

UNIVERSAL DISPERSION TABLES

1. LOVE WAVES ACROSS OCEANS AND CONTINENTS ON A SPHERICAL EARTH

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ABSTRACT

The variational approach to surface wave dispersion problems has been largely replaced by the powerful method of Haskell which is exact and particularly convenient for use on digital computers. This paper shows how the two methods may be combined to yield dispersion curves which can be used to interpret data from any layered structure.

A set of graphs and tables is presented which can be used to calculate the dispersion of Love waves in the period range of 4 to 1000 seconds over any spherical earth model. In addition, it is possible to determine by inspection which portion of the earth is contributing to a set of observed dispersion data thereby facilitating the design of an appropriate earth model. These tables can be used to determine how much freedom can be taken with proposed models without violating dispersion data. Application to the inverse problem is immediate.

INTRODUCTION

The calculation of the dispersion relationships for surface waves travelling over realistic spherical earth models is a fundamental seismological problem, arising both in earth structure and in source mechanism studies. It is a routine matter now, for those having access to high speed computers, to calculate the dispersion appropriate for any mode of propagation in a given radially symmetric earth model. Fairly complete fundamental mode solutions have been published for the standard earth models of Gutenberg, Jeffreys, Lehmann, Bullen and Bullard, and minor variations of these velocity and density structures. Comparison of these theoretical calculations with long period observational data show that the Gutenberg or Lehmann velocity structures and the Bullen A density structures provide better agreement than the alternatives, but none of the standard earth models is completely satisfactory. Because of the large number of parameters involved in defining a realistic earth model and the complicated way in which they enter into the dispersion relations, it is difficult to determine which parameters must be changed in order to achieve better agreement between the theory and the data. Even in crustal studies where the total thickness of the earth's crust is the only quantity of interest, good agreement between observed dispersion and a curve from a set of standard curves where only the total crustal thickness is varied is seldom obtained. This indicates that the velocity-density structure of the standard model must also be varied. Published dispersion curves or families of dispersion curves do not permit the estimation of the effect of these variations. A large volume of dispersion curve families would be required to extend the standard curve matching method to include the effects of crustal and mantle layering and different crustal velocity-density structures.

The trial and error method of modifying a test structure and recomputing dispersion is a slowly converging process without clear-cut guide lines as to the necessary modifications. Even with a high-speed digital computer the calculations are so tedious that only the most tentative efforts have been made to modify a trial struc-

ture until there is good agreement between theory and data, thereby taking full advantage of the surface wave information. Even in the few cases where good agreement has been obtained between a theoretical dispersion curve and observed dispersion data, it has not been possible to make any statements concerning the possibility of other structures fitting equally well. It is not usually clear which features of the proposed model are necessary and which may be modified without violating the data. It is particularly difficult for other earth scientists to assess the relative merits of various competing earth models.

The present series of papers was motivated by the above considerations but have been expanded to allow groups without access to electronic computers to conveniently compute dispersion for complicated structures by hand or with a desk calculator.

A method is developed here which is a modification of Jeffreys' (1961) suggested use of Rayleigh's principle. Haskell's matrix method is used to calculate the period relationship (phase velocity vs. period) and the eigenfunctions for a layered medium. The eigenfunction is considered invariant for small changes in the physical parameters in the calculation of variational partial derivatives. The result is a series of tables and graphs which show the effect of every parameter in the waveguide at all periods. This information, along with the theoretical dispersion results for the trial model, permits the rapid calculation of the dispersion for any other model by hand or with a desk calculator.

This initial paper presents results pertinent for fundamental Love wave phase velocity calculations in the period range 4 to 1000 seconds. Later papers will deal with Rayleigh waves, higher modes and free oscillations. The tables presented here can also be used to compute Love wave attenuation simply by allowing the parameter perturbations to become complex.

THEORY

Although the variational method has been used to calculate approximately the steady state response of a radially or vertically inhomogeneous waveguide, the method finds its proper role as a corrective scheme to investigate the effect of small changes in the waveguide. It should be pointed out that even though the differences among the various proposed earth models are physically significant, they are mathematically small, and the restriction to "small changes" is not severe.

The analysis follows that of Jeffreys (1961) generalized to multi-layered media. The following analysis also holds for a spherical body with the change of variables given in Anderson and Toksöz (1963). If the horizontal transverse displacement for a wave travelling in the x -direction is

$$v(z) \cos(\omega t - kx) \quad (1)$$

the average values of the kinetic energy, T , and the elastic potential energy, V , are

$$4T = \int \rho \omega^2 v^2 dz, \quad 4V = \int \mu(k^2 v^2 + v'^2) dz \quad (2)$$

where the integration extends over the entire depth of the waveguide and the prime denotes differentiation with respect to the depth variable z .

Since the kinetic energy and the potential energy, averaged over a cycle, are equal

$$\omega^2 I_0 = k^2 I_1 + I_2 \quad (3)$$

where

$$\begin{aligned} I_0 &= \int \rho v^2 dz \\ I_1 &= \int \mu v^2 dz \\ I_2 &= \int \mu v'^2 dz \end{aligned} \quad (4)$$

The dispersion relation $\omega = \omega(k)$ for the structure being studied can be obtained by a variety of techniques including numerical integration of the equations of motion, a variational technique or the Thomson-Haskell matrix method. The latter is particularly convenient for use on computers and has the additional advantage, for the problem at hand, of yielding closed form expressions for the above integrals. The theory of the matrix method applied to a variety of surface wave problems is treated by Haskell (1953), Anderson (1961), Anderson (1962), Harkrider and Anderson (1962), Gilbert and MacDonald (1960) and Anderson and Toksöz (1963). It need not be discussed further here. The other methods can also be used as a basis for the sort of calculations presented here, but they would have the disadvantages inherent in any completely numerical method.

Once having the dispersion relation and the eigenfunctions we wish to investigate the change in phase velocity at a given period corresponding to a given change in a physical parameter. If we vary μ , keeping ω and ρ fixed, we have, to first order,

$$\frac{\delta c}{\delta \mu} = \left(ck^2 \frac{\delta I_1}{\delta \mu} + c \frac{\delta I_2}{\delta \mu} \right) / (2I_1 k^2) \quad (5)$$

Similarly, if we vary ρ , keeping ω and μ constant

$$\frac{\delta c}{\delta \rho} = \left(-c^3 \frac{\delta I_0}{\delta \rho} \right) / 2I_1 \quad (6)$$

In a layered structure of n homogeneous layers

$$\begin{aligned} I_0 &= \sum_{m=1}^n \int_{h_m}^{h_{m+1}} \rho_m v^2 dz = \sum_{m=1}^n I_{0m} \\ I_1 &= \sum_{m=1}^n \int_{h_m}^{h_{m+1}} \mu_m v^2 dz = \sum_{m=1}^n I_{1m} \\ I_2 &= \sum_{m=1}^n \int_{h_m}^{h_{m+1}} \mu_m v'^2 dz = \sum_{m=1}^n I_{2m} \end{aligned} \quad (7)$$

By Rayleigh's Principle, for a perturbation of parameters only in the m th layer

$$\begin{aligned}\delta I_0 &= \delta I_{0_m} = \int_{h_m}^{h_{m+1}} \delta \rho_m v^2 dz \\ \delta I_1 &= \delta I_{1_m} = \int_{h_m}^{h_{m+1}} \delta \mu_m v^2 dz \\ \delta I_2 &= \delta I_{2_m} = \int_{h_m}^{h_{m+1}} \delta \mu_m v'^2 dz\end{aligned}\tag{8}$$

Because of the linearization the total effect on phase velocity is

$$dc = \sum_{m=1}^n \left(\frac{\delta c}{\delta \mu} \right)_m d\mu_m + \sum_{m=1}^n \left(\frac{\delta c}{\delta \rho} \right)_m d\rho_m\tag{9}$$

The unperturbed layers, of course, do not contribute to the summation.

In the Haskell formulation of the surface wave problem the motion-stress vector in the m th layer, $\mathfrak{D}_m(z)$, can be written

$$\mathfrak{D}_m(z) = B_m \mathfrak{D}_m(z_m)\tag{10}$$

Where m is the layer index and the depth corresponding to $z = z_m$ is the top of the m th layer. With the convention

$$\mathfrak{D}_m(z) = (\dot{v}/c, p_{yz})$$

it follows that

$$\dot{v}(z)/c = B_{11} \dot{v}(z_m)/c + B_{12} p_{yz}(z_m)\tag{11}$$

where

$$\begin{aligned}B_{11} &= \cos kr_{\beta_m} d_m \\ B_{12} &= i(\mu_m r_{\beta_m})^{-1} \sin kr_{\beta_m} d_m \\ d_m &= h_{m+1} - h_m \\ r_{\beta_m} &= (c^2/\beta_m^2 - 1)^{1/2}\end{aligned}\tag{12}$$

The energy integrals can now be calculated exactly

$$\begin{aligned}I_{0_m} = -\frac{1}{k^2} &\left[\left(\frac{\dot{v}}{c} \right)_m^2 \left(\frac{h_m}{2} + \frac{\sin 2Q}{4kr_{\beta_m}} \right) - \left(\frac{\dot{v}}{c} \right)_m (p_{yz})_m \mu_m^{-1} r_{\beta_m}^{-2} \left(\frac{1 - \cos 2Q}{2k} \right) \right. \\ &\left. + (p_{yz})_m^2 \mu_m^{-2} r_{\beta_m}^{-2} \left(\frac{h_m}{2} - \frac{\sin 2Q}{4kr_{\beta_m}} \right) \right]\end{aligned}\tag{13}$$

$$I_{1_m} = \frac{\mu_m}{\rho_m} I_{0_m} \quad (14)$$

$$I_{2_m} = - \left(\frac{\dot{v}}{c} \right)^2 \mu_m r_{\beta_m}^2 \left[\frac{h_m}{2} - \frac{\sin 2Q}{4kr_{\beta_m}} \right] - \left(\frac{\dot{v}}{c} \right)_m (p_{yz})_m \left[\frac{1 - \cos 2Q}{2k} \right] - (p_{yz})_m^2 \mu_m^{-1} \left[\frac{h_m}{2} + \frac{\sin 2Q}{4kr_{\beta_m}} \right] \quad (15)$$

where $Q = kr_{\beta_m} d_m$.

The *earth stretching* transformations of Anderson and Toksöz (1963) were used in the calculation of I_0 , I_1 , and I_2 , these integrals now representing good approximations for the spherical earth problem.

The effect of other parameters in the system can easily be investigated from the above equations. For example, the following relations are useful

$$\left(\rho \frac{\delta c}{\delta \rho} \right)_\beta = \left(\rho \frac{\delta c}{\delta \rho} \right)_\mu + \left(\mu \frac{\delta c}{\delta \mu} \right)_\rho \quad (16)$$

$$\left(h \frac{\delta c}{\delta h} \right)_{\rho, \mu, \beta} \approx \left(\rho \frac{\delta c}{\delta \rho} \right)_\beta \quad (17)$$

$$\left(\beta \frac{\delta c}{\delta \beta} \right)_\rho \approx 2 \left(\mu \frac{\delta c}{\delta \mu} \right)_\rho \quad (18)$$

where h is a layer thickness and the subscripts are quantities being held constant.

USE OF TABLES AND CURVES

The calculation of dispersion over any spherical, layered earth model involves the use of two tables. The first gives the layer parameters for the trial model and the second gives the partial derivatives of phase velocity with respect to these layer parameters at various periods. Complete tables are presented here for two trial earth models—one oceanic and one continental. A series of partial derivative graphs are presented for several models to illustrate their behavior. In addition to the partial derivative tables, a set of tables is given which indicates the effect of a 10% change in the parameter. The numbers in the partial derivative tables are, in fact, derived from these latter tables.

Table 1 gives the layer index, layer thickness, and depth, shear velocity, density and rigidity for each layer in a model designated Gutenberg-Birch II. This is a continental type model with a density distribution that is closely related to the velocity distribution. Table 2 gives the corresponding values for a model designated CIT13F. This is a model that was designed in the course of a study of the oceanic mantle and gives a good fit to oceanic Love wave data. These models are the trial structures upon which the basic partial derivative tables are based. Tables 1 and 2 also tabulate modifications of these models in which the crust and upper mantle are split into finer layers for detailed studies of this region using shorter period Love

TABLE 1
LAYER INDEX (*M*), LAYER THICKNESS (*D*), SHEAR VELOCITY (BETA), DENSITY (RHO) AND RIGIDITY (*N*) FOR GUTENBERG BIRCH II
CONTINENTAL EARTH MODEL

GUTENBERG BIRCH II						LAMINATED CRUST					
M	D (km)	DEPTH (km)	BETA (km/sec)	RHO (g/cm ³)	N (10 ¹⁰ dy/cm ²)	M	D (km)	DEPTH (km)	BETA (km/sec)	RHO (g/cm ³)	N (10 ¹⁰ dy/cm ²)
1	19.0	9.50	3.550	2.750	34.65	1	0.5	0.25	3.550	2.750	34.65
2	2.0	20.00	3.800	2.900	41.87	2	0.5	0.75	3.550	2.750	34.65
3	2.0	22.00	3.800	2.900	41.87	3	1.0	1.50	3.550	2.750	34.65
4	2.0	24.00	3.800	2.900	41.87	4	1.0	2.50	3.550	2.750	34.65
5	2.0	26.00	3.800	2.900	41.87	5	1.0	3.50	3.550	2.750	34.65
6	6.0	30.00	3.800	2.900	41.87	6	1.0	4.50	3.550	2.750	34.65
7	5.0	35.50	3.800	2.900	41.87	7	2.0	6.00	3.550	2.750	34.65
8	7.0	41.50	4.587	3.560	74.90	8	2.0	8.00	3.550	2.750	34.65
9	5.0	47.50	4.560	3.543	73.67	9	5.0	11.50	3.550	2.750	34.65
10	5.0	52.50	4.543	3.530	72.85	10	5.0	16.50	3.550	2.750	34.65
11	5.0	57.50	4.520	3.515	71.81	11	5.0	21.50	3.800	2.900	41.87
12	5.0	62.50	4.505	3.504	71.11	12	5.0	26.50	3.800	2.900	41.87
13	5.0	67.50	4.487	3.500	70.46	13	5.0	31.50	3.800	2.900	41.87
14	5.0	72.50	4.475	3.494	69.96	14	4.0	36.00	3.800	2.900	41.87
15	5.0	77.50	4.460	3.490	69.42	15	2.0	39.00	4.587	3.560	74.90
16	10.0	85.00	4.440	3.488	68.76	16	5.0	42.50	4.587	3.560	74.90
17	20.0	100.00	4.420	3.485	68.27	17	5.0	47.50	4.560	3.543	73.67
18	20.0	120.00	4.400	3.513	68.01	18	5.0	52.50	4.543	3.530	72.85
19	20.0	140.00	4.390	3.528	67.99	19	5.0	57.50	4.520	3.515	71.81
20	20.0	160.00	4.400	3.546	68.65	20	5.0	62.50	4.505	3.504	71.11
21	20.0	180.00	4.420	3.564	69.62	21	5.0	67.50	4.487	3.500	70.46
22	20.0	200.00	4.450	3.582	70.93	22	5.0	72.50	4.475	3.494	69.96
23	20.0	220.00	4.480	3.606	72.37	23	5.0	77.50	4.460	3.490	69.42
24	20.0	240.00	4.520	3.628	74.12	24	10.0	85.00	4.440	3.488	68.76
25	20.0	260.00	4.570	3.652	76.27	25	10.0	95.00	4.420	3.495	68.27
26	20.0	280.00	4.610	3.676	78.12	26	10.0	105.00	4.400	3.495	68.27
27	35.0	307.50	4.660	3.700	80.34	27	20.0	120.00	4.400	3.513	68.01
28	50.0	350.00	4.810	3.773	87.29	28	20.0	140.00	4.390	3.528	67.99
29	50.0	400.00	4.860	3.848	94.28	29	20.0	160.00	4.400	3.546	68.65
30	50.0	450.00	5.090	3.924	101.66	30	20.0	180.00	4.420	3.564	69.62
31	50.0	500.00	5.220	3.996	108.88	31	20.0	200.00	4.450	3.582	70.93
32	50.0	550.00	5.360	4.071	116.95	32	20.0	220.00	4.480	3.606	72.37
33	75.0	612.50	5.500	4.147	125.44	33	20.0	240.00	4.520	3.628	74.12
34	100.0	700.00	5.770	4.301	143.19	34	20.0	260.00	4.570	3.652	76.27
35	100.0	800.00	6.040	4.422	161.32	35	20.0	280.00	4.610	3.676	78.12
36	100.0	900.00	6.300	4.543	180.31	36	35.0	307.50	4.660	3.700	80.34
37	150.0	1025.00	6.350	4.573	184.39	37	50.0	350.00	4.810	3.773	87.29
38	200.0	1200.00	6.500	4.694	198.32	38	50.0	400.00	4.950	3.848	94.28
39	200.0	1400.00	6.600	4.769	207.73	39	50.0	450.00	5.090	3.924	101.66
40	200.0	1600.00	6.750	4.845	220.75	40	50.0	500.00	5.220	3.996	108.88
41	200.0	1800.00	6.850	4.920	230.85	41	50.0	550.00	5.360	4.071	116.95
42	200.0	2000.00	6.950	4.996	241.31	42	75.0	612.50	5.500	4.147	125.44
43	200.0	2200.00	7.000	5.056	247.74	43	100.0	700.00	5.770	4.301	143.19
44	200.0	2400.00	7.100	5.116	257.89	44	100.0	800.00	6.040	4.422	161.32
45	200.0	2600.00	7.200	5.192	269.15	45	100.0	900.00	6.300	4.543	180.31
46	200.0	2800.00	7.250	5.267	276.84	46	200.0	1050.00	6.350	4.573	184.39
47	200.0	3000.00	7.200	5.267	273.04						
48	20.0	3110.00	7.200	5.252	272.26						

TABLE 2
LAYER INDEX (*M*), LAYER THICKNESS (*D*), SHEAR VELOCITY (*BETA*), DENSITY (*RHO*) AND RIGIDITY (*N*) FOR CITI3F OCEANIC EARTH MODEL

