (MAHLI images collected on sol 270). Second row from top shows contrast-stretched images (note dark LIBS laser spots in the north image). Bottom row shows images processed to enhance the pixel representation of vein and nodule abundances for quantitative analysis; total vein and nodule area is 5.18% of the borehole wall.

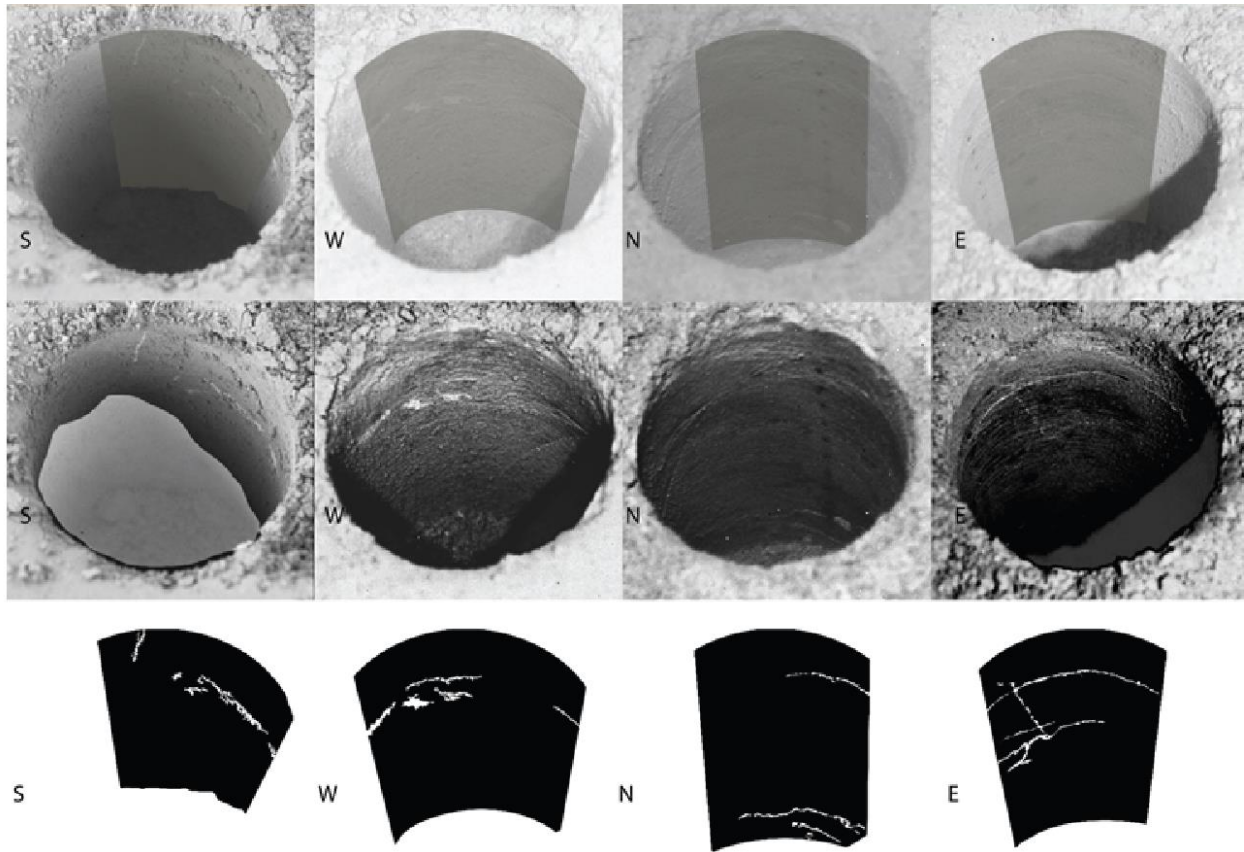


Fig. S-2. Analysis of veins in the Cumberland borehole wall. Upper row shows primary images in grayscale with sectors (black) selected for mapping from each MAHLI image (MAHLI images collected on sol 279). Second row from top shows contrast-stretched images. Bottom row shows images processed for pixel representation of vein and nodule abundances; vein and nodule area is 1.74% of the borehole wall.

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