CITI3F OCEANIC				OCEANIC				LAMINATED CRUST			
M	D (km)	DEPTH (km)	BETA (km/sec)	RHO (g/cm ³)	N (10 ¹⁰ dy/cm ²)	M	D (km)	DEPTH (km)	BETA (km/sec)	RHO (g/cm ³)	N (10 ¹⁰ dy/cm ²)
1	0.5	0.25	0.800	1.900	1.21	1	0.1	0.05	0.800	1.900	1.21
2	2.0	1.50	2.800	2.540	21.06	2	0.2	0.20	0.800	1.900	1.21
3	5.0	5.00	3.700	2.900	39.70	3	0.2	0.40	0.800	1.900	1.21
4	9.0	12.00	4.600	3.320	70.25	4	0.5	0.75	2.800	2.540	21.06
5	5.0	19.00	4.600	3.325	70.35	5	0.5	1.25	2.800	2.540	21.06
6	5.0	24.00	4.560	3.330	69.24	6	1.0	2.00	2.800	2.540	21.06
7	10.0	31.50	4.460	3.335	66.33	7	1.0	3.00	3.700	2.900	39.70
8	20.0	46.50	4.400	3.350	64.85	8	2.0	4.50	3.700	2.900	39.70
9	20.0	66.50	4.400	3.375	65.34	9	2.0	6.50	3.700	2.900	39.70
10	20.0	86.50	4.400	3.390	65.63	10	2.0	8.50	4.600	3.320	70.25
11	20.0	106.50	4.400	3.410	66.01	11	2.0	10.50	4.600	3.320	70.25
12	20.0	126.50	4.400	3.425	66.30	12	2.0	12.50	4.600	3.320	70.25
13	20.0	146.50	4.440	3.460	67.81	13	2.0	14.50	4.600	3.320	70.25
14	20.0	166.50	4.480	3.460	69.44	14	1.0	16.00	4.600	3.320	70.25
15	20.0	186.50	4.510	3.475	70.68	15	5.0	19.00	4.600	3.325	70.35
16	20.0	206.50	4.540	3.490	71.93	16	5.0	24.00	4.560	3.330	69.24
17	20.0	226.50	4.540	3.510	72.34	17	5.0	29.00	4.460	3.335	66.33
18	20.0	246.50	4.540	3.525	72.65	18	5.0	34.00	4.460	3.335	66.33
19	20.0	266.50	4.560	3.540	73.60	19	5.0	39.00	4.400	3.350	64.85
20	20.0	286.50	4.560	3.560	74.92	20	5.0	44.00	4.400	3.350	64.85
21	20.0	306.50	4.560	3.570	74.23	21	5.0	49.00	4.400	3.350	64.85
22	20.0	326.50	4.580	3.590	75.30	22	5.0	54.00	4.400	3.350	64.85
23	20.0	346.50	4.580	3.605	75.61	23	10.0	61.50	4.400	3.375	65.34
24	40.0	376.50	4.580	3.630	76.14	24	10.0	71.50	4.400	3.375	65.34
25	50.0	421.50	4.620	3.690	78.76	25	10.0	81.50	4.400	3.390	65.63
26	10.0	451.50	4.670	3.775	82.32	26	10.0	91.50	4.400	3.390	65.63
27	100.0	506.50	5.500	4.020	121.60	27	20.0	106.50	4.400	3.410	66.01
28	100.0	606.50	5.620	4.225	133.44	28	20.0	126.50	4.400	3.425	66.30
29	100.0	706.50	5.890	4.400	152.64	29	20.0	146.50	4.440	3.440	67.81
30	100.0	806.50	6.000	4.560	164.16	30	20.0	166.50	4.480	3.460	69.44
31	100.0	906.50	6.200	4.630	177.97	31	20.0	186.50	4.510	3.475	70.68
32	200.0	1056.50	6.410	4.740	194.75	32	20.0	206.50	4.540	3.490	71.93
33	200.0	1256.50	6.550	4.850	208.07	33	20.0	226.50	4.540	3.510	72.34
34	200.0	1456.50	6.690	4.960	221.99	34	20.0	246.50	4.540	3.525	72.65
35	200.0	1656.50	6.780	5.070	233.05	35	20.0	266.50	4.560	3.540	73.60
36	150.0	1831.50	6.850	5.150	241.65	36	20.0	286.50	4.560	3.560	74.92
37	100.0	1956.50	6.900	5.208	247.95	37	20.0	306.50	4.560	3.570	75.30
38	100.0	2056.50	6.950	5.270	254.55	38	20.0	326.50	4.580	3.590	75.61
39	100.0	2156.50	7.000	5.320	260.67	39	20.0	346.50	4.580	3.605	76.14
40	100.0	2256.50	7.050	5.370	266.90	40	40.0	376.50	4.580	3.630	76.81
41	100.0	2356.50	7.100	5.420	273.22	41	50.0	421.50	4.620	3.690	78.76
42	100.0	2456.50	7.140	5.470	278.85	42	100.0	451.50	4.670	3.775	82.32
43	100.0	2556.50	7.190	5.520	285.36	43	100.0	506.50	5.500	4.020	121.60
44	100.0	2656.50	7.230	5.560	290.63	44	100.0	606.50	5.620	4.225	133.44
45	154.0	2783.50	7.280	5.610	297.32	45	100.0	706.50	5.890	4.400	152.64
46	100.0	2910.50	7.300	5.660	301.62	46	200.0	856.50	6.000	4.560	164.16

waves. Any given crustal and upper mantle structure can be achieved by perturbing the density and rigidity in the upper layers. Table 3 gives the layer parameters for a model patterned after the Gutenberg IV model of MacDonald and Ness (1961). This model has a Bullen A type density distribution. The Jeffreys-Bullen model is also tabulated in table 3.

Table 4 presents the complete dispersion and partial derivative results for the Gutenberg-Birch II model. If the parameters in the layers are changed in order to approximate another continental type structure the phase velocity at the indicated period is changed by an amount Δc , where

$$\Delta c = \sum_{M=1}^N \text{DCDRHO}(M) \cdot \Delta \rho + \sum_{M=1}^N \text{DCDMU}(M) \cdot \Delta \mu \quad (19)$$

In this case $N = 46$ is the total number of layers used to approximate the mantle but the summation need only extend over the perturbed layers. DCDRHO and DCDMU are computerese for $\delta c/\delta \rho$ and $\delta c/\delta \mu$.

Table 5 gives the effect of a ten-percent change in the parameters for this model and in this case

$$\Delta c = 10 \sum_{M=1}^N [(\text{DC/DRHO}(M)) \cdot (\Delta \rho/\rho)] + 10 \sum_{M=1}^N [(\text{DC/DMU}(M)) \cdot (\Delta \mu/\mu)] \quad (20)$$

or

$$\begin{aligned} \Delta c = 21 \sum_{M=1}^N [\text{DC/DMU}(M)] \cdot \Delta \beta/\beta \\ + 10 \sum_{M=1}^N [\text{DC/DMU}(M) + \text{DC/DRHO}(M)] \cdot \Delta \rho/\rho \end{aligned} \quad (21)$$

When only the shear velocity is being perturbed the second summation in the last expression does not contribute. DC/DMU and DC/DRHO are, respectively, $(\rho \delta c/\delta \rho)_\mu/10$ and $(\mu \delta c/\delta \mu)_\rho/10$.

Tables 6 and 7 give the corresponding results for the CIT13F model. As much as possible a new mantle structure should be designed in the framework of the layering given. When this is too restrictive tables 8 through 11 allow finer adjustments to be made in the near surface structure in order to satisfy short period (< 200 second) data. Still finer adjustments may be made by splitting the layers again and apportioning the partial derivatives appropriately.

ACCURACY OF THE METHOD

The partial derivatives have been tested for a variety of cases, and tables similar to the ones presented here have been in routine use for about 14 months at Caltech. The tables are believed to be error free and very accurate in spite of the various approximations that have been used in their calculation. Each user, however, should convince himself of the reliability and extent of applicability of the tables for his own

TABLE 3
LAYER PARAMETERS FOR THE JEFFREYS-BULLEN AND GUTENBERG IV CONTINENTAL
EARTH MODELS

JEFFREYS-BULLEN

M	D (km)	DEPTH (km)	BETA (km/sec)	RHO (g/cm ³)	N (10 ¹⁰ dy/cm ²)
1	15	7.5	3.360	2.650	29.91
2	18	24.0	3.740	2.870	40.14
3	17	41.5	4.360	3.330	63.30
4	25	62.5	4.390	3.350	64.56
5	35	92.5	4.440	3.370	66.43
6	40	130.0	4.490	3.410	68.74
7	50	175.0	4.560	3.450	71.73
8	50	225.0	4.640	3.490	75.13
9	50	275.0	4.720	3.530	78.64
10	50	325.0	4.800	3.570	82.25
11	63	381.5	4.900	3.615	86.79
12	37	431.5	5.040	3.700	93.98
13	100	500.0	5.310	3.890	109.68
14	100	600.0	5.660	4.125	132.14
15	100	700.0	5.930	4.320	151.91
16	100	800.0	6.130	4.490	168.72
17	150	925.0	6.290	4.620	182.78
18	200	1100.0	6.440	4.739	196.54
19	400	1400.0	6.620	4.915	215.39
20	400	1800.0	6.830	5.135	239.54
21	400	2200.0	7.020	5.340	263.15
22	400	2600.0	7.210	5.540	287.99

GUTENBERG IV

M	D (km)	DEPTH (km)	BETA (km/sec)	RHO (g/cm ³)	N (10 ¹⁰ dy/cm ²)
1	21	10.5	3.55	2.738	34.50
2	10	26.0	3.80	3.000	43.31
3	20	41.0	4.65	3.321	71.80
4	10	56.0	4.60	3.370	71.30
5	10	66.0	4.57	3.352	70.00
6	10	76.0	4.51	3.358	68.30
7	10	86.0	4.46	3.368	66.99
8	10	96.0	4.41	3.378	65.69
9	20	111.0	4.37	3.388	64.70
10	30	136.0	4.35	3.409	64.50
11	20	161.0	4.36	3.430	65.20
12	30	186.0	4.38	3.461	66.39
13	20	211.0	4.42	3.481	68.00
14	30	236.0	4.46	3.500	69.62
15	50	276.0	4.52	3.524	71.99
16	50	326.0	4.66	3.592	78.00
17	50	376.0	4.82	3.650	84.79
18	50	426.0	5.00	3.696	92.40
19	50	476.0	5.14	3.820	100.92
20	100	551.0	5.38	4.010	116.06
21	100	651.0	5.69	4.140	134.03
22	100	751.0	5.96	4.390	155.93
23	100	851.0	6.15	4.550	172.09
24	100	951.0	6.24	4.620	179.89
25	200	1101.0	6.34	4.730	190.12
26	200	1301.0	6.47	4.850	203.02
27	200	1501.0	6.61	4.970	217.14
28	200	1701.0	6.72	5.050	228.04
29	200	1901.0	6.81	5.200	241.15
30	100	2051.0	6.88	5.302	250.96
31	100	2151.0	6.88	5.302	250.96
32	200	2301.0	6.94	5.439	261.96
33	200	2501.0	7.06	5.497	273.99
34	200	2701.0	7.14	5.590	284.97
35	100	2851.0	7.11	5.697	287.99
36	100	2951.0	7.11	5.700	288.14

TABLE 4a
PERIOD (T), PHASE VELOCITY (c) AND VARIATIONAL PARTIAL DERIVATIVES FOR GUTENBERG BIRCH II
CONTINENTAL EARTH MODEL

GUTENBERG BIRCH II CONTINENTAL									
PSEUDO SPHERICAL CALCULATION									
11 SECS) 1079.48									
C/K/SEC) 6.720									
951.57									
6.620									
861.17									
6.320									
788.74									
6.420									
727.21									
6.320									
673.12									
6.220									
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO
1	-0.00256	0.00052	-0.02542	0.00060	-0.02783	0.00067	-0.03604	0.00074	-0.03214
2	-0.00235	0.00005	-0.00265	0.00006	-0.00290	0.00007	-0.00313	0.00008	-0.00340
3	-0.00235	0.00005	-0.00265	0.00006	-0.00290	0.00007	-0.00313	0.00008	-0.00340
4	-0.00235	0.00005	-0.00265	0.00006	-0.00290	0.00007	-0.00313	0.00008	-0.00340
5	-0.00234	0.00005	-0.00264	0.00006	-0.00289	0.00007	-0.00312	0.00008	-0.00334
6	-0.00201	0.00016	-0.00279	0.00019	-0.00289	0.00021	-0.00333	0.00026	-0.00355
7	-0.00582	0.00014	-0.00655	0.00016	-0.00717	0.00017	-0.00932	0.00019	-0.01060
8	-0.00811	0.00019	-0.00913	0.00022	-0.00717	0.00024	-0.01078	0.00027	-0.01225
9	-0.00577	0.00013	-0.00649	0.00015	-0.00710	0.00017	-0.00766	0.00019	-0.00819
10	-0.00575	0.00013	-0.00647	0.00015	-0.00707	0.00017	-0.00763	0.00019	-0.00816
11	-0.00572	0.00013	-0.00644	0.00015	-0.00705	0.00017	-0.00760	0.00019	-0.00812
12	-0.00570	0.00013	-0.00642	0.00015	-0.00702	0.00017	-0.00757	0.00019	-0.00809
13	-0.00568	0.00013	-0.00639	0.00015	-0.00699	0.00017	-0.00753	0.00019	-0.00805
14	-0.00566	0.00013	-0.00637	0.00015	-0.00696	0.00017	-0.00750	0.00019	-0.00801
15	-0.00564	0.00013	-0.00634	0.00015	-0.00693	0.00017	-0.00747	0.00019	-0.00798
16	-0.01122	0.00027	-0.01261	0.00031	-0.01378	0.00034	-0.01484	0.00038	-0.01585
17	-0.02219	0.00053	-0.02493	0.00061	-0.02722	0.00065	-0.02930	0.00076	-0.03127
18	-0.02181	0.00053	-0.02447	0.00061	-0.02669	0.00068	-0.02871	0.00075	-0.03060
19	-0.02141	0.00052	-0.02400	0.00060	-0.02614	0.00068	-0.02807	0.00075	-0.02988
20	-0.02101	0.00052	-0.02350	0.00060	-0.02556	0.00067	-0.02742	0.00074	-0.02914
21	-0.02059	0.00052	-0.02299	0.00060	-0.02497	0.00067	-0.02673	0.00074	-0.02836
22	-0.02016	0.00051	-0.02247	0.00059	-0.02436	0.00066	-0.02603	0.00073	-0.02756
23	-0.01973	0.00051	-0.02194	0.00059	-0.02373	0.00066	-0.02531	0.00072	-0.02679
24	-0.01929	0.00051	-0.02140	0.00058	-0.02310	0.00065	-0.02458	0.00072	-0.02591
25	-0.01885	0.00050	-0.02086	0.00057	-0.02246	0.00064	-0.02384	0.00071	-0.02507
26	-0.01841	0.00050	-0.02032	0.00057	-0.02182	0.00063	-0.02310	0.00070	-0.02423
27	-0.03124	0.00086	-0.03434	0.00098	-0.03675	0.00109	-0.03877	0.00120	-0.04050
28	-0.04241	0.00119	-0.04633	0.00135	-0.04929	0.00150	-0.05167	0.00163	-0.05364
29	-0.03971	0.00114	-0.03984	0.00129	-0.04542	0.00142	-0.04725	0.00154	-0.04865
30	-0.03709	0.00109	-0.03984	0.00123	-0.04171	0.00134	-0.04301	0.00144	-0.04391
31	-0.03457	0.00104	-0.03680	0.00116	-0.03818	0.00126	-0.03904	0.00134	-0.03948
32	-0.03216	0.00099	-0.03390	0.00109	-0.03486	0.00117	-0.03532	0.00124	-0.03537
33	-0.04428	0.00140	-0.04612	0.00152	-0.04689	0.00162	-0.04695	0.00170	-0.04645
34	-0.05211	0.00168	-0.05334	0.00180	-0.05334	0.00188	-0.05252	0.00194	-0.05105
35	-0.04471	0.00149	-0.04482	0.00156	-0.04394	0.00159	-0.04240	0.00161	-0.04134
36	-0.03828	0.00131	-0.03758	0.00134	-0.03612	0.00134	-0.03415	0.00132	-0.03180
37	-0.04787	0.00172	-0.04302	0.00178	-0.04302	0.00168	-0.03972	0.00162	-0.03607
38	-0.04852	0.00185	-0.04474	0.00178	-0.04053	0.00168	-0.03609	0.00155	-0.03156
39	-0.03401	0.00140	-0.02986	0.00128	-0.02583	0.00116	-0.02195	0.00102	-0.01828
40	-0.02324	0.00103	-0.01934	0.00090	-0.01591	0.00077	-0.01285	0.00064	-0.00942
41	-0.01553	0.00075	-0.01220	0.00061	-0.00951	0.00049	-0.00727	0.00039	-0.00545
42	-0.01014	0.00053	-0.00749	0.00041	-0.00550	0.00031	-0.00397	0.00023	-0.00278
43	-0.00649	0.00037	-0.00448	0.00026	-0.00310	0.00019	-0.00209	0.00013	-0.00138
44	-0.00406	0.00025	-0.00262	0.00017	-0.00169	0.00011	-0.00107	0.00007	-0.00065
45	-0.00252	0.00017	-0.00151	0.00010	-0.00091	0.00007	-0.00053	0.00004	-0.00030
46	-0.00157	0.00012	-0.00088	0.00007	-0.00049	0.00004	-0.00027	0.00002	-0.00014
47	-0.00100	0.00008	-0.00053	0.00004	-0.00028	0.00002	-0.00015	0.00001	-0.00007
48	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000

TABLE 4b
PERIOD (T), PHASE VELOCITY (c) AND VARIATIONAL PARTIAL DERIVATIVES FOR GUTENBERG BIRCH II
CONTINENTAL EARTH MODEL

GUTENBERG BIRCH II									
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO
T (SECS)	624.48	580.00	538.79	500.19	463.71	428.91			
C (K/SEC)	6.120	6.020	5.920	5.820	5.720	5.620			
1	-0.03621	-0.00098	-0.03820	-0.00107	-0.04419	-0.00136	-0.04613	-0.00147	-0.00147
2	-0.03377	-0.00010	-0.00398	-0.00011	-0.00439	-0.00013	-0.00459	-0.00014	-0.00015
3	-0.00376	-0.00010	-0.00397	-0.00011	-0.00418	-0.00012	-0.00438	-0.00013	-0.00015
4	-0.00376	-0.00010	-0.00396	-0.00011	-0.00417	-0.00012	-0.00437	-0.00013	-0.00015
5	-0.00122	-0.00010	-0.00396	-0.00011	-0.00416	-0.00012	-0.00436	-0.00013	-0.00015
6	-0.01122	-0.00031	-0.01184	-0.00033	-0.01244	-0.00036	-0.01305	-0.00039	-0.00046
7	-0.00930	-0.00026	-0.00981	-0.00028	-0.01031	-0.00030	-0.01081	-0.00033	-0.00046
8	-0.01296	-0.00036	-0.01366	-0.00039	-0.01436	-0.00042	-0.01505	-0.00045	-0.00058
9	-0.00921	-0.00025	-0.00970	-0.00028	-0.01020	-0.00030	-0.01068	-0.00032	-0.00038
10	-0.00917	-0.00025	-0.00966	-0.00027	-0.01015	-0.00030	-0.01058	-0.00032	-0.00038
11	-0.00912	-0.00025	-0.00961	-0.00027	-0.01010	-0.00030	-0.01052	-0.00032	-0.00038
12	-0.00908	-0.00025	-0.00957	-0.00027	-0.01005	-0.00030	-0.01046	-0.00032	-0.00038
13	-0.00904	-0.00025	-0.00952	-0.00027	-0.00999	-0.00030	-0.01040	-0.00032	-0.00037
14	-0.00899	-0.00025	-0.00947	-0.00027	-0.00994	-0.00030	-0.01034	-0.00032	-0.00037
15	-0.00895	-0.00025	-0.00942	-0.00027	-0.00989	-0.00030	-0.01028	-0.00032	-0.00037
16	-0.00891	-0.00025	-0.00937	-0.00027	-0.00984	-0.00030	-0.01022	-0.00032	-0.00037
17	-0.00887	-0.00025	-0.00932	-0.00027	-0.00979	-0.00030	-0.01016	-0.00032	-0.00037
18	-0.00883	-0.00025	-0.00927	-0.00027	-0.00974	-0.00030	-0.01010	-0.00032	-0.00037
19	-0.00879	-0.00025	-0.00922	-0.00027	-0.00969	-0.00030	-0.01004	-0.00032	-0.00037
20	-0.00875	-0.00025	-0.00917	-0.00027	-0.00964	-0.00030	-0.01000	-0.00032	-0.00037
21	-0.00871	-0.00025	-0.00912	-0.00027	-0.00959	-0.00030	-0.00994	-0.00032	-0.00037
22	-0.00867	-0.00025	-0.00907	-0.00027	-0.00954	-0.00030	-0.00989	-0.00032	-0.00037
23	-0.00863	-0.00025	-0.00902	-0.00027	-0.00949	-0.00030	-0.00984	-0.00032	-0.00037
24	-0.00859	-0.00025	-0.00897	-0.00027	-0.00944	-0.00030	-0.00979	-0.00032	-0.00037
25	-0.00855	-0.00025	-0.00892	-0.00027	-0.00939	-0.00030	-0.00974	-0.00032	-0.00037
26	-0.00851	-0.00025	-0.00887	-0.00027	-0.00934	-0.00030	-0.00969	-0.00032	-0.00037
27	-0.00847	-0.00025	-0.00882	-0.00027	-0.00929	-0.00030	-0.00964	-0.00032	-0.00037
28	-0.00843	-0.00025	-0.00877	-0.00027	-0.00924	-0.00030	-0.00959	-0.00032	-0.00037
29	-0.00839	-0.00025	-0.00872	-0.00027	-0.00919	-0.00030	-0.00954	-0.00032	-0.00037
30	-0.00835	-0.00025	-0.00867	-0.00027	-0.00914	-0.00030	-0.00949	-0.00032	-0.00037
31	-0.00831	-0.00025	-0.00862	-0.00027	-0.00909	-0.00030	-0.00944	-0.00032	-0.00037
32	-0.00827	-0.00025	-0.00857	-0.00027	-0.00904	-0.00030	-0.00939	-0.00032	-0.00037
33	-0.00823	-0.00025	-0.00852	-0.00027	-0.00900	-0.00030	-0.00934	-0.00032	-0.00037
34	-0.00819	-0.00025	-0.00847	-0.00027	-0.00895	-0.00030	-0.00929	-0.00032	-0.00037
35	-0.00815	-0.00025	-0.00842	-0.00027	-0.00890	-0.00030	-0.00924	-0.00032	-0.00037
36	-0.00811	-0.00025	-0.00837	-0.00027	-0.00885	-0.00030	-0.00919	-0.00032	-0.00037
37	-0.00807	-0.00025	-0.00832	-0.00027	-0.00880	-0.00030	-0.00914	-0.00032	-0.00037
38	-0.00803	-0.00025	-0.00827	-0.00027	-0.00875	-0.00030	-0.00909	-0.00032	-0.00037
39	-0.00799	-0.00025	-0.00822	-0.00027	-0.00870	-0.00030	-0.00904	-0.00032	-0.00037
40	-0.00795	-0.00025	-0.00817	-0.00027	-0.00865	-0.00030	-0.00899	-0.00032	-0.00037
41	-0.00791	-0.00025	-0.00812	-0.00027	-0.00860	-0.00030	-0.00894	-0.00032	-0.00037
42	-0.00787	-0.00025	-0.00807	-0.00027	-0.00855	-0.00030	-0.00889	-0.00032	-0.00037
43	-0.00783	-0.00025	-0.00802	-0.00027	-0.00850	-0.00030	-0.00884	-0.00032	-0.00037
44	-0.00779	-0.00025	-0.00797	-0.00027	-0.00845	-0.00030	-0.00879	-0.00032	-0.00037
45	-0.00775	-0.00025	-0.00792	-0.00027	-0.00840	-0.00030	-0.00874	-0.00032	-0.00037
46	-0.00771	-0.00025	-0.00787	-0.00027	-0.00835	-0.00030	-0.00869	-0.00032	-0.00037
47	-0.00767	-0.00025	-0.00782	-0.00027	-0.00830	-0.00030	-0.00864	-0.00032	-0.00037
48	-0.00763	-0.00025	-0.00777	-0.00027	-0.00825	-0.00030	-0.00859	-0.00032	-0.00037

TABLE 4c
PERIOD (T), PHASE VELOCITY (c) AND VARIATIONAL PARTIAL DERIVATIVES FOR GUTENBERG BIRCH II
CONTINENTAL EARTH MODEL

GUTENBERG BIRCH II CONTINENTAL											
PSEUDO SPHERICAL CALCULATION											
T (SECS) 422.12											
C (K/SEC) 5.630											
388.89											
5.500											
356.64											
5.400											
325.10											
5.300											
294.04											
5.200											
263.25											
5.100											
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO
1	-0.04652	0.00150	-0.04852	0.00162	-0.05057	0.00175	-0.05271	0.00189	-0.05501	0.00205	-0.05758
2	-0.04844	0.00016	-0.05004	0.00017	-0.05225	0.00018	-0.05471	0.00020	-0.05717	0.00021	-0.05978
3	-0.04883	0.00016	-0.05003	0.00017	-0.05224	0.00018	-0.05466	0.00020	-0.05716	0.00021	-0.05975
4	-0.04882	0.00016	-0.05002	0.00017	-0.05223	0.00018	-0.05465	0.00020	-0.05715	0.00021	-0.05974
5	-0.04881	0.00016	-0.05001	0.00017	-0.05222	0.00018	-0.05464	0.00020	-0.05714	0.00021	-0.05973
6	-0.04879	0.00016	-0.05000	0.00017	-0.05221	0.00018	-0.05463	0.00020	-0.05713	0.00021	-0.05972
7	-0.04878	0.00016	-0.05000	0.00017	-0.05220	0.00018	-0.05462	0.00020	-0.05712	0.00021	-0.05971
8	-0.04877	0.00016	-0.05000	0.00017	-0.05219	0.00018	-0.05461	0.00020	-0.05711	0.00021	-0.05970
9	-0.04876	0.00016	-0.05000	0.00017	-0.05218	0.00018	-0.05460	0.00020	-0.05710	0.00021	-0.05969
10	-0.04875	0.00016	-0.05000	0.00017	-0.05217	0.00018	-0.05459	0.00020	-0.05709	0.00021	-0.05968
11	-0.04874	0.00016	-0.05000	0.00017	-0.05216	0.00018	-0.05458	0.00020	-0.05708	0.00021	-0.05967
12	-0.04873	0.00016	-0.05000	0.00017	-0.05215	0.00018	-0.05457	0.00020	-0.05707	0.00021	-0.05966
13	-0.04872	0.00016	-0.05000	0.00017	-0.05214	0.00018	-0.05456	0.00020	-0.05706	0.00021	-0.05965
14	-0.04871	0.00016	-0.05000	0.00017	-0.05213	0.00018	-0.05455	0.00020	-0.05705	0.00021	-0.05964
15	-0.04870	0.00016	-0.05000	0.00017	-0.05212	0.00018	-0.05454	0.00020	-0.05704	0.00021	-0.05963
16	-0.04869	0.00016	-0.05000	0.00017	-0.05211	0.00018	-0.05453	0.00020	-0.05703	0.00021	-0.05962
17	-0.04868	0.00016	-0.05000	0.00017	-0.05210	0.00018	-0.05452	0.00020	-0.05702	0.00021	-0.05961
18	-0.04867	0.00016	-0.05000	0.00017	-0.05209	0.00018	-0.05451	0.00020	-0.05701	0.00021	-0.05960
19	-0.04866	0.00016	-0.05000	0.00017	-0.05208	0.00018	-0.05450	0.00020	-0.05700	0.00021	-0.05959
20	-0.04865	0.00016	-0.05000	0.00017	-0.05207	0.00018	-0.05449	0.00020	-0.05699	0.00021	-0.05958
21	-0.04864	0.00016	-0.05000	0.00017	-0.05206	0.00018	-0.05448	0.00020	-0.05698	0.00021	-0.05957
22	-0.04863	0.00016	-0.05000	0.00017	-0.05205	0.00018	-0.05447	0.00020	-0.05697	0.00021	-0.05956
23	-0.04862	0.00016	-0.05000	0.00017	-0.05204	0.00018	-0.05446	0.00020	-0.05696	0.00021	-0.05955
24	-0.04861	0.00016	-0.05000	0.00017	-0.05203	0.00018	-0.05445	0.00020	-0.05695	0.00021	-0.05954
25	-0.04860	0.00016	-0.05000	0.00017	-0.05202	0.00018	-0.05444	0.00020	-0.05694	0.00021	-0.05953
26	-0.04859	0.00016	-0.05000	0.00017	-0.05201	0.00018	-0.05443	0.00020	-0.05693	0.00021	-0.05952
27	-0.04858	0.00016	-0.05000	0.00017	-0.05200	0.00018	-0.05442	0.00020	-0.05692	0.00021	-0.05951
28	-0.04857	0.00016	-0.05000	0.00017	-0.05199	0.00018	-0.05441	0.00020	-0.05691	0.00021	-0.05950
29	-0.04856	0.00016	-0.05000	0.00017	-0.05198	0.00018	-0.05440	0.00020	-0.05690	0.00021	-0.05949
30	-0.04855	0.00016	-0.05000	0.00017	-0.05197	0.00018	-0.05439	0.00020	-0.05689	0.00021	-0.05948
31	-0.04854	0.00016	-0.05000	0.00017	-0.05196	0.00018	-0.05438	0.00020	-0.05688	0.00021	-0.05947
32	-0.04853	0.00016	-0.05000	0.00017	-0.05195	0.00018	-0.05437	0.00020	-0.05687	0.00021	-0.05946
33	-0.04852	0.00016	-0.05000	0.00017	-0.05194	0.00018	-0.05436	0.00020	-0.05686	0.00021	-0.05945
34	-0.04851	0.00016	-0.05000	0.00017	-0.05193	0.00018	-0.05435	0.00020	-0.05685	0.00021	-0.05944
35	-0.04850	0.00016	-0.05000	0.00017	-0.05192	0.00018	-0.05434	0.00020	-0.05684	0.00021	-0.05943
36	-0.04849	0.00016	-0.05000	0.00017	-0.05191	0.00018	-0.05433	0.00020	-0.05683	0.00021	-0.05942
37	-0.04848	0.00016	-0.05000	0.00017	-0.05190	0.00018	-0.05432	0.00020	-0.05682	0.00021	-0.05941
38	-0.04847	0.00016	-0.05000	0.00017	-0.05189	0.00018	-0.05431	0.00020	-0.05681	0.00021	-0.05940
39	-0.04846	0.00016	-0.05000	0.00017	-0.05188	0.00018	-0.05430	0.00020	-0.05680	0.00021	-0.05939
40	-0.04845	0.00016	-0.05000	0.00017	-0.05187	0.00018	-0.05429	0.00020	-0.05679	0.00021	-0.05938
41	-0.04844	0.00016	-0.05000	0.00017	-0.05186	0.00018	-0.05428	0.00020	-0.05678	0.00021	-0.05937
42	-0.04843	0.00016	-0.05000	0.00017	-0.05185	0.00018	-0.05427	0.00020	-0.05677	0.00021	-0.05936
43	-0.04842	0.00016	-0.05000	0.00017	-0.05184	0.00018	-0.05426	0.00020	-0.05676	0.00021	-0.05935
44	-0.04841	0.00016	-0.05000	0.00017	-0.05183	0.00018	-0.05425	0.00020	-0.05675	0.00021	-0.05934
45	-0.04840	0.00016	-0.05000	0.00017	-0.05182	0.00018	-0.05424	0.00020	-0.05674	0.00021	-0.05933
46	-0.04839	0.00016	-0.05000	0.00017	-0.05181	0.00018	-0.05423	0.00020	-0.05673	0.00021	-0.05932
47	-0.04838	0.00016	-0.05000	0.00017	-0.05180	0.00018	-0.05422	0.00020	-0.05672	0.00021	-0.05931
48	-0.04837	0.00016	-0.05000	0.00017	-0.05179	0.00018	-0.05421	0.00020	-0.05671	0.00021	-0.05930

TABLE 4d
PERIOD (T), PHASE VELOCITY (c) AND VARIATIONAL PARTIAL DERIVATIVES FOR GUTENBERG BIRCH II CONTINENTAL
EARTH MODEL

GUTENBERG BIRCH II		201.79		170.93		140.07		109.70		81.33	
T (SECS)		4.900		4.800		4.700		4.600		4.500	
C (K/SEC)		5.000									
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO
1	-0.06062	0.03244	-0.06445	0.00270	-0.06965	0.00305	-0.07737	0.00354	-0.09027	0.00432	-0.11513
2	-0.060627	0.00025	-0.00665	0.00028	-0.00713	0.00032	-0.00792	0.00037	-0.00914	0.00044	-0.01143
3	-0.00625	0.00025	-0.00663	0.00028	-0.00710	0.00032	-0.00787	0.00036	-0.00907	0.00044	-0.01127
4	-0.00623	0.00025	-0.00660	0.00028	-0.00710	0.00032	-0.00782	0.00036	-0.00898	0.00044	-0.01110
5	-0.00621	0.00025	-0.00658	0.00028	-0.00706	0.00031	-0.00777	0.00036	-0.00890	0.00044	-0.01093
6	-0.01849	0.00076	-0.01956	0.00084	-0.02096	0.00094	-0.02297	0.00108	-0.02614	0.00130	-0.03168
7	-0.01523	0.00063	-0.01607	0.00069	-0.01716	0.00078	-0.01870	0.00089	-0.02106	0.00106	-0.02498
8	-0.02108	0.00086	-0.02220	0.00095	-0.02364	0.00105	-0.02563	0.00119	-0.02858	0.00140	-0.03323
9	-0.01490	0.00061	-0.01567	0.00067	-0.01664	0.00074	-0.01797	0.00084	-0.01989	0.00097	-0.02279
10	-0.01477	0.00061	-0.01551	0.00067	-0.01644	0.00074	-0.01769	0.00083	-0.01946	0.00096	-0.02202
11	-0.01463	0.00060	-0.01534	0.00066	-0.01623	0.00073	-0.01741	0.00082	-0.01904	0.00094	-0.02127
12	-0.01449	0.00060	-0.01517	0.00066	-0.01602	0.00072	-0.01712	0.00081	-0.01860	0.00092	-0.02054
13	-0.01435	0.00060	-0.01500	0.00065	-0.01580	0.00071	-0.01682	0.00080	-0.01817	0.00090	-0.01982
14	-0.01420	0.00059	-0.01482	0.00064	-0.01557	0.00071	-0.01652	0.00078	-0.01774	0.00088	-0.01911
15	-0.01404	0.00059	-0.01463	0.00064	-0.01534	0.00070	-0.01622	0.00077	-0.01730	0.00086	-0.01841
16	-0.02762	0.00116	-0.02871	0.00126	-0.02999	0.00137	-0.03153	0.00151	-0.03331	0.00167	-0.03471
17	-0.05329	0.00227	-0.05509	0.00245	-0.05710	0.00265	-0.05932	0.00287	-0.06144	0.00312	-0.06187
18	-0.05035	0.00219	-0.05162	0.00234	-0.05289	0.00250	-0.05400	0.00266	-0.05434	0.00281	-0.05193
19	-0.04720	0.00210	-0.04794	0.00222	-0.04848	0.00234	-0.04854	0.00244	-0.04733	0.00249	-0.04277
20	-0.04391	0.00199	-0.04412	0.00209	-0.04395	0.00217	-0.04306	0.00222	-0.04056	0.00218	-0.03450
21	-0.04053	0.00188	-0.04023	0.00195	-0.03943	0.00199	-0.03771	0.00198	-0.03419	0.00188	-0.02724
22	-0.03713	0.00177	-0.03637	0.00180	-0.03500	0.00181	-0.03260	0.00176	-0.02835	0.00160	-0.02105
23	-0.03377	0.00165	-0.03260	0.00166	-0.03076	0.00163	-0.02783	0.00154	-0.02313	0.00133	-0.01592
24	-0.03053	0.00152	-0.02899	0.00151	-0.02676	0.00145	-0.02347	0.00133	-0.01858	0.00110	-0.01179
25	-0.02737	0.00140	-0.02558	0.00136	-0.02307	0.00128	-0.01957	0.00113	-0.01471	0.00089	-0.00856
26	-0.02441	0.00128	-0.02240	0.00122	-0.01972	0.00112	-0.01614	0.00096	-0.01148	0.00071	-0.00610
27	-0.03637	0.00197	-0.03253	0.00183	-0.02765	0.00162	-0.02152	0.00132	-0.01417	0.00091	-0.00664
28	-0.03973	0.00222	-0.03404	0.00198	-0.02728	0.00165	-0.01951	0.00123	-0.01128	0.00074	-0.00428
29	-0.02800	0.00163	-0.02267	0.00138	-0.01681	0.00106	-0.01075	0.00071	-0.00522	0.00036	-0.00149
30	-0.01926	0.00117	-0.01466	0.00093	-0.01000	0.00066	-0.00566	0.00039	-0.00228	0.00016	-0.00048
31	-0.01294	0.00081	-0.00923	0.00060	-0.00576	0.00039	-0.00287	0.00020	-0.00095	0.00007	-0.00014
32	-0.00852	0.00055	-0.00567	0.00038	-0.00322	0.00023	-0.00140	0.00010	-0.00037	0.00003	-0.00004
33	-0.00763	0.00051	-0.00466	0.00033	-0.00236	0.00017	-0.00087	0.00007	-0.00018	0.00001	-0.00001
34	-0.00473	0.00032	-0.00254	0.00018	-0.00108	0.00008	-0.00031	0.00002	-0.00005	0.00000	-0.00000
35	-0.00182	0.00013	-0.00083	0.00006	-0.00028	0.00000	-0.00006	0.00000	-0.00001	0.00000	-0.00000
36	-0.00068	0.00005	-0.00026	0.00002	-0.00007	0.00001	-0.00001	0.00000	-0.00000	0.00000	-0.00000
37	-0.00034	0.00002	-0.00011	0.00001	-0.00002	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
38	-0.00009	0.00001	-0.00002	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	-0.00000
39	-0.00001	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	-0.00000
40	-0.00003	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	-0.00000
41	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	-0.00000

TABLE 5b
 PHASE VELOCITY PERTURBATIONS (IN KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY (DC/DRHO)
 AND RIGIDITY (DC/DMU) FOR GUTENBERG-BIRCH II CONTINENTAL EARTH MODEL
 GUTENBERG-BIRCH II

TISECS)	624.48	580.00	538.79	500.19	463.71	428.91
CI(K/SEC)	6.120	6.020	5.920	5.820	5.720	5.620
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU
1	-0.00996	0.00340	-0.01051	0.00370	-0.01105	0.00402
2	-0.00109	0.00043	-0.00115	0.00047	-0.00121	0.00051
3	-0.00109	0.00043	-0.00115	0.00047	-0.00121	0.00051
4	-0.00109	0.00043	-0.00115	0.00047	-0.00121	0.00051
5	-0.00109	0.00043	-0.00115	0.00047	-0.00121	0.00051
6	-0.00325	0.00123	-0.00343	0.00140	-0.00361	0.00152
7	-0.00270	0.00107	-0.00288	0.00117	-0.00299	0.00127
8	-0.00461	0.00266	-0.00486	0.00289	-0.00511	0.00314
9	-0.00326	0.00186	-0.00344	0.00203	-0.00361	0.00220
10	-0.00324	0.00184	-0.00341	0.00200	-0.00358	0.00217
11	-0.00321	0.00181	-0.00338	0.00197	-0.00352	0.00214
12	-0.00318	0.00179	-0.00335	0.00195	-0.00350	0.00211
13	-0.00316	0.00177	-0.00333	0.00193	-0.00350	0.00209
14	-0.00314	0.00176	-0.00331	0.00191	-0.00347	0.00207
15	-0.00312	0.00174	-0.00329	0.00189	-0.00345	0.00205
16	-0.00620	0.00344	-0.00652	0.00374	-0.00684	0.00405
17	-0.01223	0.00680	-0.01286	0.00739	-0.01348	0.00800
18	-0.01200	0.00672	-0.01260	0.00729	-0.01319	0.00789
19	-0.01174	0.00666	-0.01230	0.00722	-0.01285	0.00781
20	-0.01146	0.00666	-0.01199	0.00721	-0.01250	0.00778
21	-0.01117	0.00668	-0.01166	0.00722	-0.01213	0.00778
22	-0.01086	0.00672	-0.01131	0.00725	-0.01173	0.00780
23	-0.01056	0.00675	-0.01097	0.00728	-0.01134	0.00780
24	-0.01024	0.00680	-0.01061	0.00731	-0.01094	0.00782
25	-0.00992	0.00686	-0.01024	0.00735	-0.01053	0.00785
26	-0.00959	0.00688	-0.00987	0.00736	-0.01011	0.00783
27	-0.01601	0.01205	-0.01640	0.01283	-0.01670	0.01359
28	-0.02132	0.01757	-0.02167	0.01858	-0.02189	0.01953
29	-0.01937	0.01743	-0.01943	0.01834	-0.01946	0.01908
30	-0.01749	0.01722	-0.01740	0.01787	-0.01717	0.01839
31	-0.01568	0.01672	-0.01543	0.01717	-0.01503	0.01746
32	-0.01401	0.01612	-0.01361	0.01637	-0.01308	0.01643
33	-0.01824	0.02276	-0.01746	0.02276	-0.01650	0.02249
34	-0.01999	0.02796	-0.01870	0.02733	-0.01725	0.02634
35	-0.01548	0.02435	-0.01410	0.02316	-0.01261	0.02166
36	-0.01195	0.02083	-0.01058	0.01925	-0.00919	0.01744
37	-0.01290	0.02397	-0.01107	0.02144	-0.00927	0.01873
38	-0.01066	0.02185	-0.00872	0.01860	-0.00693	0.01538
39	-0.00563	0.01285	-0.00433	0.01028	-0.00322	0.00794
40	-0.00282	0.00724	-0.00203	0.00542	-0.00141	0.00389
41	-0.00135	0.00385	-0.00091	0.00268	-0.00036	0.00178
42	-0.00062	0.00195	-0.00038	0.00126	-0.00015	0.00077
43	-0.00027	0.00093	-0.00015	0.00055	-0.00008	0.00031
44	-0.00011	0.00042	-0.00006	0.00023	-0.00001	0.00012
45	-0.00004	0.00019	-0.00002	0.00009	-0.00001	0.00004
46	-0.00002	0.00008	-0.00001	0.00004	-0.00000	0.00001
47	-0.00001	0.00004	-0.00000	0.00002	-0.00000	0.00001
48	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000

TABLE 5c
PHASE VELOCITY PERTURBATIONS (IN KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY (DC/DRHO)
AND RIGIDITY (DC/DMU) FOR GUTENBERG-BIRCH II CONTINENTAL EARTH MODEL
VARIATIONS FOR 10 0/0 CHANGE IN PARAMETER
GUTENBERG BIRCH II CONTINENTAL

PSEUDO SPHERICAL CALCULATION		388.89		356.64		325.10		294.04		263.25	
T (SECS) 422.12		5.500		5.400		5.300		5.200		5.100	
C (K/SEC) 5.600											
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO
1	-0.01279	0.00518	-0.01334	0.00560	-0.01450	0.00655	-0.01513	0.00710	-0.01584	0.00773	0.00837
2	-0.00140	0.00066	-0.00146	0.00071	-0.00152	0.00076	-0.00158	0.00083	-0.00165	0.00089	0.00097
3	-0.00140	0.00065	-0.00146	0.00071	-0.00152	0.00076	-0.00158	0.00083	-0.00165	0.00089	0.00097
4	-0.00140	0.00065	-0.00146	0.00071	-0.00152	0.00076	-0.00158	0.00083	-0.00165	0.00089	0.00097
5	-0.00139	0.00065	-0.00145	0.00071	-0.00151	0.00076	-0.00157	0.00083	-0.00164	0.00089	0.00097
6	-0.00417	0.00196	-0.00434	0.00212	-0.00452	0.00229	-0.00470	0.00247	-0.00490	0.00268	0.00289
7	-0.00345	0.00163	-0.00359	0.00176	-0.00374	0.00190	-0.00389	0.00206	-0.00404	0.00223	0.00242
8	-0.00589	0.00404	-0.00613	0.00436	-0.00638	0.00470	-0.00663	0.00507	-0.00689	0.00548	0.00593
9	-0.00416	0.00283	-0.00433	0.00305	-0.00450	0.00329	-0.00467	0.00355	-0.00486	0.00383	0.00414
10	-0.00412	0.00279	-0.00429	0.00301	-0.00445	0.00324	-0.00463	0.00349	-0.00480	0.00377	0.00408
11	-0.00408	0.00274	-0.00424	0.00296	-0.00441	0.00318	-0.00457	0.00343	-0.00475	0.00370	0.00402
12	-0.00404	0.00271	-0.00420	0.00292	-0.00436	0.00314	-0.00453	0.00338	-0.00469	0.00365	0.00394
13	-0.00401	0.00268	-0.00417	0.00288	-0.00433	0.00310	-0.00449	0.00334	-0.00465	0.00360	0.00388
14	-0.00398	0.00265	-0.00414	0.00285	-0.00430	0.00307	-0.00444	0.00330	-0.00460	0.00355	0.00383
15	-0.00395	0.00262	-0.00410	0.00282	-0.00425	0.00305	-0.00440	0.00326	-0.00456	0.00351	0.00378
16	-0.00782	0.00517	-0.00812	0.00556	-0.00841	0.00598	-0.00870	0.00642	-0.00899	0.00690	0.00742
17	-0.01535	0.01019	-0.01591	0.01094	-0.01645	0.01174	-0.01698	0.01258	-0.01751	0.01348	0.01446
18	-0.01493	0.01030	-0.01543	0.01072	-0.01591	0.01146	-0.01637	0.01225	-0.01681	0.01307	0.01395
19	-0.01445	0.00983	-0.01489	0.01051	-0.01530	0.01121	-0.01568	0.01193	-0.01630	0.01268	0.01345
20	-0.01394	0.00973	-0.01431	0.01037	-0.01466	0.01103	-0.01496	0.01169	-0.01521	0.01235	0.01302
21	-0.01339	0.00965	-0.01371	0.01025	-0.01397	0.01085	-0.01419	0.01151	-0.01434	0.01203	0.01259
22	-0.01283	0.00959	-0.01307	0.01014	-0.01326	0.01069	-0.01339	0.01122	-0.01345	0.01171	0.01216
23	-0.01226	0.00950	-0.01244	0.01001	-0.01255	0.01050	-0.01260	0.01095	-0.01256	0.01136	0.01169
24	-0.01167	0.00942	-0.01178	0.00988	-0.01183	0.01031	-0.01179	0.01068	-0.01167	0.01099	0.01121
25	-0.01109	0.00934	-0.01113	0.00975	-0.01111	0.01011	-0.01100	0.01041	-0.01079	0.01062	0.01072
26	-0.01050	0.00920	-0.01048	0.00956	-0.01039	0.00985	-0.01021	0.01007	-0.00993	0.01018	0.01017
27	-0.01000	0.00910	-0.01004	0.00918	-0.01003	0.00953	-0.01002	0.00972	-0.01002	0.01071	0.01043
28	-0.02152	0.02184	-0.02103	0.02222	-0.02034	0.02237	-0.01941	0.02223	-0.01823	0.02173	0.02082
29	-0.01831	0.02047	-0.01758	0.02048	-0.01665	0.02021	-0.01552	0.02023	-0.01417	0.01867	0.01728
30	-0.01540	0.01886	-0.01451	0.01852	-0.01344	0.01790	-0.01221	0.01765	-0.01081	0.01564	0.01395
31	-0.01281	0.01706	-0.01182	0.01643	-0.01070	0.01581	-0.00946	0.01530	-0.00810	0.01428	0.01195
32	-0.01028	0.01525	-0.00954	0.01438	-0.00842	0.01325	-0.00723	0.01187	-0.00598	0.01025	0.00843
33	-0.01455	0.01955	-0.01094	0.01795	-0.00956	0.01605	-0.00773	0.01397	-0.00614	0.01147	0.00845
34	-0.01178	0.02372	-0.00994	0.01827	-0.00812	0.01539	-0.00636	0.01276	-0.00472	0.00989	0.00712
35	-0.00761	0.01506	-0.00611	0.01264	-0.00471	0.01018	-0.00344	0.00778	-0.00235	0.00536	0.00362
36	-0.00489	0.01067	-0.00373	0.00850	-0.00270	0.00644	-0.00184	0.00458	-0.00115	0.00330	0.00176
37	-0.00428	0.00987	-0.00308	0.00740	-0.00208	0.00522	-0.00131	0.00342	-0.00075	0.00293	0.00135
38	-0.00258	0.00650	-0.00170	0.00445	-0.00104	0.00283	-0.00058	0.00164	-0.00029	0.00084	0.00037
39	-0.00091	0.00253	-0.00054	0.00155	-0.00029	0.00086	-0.00014	0.00043	-0.00006	0.00018	0.00006
40	-0.00030	0.00092	-0.00015	0.00050	-0.00007	0.00024	-0.00003	0.00010	-0.00001	0.00003	0.00001
41	-0.00009	0.00031	-0.00004	0.00015	-0.00002	0.00006	-0.00001	0.00002	-0.00000	0.00001	0.00000
42	-0.00002	0.00009	-0.00001	0.00004	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	0.00000
43	-0.00001	0.00003	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000
44	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000
45	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000
46	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000
47	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000
48	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	0.00000

TISECS)	232.54	201.79	170.93	140.07	109.70	81.33	4,500	
							DC/DRHO	DC/DMU
M	DC/DRHO	DC/DRHO	DC/DRHO	DC/DRHO	DC/DRHO	DC/DRHO	DC/DRHO	DC/DRHO
1	-0.01667	0.03846	-0.01772	0.00337	-0.01915	0.01056	-0.02128	0.01225
2	-0.00182	0.00107	-0.00193	0.00118	-0.00208	0.00133	-0.00230	0.00153
3	-0.00181	0.00107	-0.00192	0.00118	-0.00207	0.00132	-0.00228	0.00153
4	-0.00181	0.00106	-0.00191	0.00118	-0.00206	0.00132	-0.00227	0.00152
5	-0.00180	0.00106	-0.00191	0.00117	-0.00205	0.00132	-0.00225	0.00152
6	-0.00536	0.00318	-0.00567	0.00351	-0.00608	0.00394	-0.00666	0.00452
7	-0.03442	0.00264	-0.00466	0.00291	-0.00498	0.00325	-0.00542	0.00373
8	-0.00751	0.00646	-0.00790	0.00709	-0.00842	0.00788	-0.00912	0.00894
9	-0.00528	0.00451	-0.00555	0.00494	-0.00590	0.00548	-0.00637	0.00618
10	-0.00521	0.00443	-0.00547	0.00485	-0.00536	0.00536	-0.00624	0.00624
11	-0.00514	0.00434	-0.00539	0.00474	-0.00531	0.00524	-0.00612	0.00587
12	-0.00508	0.00427	-0.00532	0.00466	-0.00526	0.00513	-0.00600	0.00574
13	-0.00502	0.00420	-0.00525	0.00458	-0.00523	0.00503	-0.00589	0.00560
14	-0.00496	0.00415	-0.00518	0.00451	-0.00514	0.00494	-0.00577	0.00548
15	-0.00490	0.00408	-0.00511	0.00443	-0.00515	0.00485	-0.00566	0.00536
16	-0.00963	0.00800	-0.01091	0.00867	-0.01046	0.00945	-0.01100	0.00966
17	-0.01862	0.01553	-0.01925	0.01672	-0.01996	0.01808	-0.02073	0.01963
18	-0.01489	0.01489	-0.01813	0.01590	-0.01968	0.01699	-0.01897	0.01812
19	-0.01665	0.01425	-0.01691	0.01507	-0.01710	0.01589	-0.01712	0.01661
20	-0.01577	0.01368	-0.01544	0.01432	-0.01559	0.01487	-0.01527	0.01521
21	-0.01444	0.01311	-0.01434	0.01356	-0.01465	0.01385	-0.01344	0.01382
22	-0.01330	0.01253	-0.01303	0.01279	-0.01254	0.01282	-0.01168	0.01246
23	-0.01218	0.01192	-0.01176	0.01198	-0.01109	0.01178	-0.01004	0.01112
24	-0.01107	0.01129	-0.01052	0.01117	-0.00971	0.01075	-0.00851	0.00983
25	-0.01000	0.01066	-0.00934	0.01038	-0.00843	0.00976	-0.00715	0.00863
26	-0.00897	0.00998	-0.00823	0.00954	-0.00725	0.00875	-0.00593	0.00747
27	-0.01346	0.01580	-0.01204	0.01472	-0.01023	0.01304	-0.00796	0.01058
28	-0.01499	0.01938	-0.01284	0.01729	-0.01029	0.01444	-0.00736	0.01076
29	-0.01078	0.01540	-0.00872	0.01298	-0.00647	0.01003	-0.00414	0.00668
30	-0.00756	0.01186	-0.00575	0.00941	-0.00392	0.00668	-0.00222	0.00394
31	-0.00517	0.00886	-0.00369	0.00658	-0.00230	0.00428	-0.00155	0.00246
32	-0.00347	0.00647	-0.00231	0.00468	-0.00131	0.00265	-0.00097	0.00129
33	-0.00316	0.00642	-0.00193	0.00408	-0.00098	0.00215	-0.00036	0.00082
34	-0.00203	0.00463	-0.00109	0.00259	-0.00047	0.00114	-0.00013	0.00007
35	-0.00081	0.00207	-0.00037	0.00098	-0.00012	0.00035	-0.00003	0.00000
36	-0.00031	0.00088	-0.00012	0.00035	-0.00003	0.00010	-0.00000	0.00000
37	-0.00015	0.00045	-0.					

TABLE 6a
PERIOD (*T*), PHASE VELOCITY (*c*) AND VARIATIONAL PARTIAL DERIVATIVES FOR CIT13F OCEANIC
EARTH MODEL

CIT13F OCEANIC												
PSEUDO SPHERICAL CALCULATION												
899.29												
6.620												
818.64												
6.520												
753.04												
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TABLE 6b
PERIOD (T), PHASE VELOCITY (c) AND VARIATIONAL PARTIAL DERIVATIVES FOR CIT13F OCEANIC
EARTH MODEL

CIT 13F OCEANIC		560.79		522.28		486.02		451.55		418.48	
T(SEC)		602.14		592.0		582.0		572.0		562.0	
C/K/SEC		6.120		6.020		5.920		5.820		5.720	
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDMU
1	-0.00101	0.00003	-0.00106	0.00003	-0.00111	0.00003	-0.00117	0.00003	-0.00122	0.00004	-0.00126
2	-0.00403	0.00011	-0.00424	0.00012	-0.00445	0.00013	-0.00466	0.00014	-0.00486	0.00015	-0.00505
3	-0.01005	0.00027	-0.01059	0.00029	-0.01111	0.00032	-0.01162	0.00035	-0.01212	0.00037	-0.01260
4	-0.01802	0.00049	-0.01898	0.00053	-0.01991	0.00057	-0.02083	0.00062	-0.02172	0.00067	-0.02258
5	-0.02996	0.00072	-0.03104	0.00079	-0.03209	0.00083	-0.03311	0.00088	-0.03400	0.00093	-0.03490
6	-0.04692	0.00127	-0.04844	0.00136	-0.04996	0.00146	-0.05146	0.00156	-0.05292	0.00166	-0.05440
7	-0.07194	0.00254	-0.07378	0.00268	-0.07562	0.00282	-0.07746	0.00296	-0.07930	0.00310	-0.08114
8	-0.09905	0.00407	-0.10109	0.00429	-0.10313	0.00451	-0.10517	0.00473	-0.10721	0.00495	-0.10925
9	-0.13832	0.00616	-0.14030	0.00638	-0.14228	0.00660	-0.14426	0.00682	-0.14624	0.00704	-0.14822
10	-0.17572	0.00865	-0.17769	0.00887	-0.17967	0.00909	-0.18165	0.00931	-0.18363	0.00953	-0.18561
11	-0.21312	0.01114	-0.21509	0.01136	-0.21707	0.01158	-0.21905	0.01180	-0.22103	0.01202	-0.22301
12	-0.25052	0.01363	-0.25249	0.01385	-0.25447	0.01407	-0.25645	0.01429	-0.25843	0.01451	-0.26041
13	-0.28792	0.01612	-0.28989	0.01634	-0.29187	0.01656	-0.29385	0.01678	-0.29583	0.01700	-0.29781
14	-0.32532	0.01861	-0.32729	0.01883	-0.32927	0.01905	-0.33125	0.01927	-0.33323	0.01949	-0.33521
15	-0.36272	0.02110	-0.36469	0.02132	-0.36667	0.02154	-0.36865	0.02176	-0.37063	0.02198	-0.37261
16	-0.40012	0.02359	-0.40209	0.02381	-0.40407	0.02403	-0.40605	0.02425	-0.40803	0.02447	-0.41001
17	-0.43752	0.02608	-0.43949	0.02630	-0.44147	0.02652	-0.44345	0.02674	-0.44543	0.02696	-0.44741
18	-0.47492	0.02857	-0.47689	0.02879	-0.47887	0.02901	-0.48085	0.02923	-0.48283	0.02945	-0.48481
19	-0.51232	0.03106	-0.51429	0.03128	-0.51627	0.03150	-0.51825	0.03172	-0.52023	0.03194	-0.52221
20	-0.54972	0.03355	-0.55169	0.03377	-0.55367	0.03399	-0.55565	0.03421	-0.55763	0.03443	-0.55961
21	-0.58712	0.03604	-0.58909	0.03626	-0.59107	0.03648	-0.59305	0.03670	-0.59503	0.03692	-0.59701
22	-0.62452	0.03853	-0.62649	0.03875	-0.62847	0.03897	-0.63045	0.03919	-0.63243	0.03941	-0.63441
23	-0.66192	0.04102	-0.66389	0.04124	-0.66587	0.04146	-0.66785	0.04168	-0.66983	0.04190	-0.67181
24	-0.69932	0.04351	-0.70129	0.04373	-0.70327	0.04395	-0.70525	0.04417	-0.70723	0.04439	-0.70921
25	-0.73672	0.04600	-0.73869	0.04622	-0.74067	0.04644	-0.74265	0.04666	-0.74463	0.04688	-0.74661
26	-0.77412	0.04849	-0.77609	0.04871	-0.77807	0.04893	-0.78005	0.04915	-0.78203	0.04937	-0.78401
27	-0.81152	0.05098	-0.81349	0.05120	-0.81547	0.05142	-0.81745	0.05164	-0.81943	0.05186	-0.82141
28	-0.84892	0.05347	-0.85089	0.05369	-0.85287	0.05391	-0.85485	0.05413	-0.85683	0.05435	-0.85881
29	-0.88632	0.05596	-0.88829	0.05618	-0.89027	0.05640	-0.89225	0.05662	-0.89423	0.05684	-0.89621
30	-0.92372	0.05845	-0.92569	0.05867	-0.92767	0.05889	-0.92965	0.05911	-0.93163	0.05933	-0.93361
31	-0.96112	0.06094	-0.96309	0.06116	-0.96507	0.06138	-0.96705	0.06160	-0.96903	0.06182	-0.97101
32	-0.99852	0.06343	-0.99999	0.06365	-1.00197	0.06387	-1.00395	0.06409	-1.00593	0.06431	-1.00791
33	-1.03592	0.06592	-1.03789	0.06614	-1.03987	0.06636	-1.04185	0.06658	-1.04383	0.06680	-1.04581
34	-1.07332	0.06841	-1.07529	0.06863	-1.07727	0.06885	-1.07925	0.06907	-1.08123	0.06929	-1.08321
35	-1.11072	0.07090	-1.11269	0.07112	-1.11467	0.07134	-1.11665	0.07156	-1.11863	0.07178	-1.12061
36	-1.14812	0.07339	-1.15009	0.07361	-1.15207	0.07383	-1.15405	0.07405	-1.15603	0.07425	-1.15801
37	-1.18552	0.07588	-1.18749	0.07610	-1.18947	0.07632	-1.19145	0.07654	-1.19343	0.07676	-1.19541
38	-1.22292	0.07837	-1.22489	0.07859	-1.22687	0.07881	-1.22885	0.07903	-1.23083	0.07925	-1.23281
39	-1.26032	0.08086	-1.26229	0.08108	-1.26427	0.08130	-1.26625	0.08152	-1.26823	0.08174	-1.27021
40	-1.29772	0.08335	-1.29969	0.08357	-1.30167	0.08379	-1.30365	0.08401	-1.30563	0.08423	-1.30761
41	-1.33512	0.08584	-1.33709	0.08606	-1.33907	0.08628	-1.34105	0.08650	-1.34303	0.08672	-1.34501
42	-1.37252	0.08833	-1.37449	0.08855	-1.37647	0.08877	-1.37845	0.08899	-1.38043	0.08921	-1.38241
43	-1.40992	0.09082	-1.41189	0.09104	-1.41387	0.09126	-1.41585	0.09148	-1.41783	0.09170	-1.41981
44	-1.44732	0.09331	-1.44929	0.09353	-1.45127	0.09375	-1.45325	0.09397	-1.45523	0.09419	-1.45721
45	-1.48472	0.09580	-1.48669	0.09602	-1.48867	0.09624	-1.49065	0.09646	-1.49263	0.09668	-1.49461
46	-1.52212	0.09829	-1.52409	0.09851	-1.52607	0.09873	-1.52805	0.09895	-1.53003	0.09917	-1.53201

TABLE 6c
PERIOD (T), PHASE VELOCITY (c) AND VARIATIONAL PARTIAL DERIVATIVES FOR CIT13F OCEANIC EARTH MODEL

[illegible]

TABLE 7a
PHASE VELOCITY PERTURBATIONS (IN KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY (DC/DRHO) AND RIGIDITY (DC/DMU) FOR CITH3F OCEANIC EARTH MODEL
VARIATIONS FOR 10 070 CHANGE IN PARAMETER
CITH3F OCEANIC

PSEUDO SPHERICAL CALCULATION		899.29		818.64		753.04		696.84		647.11	
T(SEC) 1009.06		6.620		6.520		6.420		6.320		6.220	
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO
1	-0.00012	0.00000	-0.00013	0.00000	-0.00016	0.00000	-0.00017	0.00000	-0.00018	0.00000	0.00000
2	-0.00064	0.00012	-0.00072	0.00014	-0.00079	0.00016	-0.00085	0.00017	-0.00091	0.00019	0.00097
3	-0.00183	0.00057	-0.00206	0.00066	-0.00225	0.00074	-0.00242	0.00082	-0.00259	0.00090	0.00276
4	-0.00377	0.00182	-0.00422	0.00209	-0.00461	0.00235	-0.00498	0.00266	-0.00534	0.00286	0.00566
5	-0.00208	0.00101	-0.00233	0.00116	-0.00255	0.00130	-0.00275	0.00144	-0.00294	0.00159	0.00314
6	-0.00208	0.00099	-0.00233	0.00114	-0.00255	0.00128	-0.00275	0.00142	-0.00294	0.00156	0.00312
7	-0.00415	0.00190	-0.00465	0.00218	-0.00508	0.00245	-0.00548	0.00271	-0.00586	0.00299	0.00623
8	-0.00826	0.00371	-0.00925	0.00425	-0.01010	0.00477	-0.01090	0.00529	-0.01165	0.00582	-0.01237
9	-0.00819	0.00371	-0.00917	0.00426	-0.01001	0.00478	-0.01079	0.00530	-0.01153	0.00583	-0.01224
10	-0.00810	0.00371	-0.00905	0.00425	-0.00988	0.00477	-0.01064	0.00529	-0.01136	0.00581	-0.01205
11	-0.00801	0.00371	-0.00894	0.00426	-0.00975	0.00477	-0.01049	0.00529	-0.01118	0.00581	-0.01185
12	-0.00789	0.00371	-0.00881	0.00425	-0.00959	0.00477	-0.01031	0.00528	-0.01098	0.00580	-0.01162
13	-0.00778	0.00377	-0.00866	0.00432	-0.00942	0.00484	-0.01011	0.00536	-0.01075	0.00588	-0.01137
14	-0.00767	0.00383	-0.00853	0.00439	-0.00926	0.00491	-0.00992	0.00544	-0.01053	0.00596	-0.01112
15	-0.00754	0.00387	-0.00837	0.00443	-0.00907	0.00496	-0.00970	0.00548	-0.01029	0.00601	-0.01084
16	-0.00741	0.00391	-0.00821	0.00447	-0.00888	0.00500	-0.00948	0.00552	-0.01003	0.00604	-0.01054
17	-0.00728	0.00391	-0.00805	0.00446	-0.00869	0.00499	-0.00926	0.00550	-0.00977	0.00601	-0.01025
18	-0.00714	0.00390	-0.00787	0.00445	-0.00848	0.00497	-0.00902	0.00548	-0.00950	0.00597	-0.00993
19	-0.00699	0.00391	-0.00769	0.00447	-0.00827	0.00498	-0.00877	0.00547	-0.00921	0.00597	-0.00961
20	-0.00686	0.00391	-0.00752	0.00445	-0.00806	0.00496	-0.00852	0.00547	-0.00893	0.00593	-0.00929
21	-0.00669	0.00389	-0.00732	0.00443	-0.00782	0.00493	-0.00825	0.00545	-0.00861	0.00587	-0.00893
22	-0.00655	0.00390	-0.00713	0.00444	-0.00760	0.00493	-0.00799	0.00540	-0.00832	0.00585	-0.00859
23	-0.00639	0.00389	-0.00694	0.00442	-0.00737	0.00490	-0.00771	0.00535	-0.00800	0.00579	-0.00824
24	-0.01235	0.00775	-0.01334	0.00878	-0.01409	0.00972	-0.01468	0.01060	-0.01514	0.01143	-0.01550
25	-0.01465	0.00974	-0.01567	0.01100	-0.01640	0.01211	-0.01693	0.01314	-0.01730	0.01409	-0.01753
26	-0.02834	0.00197	-0.03000	0.00221	-0.03031	0.00242	-0.03119	0.00261	-0.03323	0.00279	-0.03325
27	-0.02834	0.02599	-0.02983	0.02811	-0.03073	0.03021	-0.03122	0.03200	-0.03136	0.03353	-0.03121
28	-0.02567	0.02530	-0.02652	0.02733	-0.02683	0.02889	-0.02676	0.03008	-0.02637	0.03094	-0.02571
29	-0.02289	0.02555	-0.02318	0.02706	-0.02301	0.02802	-0.02251	0.03008	-0.02637	0.03094	-0.02571
30	-0.02023	0.02436	-0.02007	0.02528	-0.01993	0.02569	-0.02251	0.02860	-0.02173	0.02881	-0.02072
31	-0.01740	0.02316	-0.01691	0.02352	-0.01612	0.02342	-0.01512	0.02571	-0.01769	0.02537	-0.01650
32	-0.02866	0.04260	-0.02704	0.04193	-0.02507	0.04031	-0.02287	0.03849	-0.02052	0.03596	-0.01810
33	-0.02055	0.03440	-0.01851	0.03233	-0.01641	0.02987	-0.01431	0.02711	-0.01224	0.02415	-0.01027
34	-0.01438	0.02702	-0.01231	0.02413	-0.01040	0.02183	-0.00863	0.01834	-0.00701	0.01551	-0.00557
35	-0.00983	0.02046	-0.00797	0.01730	-0.00639	0.01444	-0.00503	0.01182	-0.00387	0.00946	-0.00290
36	-0.00501	0.01145	-0.00385	0.00916	-0.00292	0.00725	-0.00218	0.00563	-0.00158	0.00426	-0.00112
37	-0.00248	0.00606	-0.00182	0.00464	-0.00133	0.00353	-0.00069	0.00202	-0.00066	0.00190	-0.00044
38	-0.00200	0.00514	-0.00140	0.00381	-0.00100	0.00280	-0.00095	0.00202	-0.00046	0.00141	-0.00030
39	-0.00160	0.00434	-0.00110	0.00311	-0.00075	0.00221	-0.00050	0.00154	-0.00033	0.00104	-0.00020
40	-0.00103	0.00309	-0.00086	0.00266	-0.00042	0.00137	-0.00026	0.00089	-0.00016	0.00056	-0.00009
41	-0.00082	0.00261	-0.00051	0.00168	-0.00032	0.00108	-0.00019	0.00067	-0.00011	0.00041	-0.00006
42	-0.00066	0.00222	-0.00040	0.00139	-0.00024	0.00086	-0.00014	0.00052	-0.00008	0.00030	-0.00004
43	-0.00054	0.00191	-0.00032	0.00116	-0.00019	0.00041	-0.00006	0.00041	-0.00006	0.00023	-0.00003
44	-0.00067	0.00257	-0.00039	0.00153	-0.00022	0.00090	-0.00012	0.00051	-0.00006	0.00028	-0.00003
45	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
46	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000

TABLE 7b
PHASE VELOCITY PERTURBATIONS (IN KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY (DC/DRHO) AND RIGIDITY (DC/DMU) FOR CIT13F OCEANIC EARTH MODEL

CIT 13F OCEANIC		560.79		522.28		486.02		451.55		418.48	
T (SECS)		602.14		592.00		582.00		572.00		562.00	
C (KM/SEC)		6.120		6.020		5.920		5.820		5.720	
N	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO
1	-0.00019	0.00000	-0.00020	0.00000	-0.00021	0.00000	-0.00022	0.00000	-0.00023	0.00000	-0.00024
2	-0.00102	0.00023	-0.00108	0.00025	-0.00113	0.00029	-0.00118	0.00031	-0.00123	0.00034	-0.00128
3	-0.00292	0.00108	-0.00307	0.00117	-0.00322	0.00127	-0.00337	0.00137	-0.00352	0.00148	-0.00365
4	-0.00598	0.00342	-0.00630	0.00372	-0.00661	0.00403	-0.00692	0.00436	-0.00721	0.00470	-0.00750
5	-0.00331	0.00190	-0.00349	0.00206	-0.00366	0.00224	-0.00383	0.00238	-0.00399	0.00256	-0.00415
6	-0.00330	0.00187	-0.00348	0.00203	-0.00365	0.00220	-0.00382	0.00238	-0.00398	0.00256	-0.00414
7	-0.00658	0.00357	-0.00693	0.00388	-0.00727	0.00420	-0.00760	0.00454	-0.00793	0.00490	-0.00824
8	-0.01308	0.00696	-0.01376	0.00756	-0.01443	0.00819	-0.01509	0.00885	-0.01572	0.00954	-0.01633
9	-0.01293	0.00696	-0.01360	0.00755	-0.01425	0.00818	-0.01489	0.00883	-0.01550	0.00952	-0.01608
10	-0.01272	0.00694	-0.01336	0.00753	-0.01399	0.00814	-0.01460	0.00879	-0.01518	0.00945	-0.01573
11	-0.01250	0.00692	-0.01312	0.00751	-0.01371	0.00811	-0.01429	0.00874	-0.01484	0.00939	-0.01535
12	-0.01224	0.00689	-0.01282	0.00747	-0.01339	0.00806	-0.01393	0.00868	-0.01443	0.00931	-0.01491
13	-0.01195	0.00698	-0.01250	0.00755	-0.01303	0.00813	-0.01353	0.00874	-0.01439	0.00936	-0.01442
14	-0.01167	0.00706	-0.01218	0.00762	-0.01267	0.00820	-0.01313	0.00880	-0.01354	0.00940	-0.01392
15	-0.01135	0.00709	-0.01183	0.00764	-0.01227	0.00821	-0.01268	0.00879	-0.01305	0.00936	-0.01337
16	-0.01102	0.00711	-0.01145	0.00765	-0.01186	0.00820	-0.01222	0.00876	-0.01254	0.00931	-0.01281
17	-0.01069	0.00705	-0.01108	0.00758	-0.01144	0.00810	-0.01176	0.00863	-0.01203	0.00914	-0.01224
18	-0.01033	0.00698	-0.01068	0.00748	-0.01099	0.00798	-0.01126	0.00848	-0.01148	0.00896	-0.01164
19	-0.00996	0.00695	-0.01027	0.00743	-0.01054	0.00791	-0.01075	0.00837	-0.01092	0.00881	-0.01102
20	-0.00960	0.00687	-0.00986	0.00733	-0.01008	0.00778	-0.01025	0.00821	-0.01036	0.00861	-0.01041
21	-0.00920	0.00678	-0.00942	0.00721	-0.00959	0.00763	-0.00971	0.00802	-0.00977	0.00838	-0.00977
22	-0.00882	0.00673	-0.00900	0.00714	-0.00912	0.00752	-0.00919	0.00788	-0.00920	0.00820	-0.00915
23	-0.00842	0.00662	-0.00856	0.00701	-0.00883	0.00736	-0.00866	0.00769	-0.00862	0.00796	-0.00852
24	-0.01575	0.01297	-0.01589	0.01366	-0.01592	0.01428	-0.01584	0.01482	-0.01564	0.01525	-0.01531
25	-0.01762	0.01578	-0.01757	0.01648	-0.01738	0.01708	-0.01705	0.01754	-0.01657	0.01784	-0.01594
26	-0.00323	0.00309	-0.00319	0.00320	-0.00312	0.00329	-0.00303	0.00335	-0.00290	0.00338	-0.00275
27	-0.03077	0.03578	-0.03003	0.03644	-0.02902	0.03674	-0.02775	0.03667	-0.02622	0.03615	-0.02442
28	-0.02478	0.03169	-0.02360	0.03152	-0.02221	0.03097	-0.02061	0.03002	-0.01883	0.02864	-0.01689
29	-0.01950	0.02816	-0.01810	0.02728	-0.01655	0.02604	-0.01488	0.02444	-0.01311	0.02250	-0.01130
30	-0.01515	0.02367	-0.01369	0.02232	-0.01215	0.02069	-0.01057	0.01880	-0.00898	0.01668	-0.00742
31	-0.01139	0.01964	-0.01001	0.01801	-0.00861	0.01618	-0.00721	0.01420	-0.00592	0.01212	-0.00468
32	-0.01566	0.02976	-0.01326	0.02823	-0.01096	0.02256	-0.00881	0.01887	-0.00685	0.01527	-0.00512
33	-0.00841	0.01797	-0.00671	0.01691	-0.00519	0.01200	-0.00388	0.00932	-0.00278	0.00694	-0.00189
34	-0.00430	0.01029	-0.00322	0.00800	-0.00232	0.00600	-0.00161	0.00430	-0.00105	0.00293	-0.00065
35	-0.00210	0.00555	-0.00147	0.00403	-0.00098	0.00280	-0.00063	0.00185	-0.00037	0.00115	-0.00021
36	-0.00076	0.00221	-0.00049	0.00150	-0.00031	0.00096	-0.00018	0.00059	-0.00010	0.00033	-0.00005
37	-0.00029	0.00090	-0.00018	0.00058	-0.00010	0.00035	-0.00006	0.00020	-0.00003	0.00010	-0.00001
38	-0.00019	0.00062	-0.00011	0.00038	-0.00006	0.00022	-0.00003	0.00012	-0.00002	0.00006	-0.00001
39	-0.00012	0.00042	-0.00007	0.00025	-0.00004	0.00014	-0.00002	0.00007	-0.00001	0.00003	-0.00000
40	-0.00008	0.00028	-0.00004	0.00016	-0.00002	0.00008	-0.00001	0.00004	-0.00000	0.00002	-0.00000
41	-0.00005	0.00019	-0.00003	0.00010	-0.00001	0.00005	-0.00001	0.00002	-0.00000	0.00001	-0.00000
42	-0.00003	0.00013	-0.00002	0.00007	-0.00001	0.00003	-0.00000	0.00001	-0.00000	0.00001	-0.00000
43	-0.00002	0.00009	-0.00001	0.00004	-0.00000	0.00002	-0.00000	0.00001	-0.00000	0.00000	-0.00000
44	-0.00001	0.00006	-0.00001	0.00003	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000
45	-0.00001	0.00007	-0.00001	0.00003	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000
46	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000

TABLE 7c
PHASE VELOCITY PERTURBATIONS (IN KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY (DC/DRHO) AND
RIGIDITY (DC/DMU) FOR CIT13F OCEANIC EARTH MODEL
VARIATIONS FOR 10 0/0 CHANGE IN PARAMETER
CIT13F OCEANIC

PSEUDO SPHERICAL CALCULATION		380.15		348.98		318.19		287.45		256.41	
T(SEC) 412.00		5.500		5.400		5.300		5.200		5.132	
C1K/SEC 5.600											
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO
1	-0.00024	0.00000	-0.00025	0.00001	-0.00026	0.00001	-0.00027	0.00001	-0.00028	0.00001	-0.00028
2	-0.00129	0.00034	-0.00134	0.00037	-0.00139	0.00040	-0.00143	0.00042	-0.00147	0.00045	-0.00152
3	-0.00368	0.00162	-0.00382	0.00174	-0.00395	0.00186	-0.00407	0.00199	-0.00420	0.00213	-0.00433
4	-0.00755	0.00514	-0.00783	0.00551	-0.00809	0.00591	-0.00835	0.00633	-0.00860	0.00677	-0.00886
5	-0.00418	0.00285	-0.00433	0.00306	-0.00447	0.00328	-0.00462	0.00351	-0.00476	0.00375	-0.00490
6	-0.00617	0.00280	-0.00642	0.00320	-0.00666	0.00362	-0.00690	0.00404	-0.00714	0.00446	-0.00738
7	-0.00830	0.00335	-0.00860	0.00374	-0.00888	0.00415	-0.00916	0.00458	-0.00943	0.00500	-0.00971
8	-0.01645	0.01040	-0.01703	0.01116	-0.01759	0.01195	-0.01812	0.01277	-0.01864	0.01364	-0.01917
9	-0.01620	0.01037	-0.01675	0.01111	-0.01728	0.01188	-0.01778	0.01268	-0.01826	0.01352	-0.01873
10	-0.01584	0.01029	-0.01636	0.01101	-0.01684	0.01175	-0.01730	0.01252	-0.01772	0.01332	-0.01814
11	-0.01545	0.01020	-0.01593	0.01090	-0.01637	0.01161	-0.01677	0.01234	-0.01713	0.01308	-0.01747
12	-0.01500	0.01009	-0.01542	0.01075	-0.01581	0.01142	-0.01615	0.01210	-0.01644	0.01278	-0.01669
13	-0.01450	0.01011	-0.01487	0.01073	-0.01520	0.01113	-0.01547	0.01182	-0.01569	0.01245	-0.01585
14	-0.01399	0.01012	-0.01431	0.01073	-0.01457	0.01117	-0.01477	0.01191	-0.01491	0.01247	-0.01498
15	-0.01343	0.01005	-0.01369	0.01062	-0.01389	0.01117	-0.01403	0.01169	-0.01409	0.01217	-0.01427
16	-0.01285	0.00996	-0.01306	0.01048	-0.01319	0.01097	-0.01326	0.01143	-0.01324	0.01183	-0.01314
17	-0.01228	0.00974	-0.01242	0.01021	-0.01249	0.01064	-0.01249	0.01112	-0.01240	0.01154	-0.01221
18	-0.01166	0.00950	-0.01175	0.00991	-0.01176	0.01028	-0.01169	0.01059	-0.01153	0.01081	-0.01127
19	-0.01104	0.00930	-0.01106	0.00966	-0.01101	0.00997	-0.01088	0.01020	-0.01066	0.01034	-0.01032
20	-0.01042	0.00904	-0.01039	0.00935	-0.01028	0.00958	-0.01009	0.00974	-0.00980	0.00979	-0.00941
21	-0.00976	0.00875	-0.00968	0.00900	-0.00952	0.00917	-0.00927	0.00925	-0.00893	0.00922	-0.00849
22	-0.00913	0.00852	-0.00900	0.00871	-0.00879	0.00881	-0.00869	0.00882	-0.00811	0.00872	-0.00761
23	-0.00849	0.00821	-0.00831	0.00835	-0.00805	0.00839	-0.00772	0.00833	-0.00729	0.00815	-0.00677
24	-0.01522	0.01559	-0.01473	0.01569	-0.01410	0.01561	-0.01332	0.01530	-0.01238	0.01473	-0.01126
25	-0.01580	0.01794	-0.01499	0.01779	-0.01403	0.01737	-0.01290	0.01657	-0.01163	0.01564	-0.01019
26	-0.00272	0.00335	-0.00253	0.00328	-0.00232	0.00316	-0.00208	0.00298	-0.00182	0.00273	-0.00154
27	-0.02404	0.03490	-0.02196	0.03329	-0.01967	0.03113	-0.01720	0.02841	-0.01458	0.02512	-0.01184
28	-0.01649	0.02643	-0.01441	0.02413	-0.01226	0.02144	-0.01009	0.01841	-0.00794	0.01513	-0.00588
29	-0.01093	0.01976	-0.00911	0.01720	-0.00733	0.01446	-0.00565	0.01143	-0.00240	0.00882	-0.00075
30	-0.00712	0.01393	-0.00563	0.01154	-0.00429	0.00916	-0.00309	0.00688	-0.00206	0.00480	-0.00125
31	-0.00444	0.00959	-0.00353	0.00755	-0.00239	0.00564	-0.00160	0.00394	-0.00098	0.00252	-0.00053
32	-0.00440	0.01123	-0.00338	0.00824	-0.00224	0.00567	-0.00137	0.00360	-0.00075	0.00236	-0.00036
33	-0.00174	0.00455	-0.00110	0.00299	-0.00064	0.00181	-0.00034	0.00098	-0.00015	0.00046	-0.00006
34	-0.00058	0.00170	-0.00033	0.00099	-0.00017	0.00052	-0.00007	0.00024	-0.00003	0.00009	-0.00001
35	-0.00018	0.00058	-0.00009	0.00030	-0.00004	0.00014	-0.00001	0.00005	-0.00000	0.00002	-0.00000
36	-0.00004	0.00015	-0.00002	0.00007	-0.00001	0.00003	-0.00000	0.00001	-0.00000	0.00000	-0.00000
37	-0.00001	0.00004	-0.00000	0.00002	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000
38	-0.00001	0.00002	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
39	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
40	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
41	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
42	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
43	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
44	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
45	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000
46	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000

TABLE 7d
PHASE VELOCITY PERTURBATIONS (IN KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY (DC/DRHO) AND RIGIDITY (DC/DMU)
FOR CIT13F OCEANIC EARTH MODEL

CIT 13F	OCEANIC		191.71 4.900	156.82 4.800	119.10 4.700	78.14 4.600	38.58 4.500
	T (SECS)	C (K/SEC)					
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO
1	-0.00029	0.00001	-0.00031	0.00001	-0.00035	0.00001	-0.00043
2	-0.00157	0.00052	-0.00163	0.00056	-0.00189	0.00071	-0.00230
3	-0.00447	0.00245	-0.00464	0.00265	-0.00536	0.00333	-0.00651
4	-0.00915	0.00779	-0.00950	0.00842	-0.01094	0.01053	-0.01318
5	-0.00505	0.00431	-0.00525	0.00466	-0.00551	0.00581	-0.00721
6	-0.00504	0.00423	-0.00522	0.00457	-0.00549	0.00550	-0.00708
7	-0.01001	0.00807	-0.01037	0.00871	-0.01090	0.00953	-0.01337
8	-0.01973	0.01561	-0.02042	0.01681	-0.02138	0.01834	-0.02521
9	-0.01923	0.01539	-0.01982	0.01651	-0.02065	0.01791	-0.02377
10	-0.01856	0.01505	-0.01903	0.01606	-0.01967	0.01729	-0.02191
11	-0.01779	0.01466	-0.01814	0.01555	-0.01858	0.01657	-0.01983
12	-0.01691	0.01418	-0.01711	0.01492	-0.01733	0.01572	-0.01776
13	-0.01596	0.01387	-0.01601	0.01445	-0.01600	0.01502	-0.01513
14	-0.01498	0.01349	-0.01488	0.01391	-0.01466	0.01424	-0.01433
15	-0.01395	0.01297	-0.01372	0.01323	-0.01330	0.01249	-0.01300
16	-0.01292	0.01240	-0.01256	0.01249	-0.01197	0.01235	-0.01169
17	-0.01190	0.01167	-0.01143	0.01160	-0.01071	0.01125	-0.01030
18	-0.01087	0.01092	-0.01031	0.01070	-0.00947	0.01016	-0.00810
19	-0.00986	0.01023	-0.00921	0.00987	-0.00830	0.00917	-0.00686
20	-0.00888	0.00947	-0.00818	0.00899	-0.00721	0.00816	-0.00575
21	-0.00791	0.00871	-0.00717	0.00812	-0.00617	0.00718	-0.00474
22	-0.00700	0.00802	-0.00623	0.00734	-0.00523	0.00632	-0.00386
23	-0.00613	0.00729	-0.00535	0.00654	-0.00437	0.00547	-0.00308
24	-0.00995	0.01263	-0.00841	0.01097	-0.00658	0.00876	-0.00434
25	-0.00860	0.01245	-0.00684	0.01022	-0.00491	0.00752	-0.00283
26	-0.00124	0.00205	-0.00093	0.00160	-0.00061	0.00110	-0.00030
27	-0.00907	0.01699	-0.00633	0.01235	-0.00376	0.00761	-0.00159
28	-0.00490	0.00828	-0.00237	0.00510	-0.00110	0.00245	-0.00031
29	-0.00164	0.00384	-0.00081	0.00198	-0.00029	0.00073	-0.00013
30	-0.00065	0.00164	-0.00027	0.00070	-0.00007	0.00020	-0.00002
31	-0.00024	0.00067	-0.00008	0.00024	-0.00002	0.00005	-0.00000
32	-0.00014	0.00040	-0.00004	0.00011	-0.00001	0.00002	-0.00000
33	-0.00002	0.00005	-0.00000	0.00001	-0.00000	0.00000	-0.00000
34	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000
35	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000

TABLE 8a
 VARIATIONAL PARTIAL DERIVATIVES FOR GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE CONTINENTAL
 EARTH MODEL

GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE

T(SEC)	84.00	78.73	73.70	68.94	64.49	60.37
C(K/SEC)	4.510	4.490	4.470	4.450	4.430	4.410
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU
1	-0.00301	0.00015	0.00016	0.00017	-0.00401	0.00020
2	-0.00301	0.00015	0.00016	0.00017	-0.00401	0.00020
3	-0.00602	0.00030	0.00032	0.00034	-0.00802	0.00041
4	-0.00601	0.00030	0.00032	0.00034	-0.00800	0.00041
5	-0.00600	0.00030	0.00032	0.00034	-0.00798	0.00041
6	-0.00599	0.00030	0.00032	0.00034	-0.00796	0.00041
7	-0.01186	0.00059	0.00063	0.00068	-0.01584	0.00081
8	-0.01186	0.00059	0.00063	0.00068	-0.01584	0.00081
9	-0.02925	0.00146	0.00157	0.00170	-0.03564	0.00184
10	-0.02847	0.00145	0.00155	0.00167	-0.03434	0.00181
11	-0.02755	0.00141	0.00150	0.00162	-0.03282	0.00174
12	-0.02657	0.00138	0.00147	0.00157	-0.03120	0.00169
13	-0.02546	0.00135	0.00143	0.00152	-0.02939	0.00163
14	-0.01949	0.00105	0.00111	0.00118	-0.02209	0.00126
15	-0.00948	0.00049	0.00051	0.00054	-0.01062	0.00056
16	-0.02318	0.00119	0.00124	0.00130	-0.02575	0.00137
17	-0.02245	0.00115	0.00120	0.00126	-0.02463	0.00131
18	-0.02174	0.00112	0.00116	0.00121	-0.02355	0.00126
19	-0.02103	0.00109	0.00112	0.00116	-0.02296	0.00124
20	-0.02034	0.00105	0.00109	0.00112	-0.02151	0.00115

T(SEC)	56.60	53.17	50.07	47.28	44.78	42.52
C(K/SEC)	4.390	4.370	4.350	4.330	4.310	4.290
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU
1	-0.00476	0.00025	0.00027	-0.00621	0.00033	-0.00734
2	-0.00476	0.00025	0.00027	-0.00621	0.00033	-0.00734
3	-0.00951	0.00049	0.00054	-0.01241	0.00066	-0.01351
4	-0.00950	0.00049	0.00054	-0.01238	0.00066	-0.01347
5	-0.00947	0.00049	0.00054	-0.01233	0.00066	-0.01342
6	-0.00944	0.00049	0.00054	-0.01228	0.00066	-0.01336
7	-0.01876	0.00098	0.00108	-0.02436	0.00131	-0.02448
8	-0.01856	0.00098	0.00108	-0.02402	0.00130	-0.02408
9	-0.04523	0.00241	0.00265	-0.05803	0.00320	-0.06281
10	-0.04396	0.00236	0.00258	-0.05546	0.00309	-0.06282
11	-0.04032	0.00223	0.00243	-0.04643	0.00283	-0.05939
12	-0.03755	0.00213	0.00231	-0.04251	0.00250	-0.04568
13	-0.03450	0.00203	0.00219	-0.03827	0.00234	-0.04190
14	-0.02526	0.00154	0.00164	-0.02739	0.00175	-0.02924
15	-0.01193	0.00066	0.00070	-0.01275	0.00073	-0.01338
16	-0.02856	0.00158	0.00166	-0.03081	0.00173	-0.03127
17	-0.02681	0.00149	0.00155	-0.02789	0.00160	-0.02837
18	-0.02518	0.00140	0.00144	-0.02578	0.00150	-0.02546
19	-0.02364	0.00132	0.00135	-0.02383	0.00138	-0.02238
20	-0.02218	0.00124	0.00126	-0.02202	0.00127	-0.02122

TABLE 8b
 VARIATIONAL PARTIAL DERIVATIVES FOR GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE CONTINENTAL
 EARTH MODEL

GUTENBERG BIRCH II		LAMINATED CRUST AND UPPER MANTLE									
T (SECS)	40.47	38.62	36.92	35.36	33.91	32.57					
C (K/SEC)	4.270	4.250	4.230	4.210	4.190	4.170					
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDMU
1	-0.00793	0.00044	-0.00853	0.00047	-0.00914	0.00051	-0.00974	0.00055	-0.01033	0.00059	-0.01091
2	-0.00793	0.00044	-0.00853	0.00047	-0.00914	0.00051	-0.00974	0.00055	-0.01033	0.00059	-0.01091
3	-0.01583	0.00087	-0.01703	0.00094	-0.01823	0.00102	-0.01943	0.00110	-0.02063	0.00117	-0.02183
4	-0.01578	0.00087	-0.01697	0.00094	-0.01817	0.00102	-0.01936	0.00110	-0.02056	0.00117	-0.02176
5	-0.01572	0.00087	-0.01690	0.00094	-0.01808	0.00102	-0.01926	0.00109	-0.02042	0.00117	-0.02156
6	-0.01563	0.00086	-0.01680	0.00094	-0.01797	0.00101	-0.01914	0.00109	-0.02028	0.00116	-0.02140
7	-0.03095	0.00172	-0.03324	0.00186	-0.03553	0.00201	-0.03780	0.00216	-0.04009	0.00231	-0.04222
8	-0.03040	0.00170	-0.03260	0.00184	-0.03481	0.00199	-0.03699	0.00213	-0.03912	0.00228	-0.04120
9	-0.07275	0.00415	-0.07778	0.00449	-0.08277	0.00483	-0.08767	0.00517	-0.09243	0.00551	-0.09703
10	-0.06556	0.00396	-0.07068	0.00426	-0.07471	0.00456	-0.07859	0.00486	-0.08229	0.00516	-0.08580
11	-0.05955	0.00359	-0.06269	0.00384	-0.06568	0.00407	-0.06847	0.00431	-0.07105	0.00453	-0.07341
12	-0.05247	0.00330	-0.05468	0.00350	-0.05669	0.00369	-0.05849	0.00387	-0.06006	0.00403	-0.06138
13	-0.04503	0.00300	-0.04632	0.00315	-0.04740	0.00329	-0.04826	0.00341	-0.04889	0.00352	-0.04928
14	-0.03056	0.00217	-0.03099	0.00226	-0.03124	0.00234	-0.03132	0.00240	-0.03123	0.00246	-0.03097
15	-0.01373	0.00084	-0.01378	0.00086	-0.01375	0.00087	-0.01364	0.00088	-0.01345	0.00088	-0.01318
16	-0.03162	0.00193	-0.03150	0.00195	-0.03118	0.00197	-0.03067	0.00197	-0.02998	0.00196	-0.02914
17	-0.02811	0.00172	-0.02769	0.00172	-0.02710	0.00171	-0.02634	0.00169	-0.02543	0.00166	-0.02440
18	-0.02500	0.00153	-0.02436	0.00151	-0.02357	0.00149	-0.02264	0.00145	-0.02159	0.00141	-0.02045
T (SECS)	31.31	30.12	28.99	27.91	26.88	25.89					
C (K/SEC)	4.150	4.130	4.110	4.090	4.070	4.050					
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDMU
1	-0.01147	0.00067	-0.01202	0.00070	-0.01255	0.00074	-0.01306	0.00078	-0.01355	0.00082	-0.01402
2	-0.01146	0.00067	-0.01201	0.00070	-0.01254	0.00074	-0.01305	0.00078	-0.01354	0.00082	-0.01400
3	-0.02289	0.00133	-0.02398	0.00141	-0.02503	0.00148	-0.02604	0.00156	-0.02701	0.00163	-0.02794
4	-0.02279	0.00133	-0.02388	0.00140	-0.02492	0.00148	-0.02592	0.00155	-0.02689	0.00163	-0.02781
5	-0.02266	0.00132	-0.02373	0.00140	-0.02476	0.00147	-0.02575	0.00155	-0.02670	0.00162	-0.02761
6	-0.02249	0.00132	-0.02355	0.00139	-0.02456	0.00147	-0.02553	0.00154	-0.02646	0.00161	-0.02735
7	-0.04433	0.00261	-0.04638	0.00276	-0.04834	0.00290	-0.05022	0.00304	-0.05201	0.00318	-0.05371
8	-0.04321	0.00257	-0.04515	0.00271	-0.04700	0.00285	-0.04876	0.00299	-0.05044	0.00312	-0.05202
9	-0.01043	0.000618	-0.010563	0.000650	-0.010960	0.000681	-0.011334	0.000712	-0.011684	0.000741	-0.012010
10	-0.08907	0.003572	-0.09211	0.003598	-0.09490	0.003624	-0.09744	0.003647	-0.09973	0.003670	-0.10176
11	-0.07551	0.00494	-0.07736	0.00512	-0.07895	0.00529	-0.08029	0.00545	-0.08137	0.00558	-0.08221
12	-0.06246	0.00432	-0.06329	0.00444	-0.06388	0.00454	-0.06423	0.00463	-0.06435	0.00470	-0.06425
13	-0.04945	0.00370	-0.04940	0.00376	-0.04915	0.00381	-0.04869	0.00383	-0.04805	0.00384	-0.04724
14	-0.03057	0.00253	-0.03002	0.00254	-0.02935	0.00254	-0.02856	0.00253	-0.02766	0.00251	-0.02667
15	-0.01286	0.00087	-0.01247	0.00086	-0.01203	0.00084	-0.01155	0.00082	-0.01103	0.00080	-0.01048
16	-0.02815	0.00190	-0.02705	0.00186	-0.02584	0.00180	-0.02455	0.00174	-0.02319	0.00168	-0.02178
17	-0.02326	0.00157	-0.02204	0.00151	-0.02075	0.00145	-0.01942	0.00138	-0.01805	0.00130	-0.01668

TABLE 8c
 VARIATIONAL PARTIAL DERIVATIVES FOR GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE CONTINENTAL EARTH MODEL
 GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE

PSEUDO SPHERICAL CALCULATION											
T(SEC)		21.30		19.14		17.00		14.83		12.56	
C(K/SEC)		4.000		3.950		3.850		3.800		3.750	

TABLE 9a
PHASE VELOCITY PERTURBATIONS (KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY AND RIGIDITY FOR
GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE CONTINENTAL EARTH MODEL

GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE

T (SECS) C (K/SEC)	84.00 4.510	78.73 4.490	73.70 4.470	68.94 4.450	64.49 4.430	60.37 4.410
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU
1	-0.00083	0.00051	-0.00088	0.00055	-0.00095	0.00060
2	-0.00083	0.00051	-0.00088	0.00055	-0.00094	0.00060
3	-0.00165	0.00103	-0.00176	0.00110	-0.00189	0.00119
4	-0.00165	0.00103	-0.00176	0.00110	-0.00189	0.00119
5	-0.00165	0.00102	-0.00175	0.00110	-0.00188	0.00119
6	-0.00165	0.00102	-0.00175	0.00110	-0.00188	0.00119
7	-0.00328	0.00204	-0.00349	0.00220	-0.00374	0.00237
8	-0.00326	0.00204	-0.00347	0.00219	-0.00371	0.00237
9	-0.00804	0.00507	-0.00855	0.00544	-0.00913	0.00588
10	-0.00783	0.00502	-0.00829	0.00538	-0.00883	0.00579
11	-0.00799	0.00590	-0.00843	0.00630	-0.00894	0.00676
12	-0.00771	0.00578	-0.00810	0.00615	-0.00855	0.00659
13	-0.00738	0.00564	-0.00772	0.00599	-0.00810	0.00638
14	-0.00565	0.00440	-0.00588	0.00466	-0.00613	0.00495
15	-0.00337	0.00364	-0.00350	0.00382	-0.00363	0.00401
16	-0.00825	0.00850	-0.00854	0.00932	-0.00884	0.00977
17	-0.00796	0.00850	-0.00820	0.00887	-0.00846	0.00926
18	-0.00767	0.00816	-0.00788	0.00848	-0.00810	0.00881
19	-0.00739	0.00780	-0.00757	0.00808	-0.00774	0.00836
20	-0.00713	0.00749	-0.00727	0.00773	-0.00741	0.00797
T (SECS) C (K/SEC)	56.60 4.390	53.17 4.370	50.07 4.350	47.28 4.330	44.78 4.310	42.52 4.290
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU
1	-0.00131	0.00086	-0.00143	0.00095	-0.00157	0.00104
2	-0.00131	0.00086	-0.00143	0.00094	-0.00156	0.00104
3	-0.00261	0.00171	-0.00286	0.00189	-0.00313	0.00208
4	-0.00261	0.00171	-0.00285	0.00189	-0.00312	0.00208
5	-0.00260	0.00171	-0.00285	0.00188	-0.00311	0.00208
6	-0.00260	0.00171	-0.00283	0.00188	-0.00310	0.00207
7	-0.00516	0.00340	-0.00563	0.00375	-0.00615	0.00413
8	-0.00510	0.00339	-0.00556	0.00373	-0.00607	0.00411
9	-0.01244	0.00836	-0.01352	0.00920	-0.01470	0.00911
10	-0.01181	0.00817	-0.01277	0.00895	-0.01380	0.00881
11	-0.01169	0.00934	-0.01255	0.01017	-0.01346	0.01047
12	-0.01089	0.00893	-0.01160	0.00968	-0.01233	0.01047
13	-0.01001	0.00849	-0.01055	0.00913	-0.01110	0.00980
14	-0.00732	0.00644	-0.00764	0.00688	-0.00794	0.00734
15	-0.00425	0.00496	-0.00440	0.00521	-0.00454	0.00447
16	-0.01017	0.01186	-0.01047	0.01241	-0.01074	0.01192
17	-0.00950	0.01097	-0.00971	0.01138	-0.00988	0.01176
18	-0.00889	0.01020	-0.00902	0.01050	-0.00910	0.01076
19	-0.00831	0.00946	-0.00837	0.00966	-0.00838	0.00982
20	-0.00777	0.00881	-0.00777	0.00893	-0.00772	0.00900

TABLE 9b
PHASE VELOCITY PERTURBATIONS (KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY AND RIGIDITY FOR
GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE CONTINENTAL EARTH MODEL
GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE

T (SECS) C (K/SEC)	40.47 4.270	38.62 4.250	36.92 4.230	35.36 4.210	33.91 4.190	32.57 4.170
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU
1	-0.00218	0.00151	-0.00235	0.00177	-0.00268	0.00190
2	-0.00218	0.00151	-0.00235	0.00177	-0.00268	0.00190
3	-0.00435	0.00301	-0.00468	0.00353	-0.00507	0.00407
4	-0.00434	0.00301	-0.00467	0.00353	-0.00506	0.00406
5	-0.00432	0.00300	-0.00465	0.00352	-0.00505	0.00405
6	-0.00430	0.00299	-0.00462	0.00351	-0.00504	0.00404
7	-0.00851	0.00595	-0.00914	0.00697	-0.01010	0.00801
8	-0.00836	0.00589	-0.00897	0.00689	-0.01017	0.00790
9	-0.02901	0.01439	-0.02139	0.01566	-0.02276	0.01192
10	-0.01830	0.01373	-0.01944	0.01478	-0.02161	0.01186
11	-0.01727	0.01505	-0.01818	0.01706	-0.01986	0.01803
12	-0.01522	0.01383	-0.01586	0.01544	-0.01696	0.01619
13	-0.01306	0.01255	-0.01343	0.01376	-0.01400	0.01429
14	-0.00886	0.00909	-0.00899	0.00979	-0.00908	0.01007
15	-0.00489	0.00629	-0.00491	0.00651	-0.00485	0.00657
16	-0.01126	0.01465	-0.01121	0.01473	-0.01092	0.01474
17	-0.00996	0.01264	-0.00981	0.01260	-0.00933	0.01245
18	-0.00882	0.01111	-0.00860	0.01083	-0.00799	0.01058
19	-0.00782	0.00976	-0.00754	0.00930	-0.00685	0.00898
20	-0.00694	0.00861	-0.00662	0.00802	-0.00587	0.00765
T (SECS) C (K/SEC)	31.31 4.150	30.12 4.130	28.99 4.110	27.91 4.090	26.88 4.070	25.89 4.050
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU
1	-0.00315	0.00231	-0.00331	0.00258	-0.00359	0.00271
2	-0.00315	0.00231	-0.00330	0.00257	-0.00359	0.00270
3	-0.00629	0.00461	-0.00659	0.00514	-0.00716	0.00540
4	-0.00627	0.00460	-0.00657	0.00513	-0.00713	0.00539
5	-0.00623	0.00458	-0.00653	0.00511	-0.00708	0.00536
6	-0.00619	0.00456	-0.00648	0.00508	-0.00702	0.00533
7	-0.01219	0.00904	-0.01275	0.01005	-0.01361	0.01055
8	-0.01188	0.00890	-0.01242	0.00987	-0.01341	0.01035
9	-0.02789	0.02141	-0.02905	0.02362	-0.03117	0.02467
10	-0.02449	0.01982	-0.02533	0.02161	-0.02680	0.02244
11	-0.02190	0.02068	-0.02243	0.02021	-0.02328	0.02021
12	-0.01811	0.01808	-0.01836	0.01902	-0.01863	0.01938
13	-0.01434	0.01549	-0.01433	0.01594	-0.01412	0.01605
14	-0.00886	0.01058	-0.00871	0.01065	-0.00828	0.01060
15	-0.00458	0.00652	-0.00444	0.00632	-0.00411	0.00617
16	-0.01002	0.01424	-0.00963	0.01352	-0.00874	0.01306
17	-0.00824	0.01137	-0.00781	0.01067	-0.00688	0.01016
18	-0.00579	0.00946	-0.00635	0.00848	-0.00543	0.00795
19	-0.00560	0.00772	-0.00516	0.00673	-0.00429	0.00622
20	-0.00463	0.00634	-0.00421	0.00537	-0.00339	0.00489

TABLE 9c
 PHASE VELOCITY PERTURBATIONS (KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY AND RIGIDITY
 FOR GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE CONTINENTAL EARTH MODEL
 VARIATIONS FOR 10 0/0 CHANGE IN PARAMETER
 GUTENBERG BIRCH II LAMINATED CRUST AND UPPER MANTLE

PSEUDO SPHERICAL CALCULATION											
19.14		17.00		14.83		12.56					
C (K/SEC)		C (K/SEC)		C (K/SEC)		C (K/SEC)					
21.30		3.950		3.800		3.750					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					
DC/DRHO		DC/DRHO		DC/DRHO		DC/DRHO					
DC/DMU		DC/DMU		DC/DMU		DC/DMU					

particular problem by modifying the trial structures and comparing the "predicted" results with those computed or published elsewhere. All published theoretical Love wave dispersion curves should be reproducible from the tables given here.

TABLE 10a
VARIATIONAL PARTIAL DERIVATIVES FOR CIT13F LAMINATED CRUST AND UPPER MANTLE
OCEANIC EARTH MODEL

CIT13F OCEANIC LAMINATED CRUST AND UPPER MANTLE													
PSEUDO SPHERICAL CALCULATION													
T(SECS) 119.11		98.96		78.15		57.53		38.61		23.42			
C(K/SEC) 4.730		4.650		4.600		4.550		4.500		4.450			
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO
1	-0.00037	0.00002	-0.00040	0.00002	-0.00045	0.00002	-0.00055	0.00003	-0.00074	0.00004	-0.00126	0.00006	0.00006
2	-0.00074	0.00003	-0.00081	0.00004	-0.00091	0.00004	-0.00110	0.00005	-0.00148	0.00008	-0.00251	0.00014	0.00014
3	-0.00074	0.00003	-0.00080	0.00004	-0.00091	0.00005	-0.00110	0.00006	-0.00147	0.00009	-0.00248	0.00019	0.00019
4	-0.00186	0.00008	-0.00221	0.00009	-0.00227	0.00011	-0.00273	0.00013	-0.00366	0.00018	-0.00612	0.00031	0.00031
5	-0.00186	0.00008	-0.00201	0.00009	-0.00227	0.00011	-0.00273	0.00013	-0.00365	0.00018	-0.00608	0.00031	0.00031
6	-0.00371	0.00017	-0.00401	0.00019	-0.00452	0.00021	-0.00545	0.00026	-0.00725	0.00036	-0.01199	0.00063	0.00063
7	-0.00371	0.00017	-0.00401	0.00019	-0.00451	0.00021	-0.00543	0.00026	-0.00720	0.00036	-0.01175	0.00060	0.00060
8	-0.00740	0.00034	-0.00799	0.00037	-0.00899	0.00043	-0.01079	0.00052	-0.01423	0.00071	-0.02284	0.00119	0.00119
9	-0.00738	0.00034	-0.00796	0.00037	-0.00894	0.00043	-0.01069	0.00052	-0.01396	0.00071	-0.02172	0.00116	0.00116
10	-0.00736	0.00033	-0.00793	0.00037	-0.00889	0.00042	-0.01059	0.00051	-0.01370	0.00068	-0.02069	0.00107	0.00107
11	-0.00733	0.00033	-0.00790	0.00037	-0.00885	0.00042	-0.01051	0.00051	-0.01351	0.00067	-0.01996	0.00103	0.00103
12	-0.00731	0.00033	-0.00787	0.00037	-0.00881	0.00042	-0.01044	0.00051	-0.01333	0.00067	-0.01928	0.00100	0.00100
13	-0.00729	0.00033	-0.00785	0.00037	-0.00877	0.00042	-0.01036	0.00050	-0.01315	0.00066	-0.01865	0.00096	0.00096
14	-0.00364	0.00017	-0.00391	0.00018	-0.00437	0.00021	-0.00515	0.00025	-0.00651	0.00033	-0.00910	0.00047	0.00047
15	-0.00181	0.00008	-0.00194	0.00009	-0.00219	0.00010	-0.00255	0.00012	-0.00319	0.00016	-0.00455	0.00024	0.00024
16	-0.01798	0.00082	-0.01929	0.00090	-0.02145	0.00102	-0.02510	0.00123	-0.03105	0.00155	-0.04067	0.00209	0.00209
17	-0.01783	0.00082	-0.01910	0.00089	-0.02119	0.00101	-0.02467	0.00121	-0.03017	0.00151	-0.03819	0.00196	0.00196
18	-0.01767	0.00081	-0.01890	0.00089	-0.02091	0.00100	-0.02422	0.00119	-0.02929	0.00147	-0.03588	0.00185	0.00185
19	-0.01749	0.00081	-0.01869	0.00088	-0.02061	0.00099	-0.02375	0.00117	-0.02839	0.00143	-0.03369	0.00174	0.00174
20	-0.01731	0.00080	-0.01845	0.00087	-0.02029	0.00098	-0.02324	0.00115	-0.02744	0.00138	-0.03152	0.00163	0.00163
21	-0.01711	0.00079	-0.01820	0.00086	-0.01995	0.00096	-0.02271	0.00112	-0.02645	0.00134	-0.02936	0.00153	0.00153
22	-0.01689	0.00078	-0.01794	0.00085	-0.01958	0.00095	-0.02214	0.00110	-0.02543	0.00129	-0.02725	0.00142	0.00142
23	-0.03314	0.00154	-0.03506	0.00167	-0.03805	0.00185	-0.04253	0.00212	-0.04777	0.00244	-0.04848	0.00254	0.00254
24	-0.03216	0.00151	-0.03384	0.00162	-0.03639	0.00178	-0.04001	0.00201	-0.04347	0.00223	-0.04083	0.00215	0.00215
25	-0.03111	0.00147	-0.03253	0.00157	-0.03462	0.00171	-0.03737	0.00189	-0.03914	0.00202	-0.03385	0.00179	0.00179
26	-0.02998	0.00142	-0.03114	0.00151	-0.03277	0.00163	-0.03464	0.00176	-0.03485	0.00181	-0.02760	0.00147	0.00147
27	-0.05650	0.00271	-0.05800	0.00285	-0.05987	0.00301	-0.06114	0.00314	-0.05758	0.00303	-0.03974	0.00215	0.00215
T(SECS) 15.56		12.55		11.30		9.98		9.23		8.63			
C(K/SEC) 4.400		4.350		4.300		4.250		4.200		4.150			
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO
1	-0.00276	0.00015	-0.00497	0.00027	-0.00730	0.00041	-0.00962	0.00056	-0.01191	0.00072	-0.01419	0.00088	0.00088
2	-0.00546	0.00037	-0.00978	0.00076	-0.01432	0.00124	-0.01877	0.00178	-0.02315	0.00239	-0.02749	0.00306	0.00306
3	-0.00530	0.00036	-0.00934	0.00140	-0.01348	0.00245	-0.01745	0.00370	-0.02125	0.00514	-0.02492	0.00677	0.00677
4	-0.01290	0.00067	-0.02242	0.00121	-0.03194	0.00177	-0.04086	0.00233	-0.04918	0.00288	-0.05699	0.00343	0.00343
5	-0.01273	0.00068	-0.02197	0.00121	-0.03111	0.00178	-0.03958	0.00234	-0.04740	0.00289	-0.05464	0.00344	0.00344
6	-0.02467	0.00137	-0.04189	0.00246	-0.05849	0.00360	-0.07347	0.00473	-0.08692	0.00584	-0.09901	0.00692	0.00692
7	-0.02360	0.00127	-0.03912	0.00219	-0.05531	0.00311	-0.06597	0.00398	-0.07667	0.00478	-0.08582	0.00554	0.00554
8	-0.04424	0.00245	-0.07087	0.00414	-0.09415	0.00577	-0.11308	0.00724	-0.12822	0.00855	-0.14015	0.00971	0.00971
9	-0.03948	0.00230	-0.05940	0.00376	-0.07479	0.00509	-0.08557	0.00620	-0.09268	0.00711	-0.09689	0.00784	0.00784
10	-0.03530	0.00192	-0.04979	0.00286	-0.05918	0.00356	-0.06418	0.00405	-0.06600	0.00435	-0.06554	0.00451	0.00451
11	-0.03248	0.00176	-0.04360	0.00249	-0.04957	0.00298	-0.05156	0.00324	-0.05091	0.00335	-0.04855	0.00333	0.00333
12	-0.02996	0.00162	-0.03830	0.00218	-0.04164	0.00249	-0.04152	0.00261	-0.03935	0.00258	-0.03603	0.00247	0.00247
13	-0.02772	0.00150	-0.03376	0.00192	-0.03510	0.00209	-0.03355	0.00210	-0.03051	0.00200	-0.02681	0.00183	0.00183
14	-0.01309	0.00071	-0.01538	0.00087	-0.01546	0.00092	-0.01431	0.00089	-0.01261	0.00082	-0.01073	0.00073	0.00073
15	-0.05902	0.00317	-0.06484	0.00365	-0.06125	0.00361	-0.05345	0.00330	-0.04448	0.00288	-0.03578	0.00242	0.00242
16	-0.05026	0.00268	-0.04950	0.00276	-0.04208	0.00245	-0.03315	0.00202	-0.02492	0.00159	-0.01810	0.00120	0.00120
17	-0.04343	0.00232	-0.03863	0.00215	-0.02969	0.00173	-0.02119	0.00129	-0.01443	0.00092	-0.00949	0.00063	0.00063
18	-0.03770	0.00201	-0.03038	0.00169	-0.02116	0.00123	-0.01369	0.00083	-0.00845	0.00053	-0.00503	0.00033	0.00033
19	-0.03283	0.00175	-0.02405	0.00134	-0.01522	0.00088	-0.00895	0.00054	-0.00502	0.00032	-0.00271	0.00018	0.00018
20	-0.02846	0.00153	-0.01896	0.00106	-0.01090	0.00063	-0.00582	0.00035	-0.00297	0.00019	-0.00145	0.00010	0.00010
21	-0.02456	0.00132	-0.01488	0.00083	-0.00777	0.00045	-0.00377	0.00023	-0.00175	0.00011	-0.00077	0.00005	0.00005
22	-0.02110	0.00114	-0.01162	0.00065	-0.00551	0.00032	-0.00243	0.00015	-0.00102	0.00007	-0.00041	0.00003	0.00003
23	-0.03350	0.00181	-0.01610	0.00091	-0.00667	0.00039	-0.00258	0.00016	-0.00095	0.00006	-0.00033	0.00002	0.00002
24	-0.02412	0.00131	-0.00960	0.00054	-0.00329	0.00019	-0.00105	0.00006	-0.00032	0.00002	-0.00009	0.00001	0.00001
25	-0.01706	0.00093	-0.00563	0.00032	-0.00159	0.00009	-0.00042	0.00003	-0.00011	0.00001	-0.00003	0.00000	0.00000
26	-0.01183	0.00065	-0.00324	0.00019	-0.00076	0.00005	-0.00017	0.00001	-0.00003	0.00000	-0.00001	0.00000	0.00000
27	-0.01351	0.00075	-0.00287	0.00017	-0.00053	0.00003	-0.00009	0.00001	-0.00001	0.00000	-0.00000	0.00000	0.00000

As an early test of the method the dispersion and partials were computed for a Jeffreys-Bullen type mantle. These results were used to predict the dispersion when the layer parameters were modified in such a way as to approximate a Gutenberg-Bullen type mantle. The actual dispersion for a Gutenberg-Bullen model was then computed. Since the partial derivative tables are routine computer output in the

TABLE 10b
 VARIATIONAL PARTIAL DERIVATIVES FOR CIT13F LAMINATED CRUST AND UPPER MANTLE
 OCEANIC EARTH MODEL

CIT 13F OCEANIC LAMINATED CRUST AND UPPER MANTLE

T(SEC)	8.12	7.68	7.29	6.94	6.62	6.32
C(K/SEC)	4.100	4.050	4.000	3.950	3.900	3.850
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU
1	-0.01650	0.00106	-0.01885	0.00124	-0.02127	0.00145
2	-0.03183	0.00380	-0.03622	0.00463	-0.04069	0.00557
3	-0.02848	0.00863	-0.03198	0.01073	-0.03543	0.01312
4	-0.06436	0.00398	-0.07135	0.00454	-0.07800	0.00511
5	-0.06138	0.00399	-0.06768	0.00454	-0.07357	0.00509
6	-0.10991	0.00799	-0.11973	0.00905	-0.12853	0.01009
7	-0.09360	0.00624	-0.10016	0.00690	-0.10556	0.00751
8	-0.14931	0.01074	-0.15605	0.01163	-0.16600	0.01239
9	-0.09880	0.00841	-0.09885	0.00882	-0.09735	0.00909
10	-0.06346	0.00455	-0.06023	0.00450	-0.05619	0.00437
11	-0.04512	0.00323	-0.04106	0.00307	-0.03668	0.00286
12	-0.03213	0.00230	-0.02803	0.00209	-0.02397	0.00186
13	-0.02293	0.00164	-0.01917	0.00143	-0.01569	0.00122
14	-0.00889	0.00063	-0.00719	0.00053	-0.00568	0.00044
15	-0.02801	0.00198	-0.02140	0.00158	-0.01597	0.00123
16	-0.01277	0.00089	-0.00877	0.00064	-0.00586	0.00044
17	-0.00605	0.00042	-0.00374	0.00027	-0.00224	0.00017
18	-0.00289	0.00020	-0.00161	0.00012	-0.00087	0.00006
19	-0.00141	0.00011	-0.00071	0.00005	-0.00034	0.00003
20	-0.00068	0.00005	-0.00031	0.00002	-0.00013	0.00001
21	-0.00033	0.00002	-0.00013	0.00001	-0.00005	0.00000
22	-0.00016	0.00001	-0.00006	0.00000	-0.00002	0.00000
T(SEC)	6.05	5.79	5.54	5.31	5.10	4.89
C(K/SEC)	3.800	3.750	3.700	3.650	3.600	3.550
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU
1	-0.03228	0.00249	-0.03558	0.00284	-0.03922	0.00324
2	-0.06050	0.01076	-0.06625	0.01258	-0.07262	0.01471
3	-0.04936	0.02661	-0.05305	0.03138	-0.05691	0.03655
4	-0.10187	0.00751	-0.10732	0.00816	-0.11263	0.00884
5	-0.09362	0.00736	-0.09787	0.00795	-0.10187	0.00856
6	-0.15467	0.01413	-0.15911	0.01511	-0.16278	0.01607
7	-0.11687	0.00946	-0.11736	0.00982	-0.11698	0.01013
8	-0.16060	0.01414	-0.15679	0.01425	-0.15174	0.01424
9	-0.08096	0.00891	-0.07523	0.00860	-0.06915	0.00820
10	-0.03683	0.00337	-0.03203	0.00305	-0.02748	0.00272
11	-0.01983	0.00181	-0.01633	0.00156	-0.01323	0.00131
12	-0.01067	0.00098	-0.00832	0.00079	-0.00636	0.00063
13	-0.00575	0.00053	-0.00424	0.00040	-0.00306	0.00030
14	-0.00179	0.00016	-0.00126	0.00012	-0.00087	0.00009
15	-0.00393	0.00036	-0.00260	0.00025	-0.00167	0.00016
16	-0.00088	0.00008	-0.00051	0.00005	-0.00028	0.00003
17	-0.00021	0.00002	-0.00010	0.00001	-0.00005	0.00000
18	-0.00005	0.00000	-0.00002	0.00000	-0.00000	0.00000
19	-0.00001	0.00000	-0.00000	0.00000	-0.00000	0.00000
20	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000
21	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000
22	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000
T(SEC)	4.70	4.52	4.35	4.20	4.05	3.92
C(K/SEC)	3.500	3.450	3.400	3.350	3.300	3.250
M	DCDRHO	DCDMU	DCDRHO	DCDMU	DCDRHO	DCDMU
1	-0.05908	0.00560	-0.06597	0.00647	-0.07393	0.00752
2	-0.10619	0.02793	-0.11757	0.03298	-0.13058	0.03903
3	-0.07518	0.01130	-0.08077	0.01287	-0.08691	0.01356
4	-0.13301	0.01193	-0.13793	0.01283	-0.14278	0.01378
5	-0.11544	0.01118	-0.11821	0.01189	-0.12071	0.01262
6	-0.16990	0.01976	-0.16980	0.02061	-0.16896	0.02143
7	-0.10765	0.01074	-0.10358	0.01073	-0.09896	0.01065
8	-0.12179	0.01303	-0.11264	0.01246	-0.10318	0.01182
9	-0.04439	0.00603	-0.03860	0.00542	-0.03317	0.00481
10	-0.01290	0.00150	-0.01028	0.00124	-0.00808	0.00102
11	-0.00477	0.00055	-0.00353	0.00043	-0.00256	0.00032
12	-0.00176	0.00020	-0.00121	0.00015	-0.00081	0.00010
13	-0.00065	0.00008	-0.00041	0.00005	-0.00026	0.00003
14	-0.00015	0.00002	-0.00009	0.00001	-0.00005	0.00000
15	-0.00001	0.00000	-0.00001	0.00000	-0.00000	0.00000
16	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000
17	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000

Caltech dispersion programs the new tables were used to predict back to the Jeffreys-Bullen model. The results are shown in fig. 1.

The tables are particularly designed for investigation of the physical properties of the crust and mantle. However, the effect of crustal thickness changes may be

estimated by use of equation 17. Figure 2 shows a rather extreme trial case where another forward-backward experiment has been performed for illustration. In the "forward" case a crustal layer has been decreased in thickness by 50 %. In the

TABLE 11a
PHASE VELOCITY PERTURBATIONS (KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY
AND RIGIDITY FOR CIT13F LAMINATED CRUST AND UPPER MANTLE OCEANIC EARTH MODEL

VARIATIONS FOR 10 C/O CHANGE IN PARAMETER													
CIT13F OCEANIC				LAMINATED CRUST AND UPPER MANTLE									
PSEUDO SPHERICAL CALCULATION													
T(SEC)		119.11		98.96		78.15		57.53		38.61		23.42	
C(K/SEC)		4.700		4.650		4.600		4.550		4.500		4.450	
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO
1	-0.00007	0.00090	-0.00008	0.00000	-0.00009	0.00000	-0.00010	0.00000	-0.00014	0.00000	-0.00024	0.00001	0.00001
2	-0.00014	0.00000	-0.00015	0.00000	-0.00017	0.00001	-0.00021	0.00001	-0.00028	0.00001	-0.00048	0.00002	0.00002
3	-0.00014	0.00000	-0.00015	0.00000	-0.00017	0.00001	-0.00021	0.00001	-0.00028	0.00001	-0.00047	0.00002	0.00002
4	-0.00047	0.00018	-0.00051	0.00020	-0.00058	0.00023	-0.00069	0.00028	-0.00093	0.00038	-0.00155	0.00066	0.00066
5	-0.00047	0.00018	-0.00051	0.00020	-0.00058	0.00023	-0.00069	0.00028	-0.00093	0.00038	-0.00154	0.00066	0.00066
6	-0.00094	0.00036	-0.00102	0.00039	-0.00115	0.00045	-0.00138	0.00056	-0.00184	0.00076	-0.00305	0.00132	0.00132
7	-0.00108	0.00036	-0.00116	0.00074	-0.00131	0.00085	-0.00157	0.00104	-0.00209	0.00142	-0.00341	0.00240	0.00240
8	-0.00215	0.00133	-0.00232	0.00147	-0.00261	0.00170	-0.00313	0.00208	-0.00413	0.00283	-0.00662	0.00473	0.00473
9	-0.00214	0.00133	-0.00231	0.00147	-0.00259	0.00169	-0.00310	0.00207	-0.00405	0.00280	-0.00630	0.00460	0.00460
10	-0.00244	0.00235	-0.00263	0.00259	-0.00295	0.00297	-0.00352	0.00362	-0.00455	0.00481	-0.00687	0.00752	0.00752
11	-0.00244	0.00234	-0.00262	0.00258	-0.00294	0.00295	-0.00349	0.00359	-0.00449	0.00474	-0.00663	0.00724	0.00724
12	-0.00243	0.00234	-0.00261	0.00257	-0.00292	0.00294	-0.00347	0.00357	-0.00442	0.00467	-0.00640	0.00699	0.00699
13	-0.00242	0.00233	-0.00260	0.00257	-0.00291	0.00293	-0.00344	0.00355	-0.00437	0.00461	-0.00619	0.00676	0.00676
14	-0.00121	0.00116	-0.00130	0.00128	-0.00145	0.00146	-0.00171	0.00176	-0.00216	0.00228	-0.00302	0.00329	0.00329
15	-0.00602	0.00581	-0.00647	0.00639	-0.00722	0.00728	-0.00849	0.00875	-0.01063	0.01124	-0.01448	0.01577	0.01577
16	-0.00599	0.00569	-0.00642	0.00624	-0.00714	0.00709	-0.00836	0.00848	-0.01034	0.01075	-0.01354	0.01448	0.01448
17	-0.00595	0.00542	-0.00637	0.00593	-0.00707	0.00672	-0.00823	0.00801	-0.01006	0.01092	-0.01274	0.01304	0.01304
18	-0.00589	0.00538	-0.00630	0.00588	-0.00697	0.00665	-0.00808	0.00788	-0.00977	0.00975	-0.01197	0.01226	0.01226
19	-0.00586	0.00522	-0.00626	0.00570	-0.00691	0.00643	-0.00796	0.00757	-0.00951	0.00926	-0.01129	0.01129	0.01129
20	-0.00580	0.00518	-0.00618	0.00564	-0.00680	0.00634	-0.00779	0.00743	-0.00919	0.00898	-0.01056	0.01059	0.01059
21	-0.00573	0.00513	-0.00610	0.00558	-0.00668	0.00625	-0.00761	0.00728	-0.00886	0.00868	-0.00984	0.00989	0.00989
22	-0.00566	0.00508	-0.00601	0.00551	-0.00656	0.00616	-0.00742	0.00712	-0.00852	0.00837	-0.00913	0.00921	0.00921
23	-0.01118	0.01009	-0.01183	0.01090	-0.01284	0.01210	-0.01436	0.01384	-0.01612	0.01591	-0.01636	0.01658	0.01658
24	-0.01085	0.00985	-0.01142	0.01059	-0.01228	0.01164	-0.01350	0.01310	-0.01467	0.01458	-0.01378	0.01405	0.01405
25	-0.01055	0.00963	-0.01103	0.01029	-0.01174	0.01120	-0.01267	0.01237	-0.01327	0.01327	-0.01147	0.01178	0.01178
26	-0.01016	0.00935	-0.01056	0.00992	-0.01111	0.01068	-0.01174	0.01155	-0.01181	0.01191	-0.00936	0.00968	0.00968
27	-0.01927	0.01792	-0.01978	0.01880	-0.02042	0.01984	-0.02085	0.02075	-0.01963	0.02002	-0.01355	0.01418	0.01418
T(SEC)		15.56		12.55		11.00		9.98		9.23		8.63	
C(K/SEC)		4.400		4.350		4.300		4.250		4.200		4.150	
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO
1	-0.00052	0.00002	-0.00094	0.00003	-0.00139	0.00005	-0.00183	0.00007	-0.00226	0.00009	-0.00270	0.00011	0.00011
2	-0.00104	0.00005	-0.00186	0.00009	-0.00272	0.00015	-0.00357	0.00022	-0.00440	0.00029	-0.00522	0.00037	0.00037
3	-0.00101	0.00007	-0.00178	0.00017	-0.00256	0.00030	-0.00332	0.00045	-0.00404	0.00062	-0.00473	0.00082	0.00082
4	-0.00328	0.00142	-0.00569	0.00254	-0.00811	0.00373	-0.01038	0.00490	-0.01249	0.00607	-0.01448	0.00723	0.00723
5	-0.00323	0.00143	-0.00558	0.00256	-0.00790	0.00375	-0.01005	0.00493	-0.01204	0.00609	-0.01388	0.00725	0.00725
6	-0.00627	0.00288	-0.01064	0.00518	-0.01486	0.00759	-0.01866	0.00997	-0.02208	0.01230	-0.02515	0.01459	0.01459
7	-0.00684	0.00503	-0.01134	0.00870	-0.01552	0.01236	-0.01913	0.01579	-0.02223	0.01899	-0.02489	0.02198	0.02198
8	-0.01283	0.00971	-0.02055	0.01644	-0.02730	0.02292	-0.03279	0.02875	-0.03718	0.03395	-0.04064	0.03856	0.03856
9	-0.01145	0.00913	-0.01723	0.01495	-0.02169	0.02021	-0.02482	0.02462	-0.02688	0.02824	-0.02810	0.03113	0.03113
10	-0.01172	0.01350	-0.01653	0.02006	-0.01965	0.02504	-0.02131	0.02842	-0.02191	0.03054	-0.02176	0.03166	0.03166
11	-0.01078	0.01239	-0.01448	0.01753	-0.01646	0.02092	-0.01712	0.02279	-0.01690	0.02352	-0.01612	0.02343	0.02343
12	-0.00995	0.01146	-0.01272	0.01535	-0.01383	0.01752	-0.01379	0.01831	-0.01307	0.01814	-0.01196	0.01735	0.01735
13	-0.00920	0.01052	-0.01121	0.01348	-0.01165	0.01472	-0.01114	0.01474	-0.01013	0.01402	-0.00890	0.01288	0.01288
14	-0.00435	0.00496	-0.00511	0.00612	-0.00513	0.00646	-0.00475	0.00627	-0.00419	0.00578	-0.00356	0.00514	0.00514
15	-0.01963	0.02229	-0.02156	0.02568	-0.02036	0.02543	-0.01777	0.02324	-0.01479	0.02023	-0.01190	0.01701	0.01701
16	-0.01674	0.01857	-0.01648	0.01912	-0.01401	0.01699	-0.01104	0.01399	-0.00830	0.01099	-0.00603	0.00834	0.00834
17	-0.01448	0.01536	-0.01288	0.01426	-0.00990	0.01145	-0.00707	0.00854	-0.00481	0.00607	-0.00316	0.00417	0.00417
18	-0.01257	0.01334	-0.01013	0.01119	-0.00706	0.00813	-0.00457	0.00549	-0.00282	0.00354	-0.00168	0.00220	0.00220
19	-0.01100	0.01138	-0.00806	0.00868	-0.00510	0.00572	-0.00300	0.00351	-0.00168	0.00205	-0.00091	0.00116	0.00116
20	-0.00953	0.00989	-0.00635	0.00686	-0.00365	0.00411	-0.00195	0.00229	-0.00099	0.00122	-0.00049	0.00062	0.00062
21	-0.00823	0.00856	-0.00499	0.00540	-0.00260	0.00294	-0.00126	0.00149	-0.00058	0.00072	-0.00026	0.00033	0.00033
22	-0.00707	0.00738	-0.00389	0.00423	-0.00185	0.00209	-0.00081	0.00096	-0.00034	0.00042	-0.00014	0.00018	0.00018
23	-0.01131	0.01185	-0.00543	0.00593	-0.00225	0.00256	-0.00087	0.00103	-0.00032	0.00040	-0.00011	0.00015	0.00015
24	-0.00814	0.00859	-0.00324	0.00356	-0.00111	0.00127	-0.00035	0.00042	-0.00011	0.00013	-0.00003	0.00004	0.00004
25	-0.00578	0.00614	-0.00191	0.00211	-0.00054	0.00062	-0.00014	0.00017	-0.00004	0.00004	-0.00001	0.00001	0.00001
26	-0.00401	0.00429	-0.00110	0.00122	-0.00026	0.00030	-0.00006	0.00007	-0.00001	0.00001	-0.00000	0.00000	0.00000
27	-0.00461	0.00497	-0.00098	0.00110	-0.00018	0.00021	-0.00003	0.00004	-0.00001	0.00001	-0.00000	0.00000	0.00000

"backward" case the thickness has been increased back to the original value—this corresponding now to a 100 % change in thickness. It is more accurate to modify the physical properties in the framework of the standard model layering as also shown in figure 2. This tactic removes the restriction of small changes since the maximum

TABLE 11b
PHASE VELOCITY PERTURBATIONS (KM/SEC) RESULTING FROM A 10% CHANGE IN DENSITY
AND RIGIDITY FOR CIT13F LAMINATED CRUST AND UPPER MANTLE OCEANIC EARTH MODEL

CIT 13F		OCEANIC		LAMINATED CRUST AND UPPER MANTLE												
T(SECS)	8.12			7.68				7.29				6.94		6.62		6.32
C(K/SEC)	4.100			4.050				4.000				3.950		3.900		3.850
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU
1	-0.00314	0.00013	-0.00358	0.00015	-0.00404	0.00018	-0.00452	0.00020	-0.00502	0.00023	-0.00556	0.00027	-0.00610	0.00030	-0.00664	0.00034
2	-0.00605	0.00046	-0.00668	0.00056	-0.00733	0.00068	-0.00801	0.00081	-0.00869	0.00095	-0.00938	0.00109	-0.01007	0.00123	-0.01076	0.00138
3	-0.00541	0.00105	-0.00608	0.00130	-0.00673	0.00160	-0.00738	0.00190	-0.00804	0.00220	-0.00870	0.00250	-0.00935	0.00280	-0.01000	0.00310
4	-0.01635	0.00839	-0.01812	0.00957	-0.01981	0.01076	-0.02142	0.01198	-0.02296	0.01322	-0.02444	0.01450	-0.02592	0.01576	-0.02739	0.01702
5	-0.01559	0.00840	-0.01719	0.00956	-0.01869	0.01072	-0.02009	0.01189	-0.02140	0.01308	-0.02263	0.01428	-0.02386	0.01549	-0.02509	0.01672
6	-0.02792	0.01684	-0.03041	0.01907	-0.03265	0.02126	-0.03464	0.02343	-0.03641	0.02557	-0.03795	0.02768	-0.03949	0.02971	-0.04124	0.03174
7	-0.02715	0.02477	-0.02905	0.02738	-0.03061	0.02980	-0.03186	0.03204	-0.03282	0.03409	-0.03349	0.03593	-0.03666	0.03771	-0.03849	0.03949
8	-0.04330	0.04262	-0.04526	0.04616	-0.04657	0.04917	-0.04732	0.05168	-0.04754	0.05367	-0.04727	0.05515	-0.04666	0.04829	-0.04604	0.04882
9	-0.02865	0.03338	-0.02867	0.03502	-0.02823	0.03609	-0.02743	0.03662	-0.02634	0.03666	-0.02500	0.03623	-0.02366	0.03586	-0.02232	0.03549
10	-0.02107	0.03197	-0.02000	0.03162	-0.01865	0.03073	-0.01714	0.02941	-0.01552	0.02773	-0.01387	0.02579	-0.01221	0.02386	-0.01076	0.02259
11	-0.01498	0.02271	-0.01363	0.02155	-0.01218	0.02006	-0.01070	0.01835	-0.00925	0.01652	-0.00786	0.01463	-0.00649	0.01292	-0.00524	0.01163
12	-0.01067	0.01615	-0.00931	0.01469	-0.00796	0.01310	-0.00668	0.01146	-0.00551	0.00984	-0.00446	0.00829	-0.00349	0.00702	-0.00264	0.00629
13	-0.00761	0.01150	-0.00636	0.01003	-0.00521	0.00856	-0.00418	0.00716	-0.00329	0.00586	-0.00253	0.00470	-0.00189	0.00374	-0.00284	0.00304
14	-0.00295	0.00444	-0.00239	0.00375	-0.00189	0.00309	-0.00146	0.00250	-0.00111	0.00197	-0.00082	0.00152	-0.00057	0.00112	-0.00034	0.00094
15	-0.00931	0.01391	-0.00711	0.01109	-0.00531	0.00864	-0.00388	0.00657	-0.00276	0.00488	-0.00192	0.00354	-0.00129	0.00224	-0.00084	0.00154
16	-0.00425	0.00614	-0.00292	0.00440	-0.00195	0.00307	-0.00127	0.00208	-0.00080	0.00137	-0.00049	0.00088	-0.00024	0.00044	-0.00019	0.00022
17	-0.00202	0.00277	-0.00125	0.00179	-0.00075	0.00112	-0.00043	0.00068	-0.00024	0.00040	-0.00013	0.00022	-0.00007	0.00012	-0.00004	0.00006
18	-0.00096	0.00132	-0.00054	0.00077	-0.00029	0.00043	-0.00015	0.00023	-0.00007	0.00012	-0.00004	0.00006	-0.00002	0.00004	-0.00001	0.00002
19	-0.00047	0.00063	-0.00024	0.00033	-0.00011	0.00017	-0.00005	0.00008	-0.00002	0.00004	-0.00001	0.00002	-0.00001	0.00001	-0.00001	0.00001
T(SECS)	6.05			5.79				5.54				5.31		5.10		4.89
C(K/SEC)	3.800			3.750				3.700				3.650		3.600		3.550
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU
1	-0.00613	0.00030	-0.00676	0.00035	-0.00745	0.00039	-0.00822	0.00045	-0.00910	0.00051	-0.01009	0.00059	-0.01118	0.00068	-0.01236	0.00078
2	-0.01149	0.00131	-0.01259	0.00153	-0.01380	0.00179	-0.01512	0.00209	-0.01661	0.00245	-0.01828	0.00288	-0.01999	0.00331	-0.02184	0.00378
3	-0.00938	0.00324	-0.01008	0.00382	-0.01081	0.00449	-0.01159	0.00529	-0.01242	0.00623	-0.01331	0.00734	-0.01433	0.00831	-0.01536	0.00938
4	-0.02587	0.01582	-0.02726	0.01719	-0.02861	0.01862	-0.02993	0.02011	-0.03123	0.02169	-0.03251	0.02337	-0.03399	0.02499	-0.03549	0.02669
5	-0.02378	0.01550	-0.02486	0.01675	-0.02588	0.01804	-0.02683	0.01935	-0.02772	0.02071	-0.02855	0.02211	-0.02949	0.02309	-0.03049	0.02469
6	-0.03929	0.02977	-0.04041	0.03183	-0.04135	0.03386	-0.04208	0.03586	-0.04263	0.03782	-0.04299	0.03975	-0.04349	0.04179	-0.04389	0.04379
7	-0.03389	0.03758	-0.03403	0.03900	-0.03392	0.04021	-0.03358	0.04119	-0.03300	0.04192	-0.03221	0.04240	-0.03149	0.04169	-0.03079	0.04119
8	-0.04657	0.05612	-0.04547	0.05658	-0.04400	0.05655	-0.04221	0.05602	-0.04014	0.05503	-0.03783	0.05358	-0.03569	0.05169	-0.03349	0.04979
9	-0.02348	0.03537	-0.02182	0.03413	-0.02007	0.03256	-0.01826	0.03069	-0.01643	0.02860	-0.01463	0.02633	-0.01283	0.02449	-0.01103	0.02219
10	-0.01223	0.02366	-0.01063	0.02142	-0.00912	0.01912	-0.00772	0.01684	-0.00644	0.01461	-0.00529	0.01250	-0.00429	0.01039	-0.00329	0.00929
11	-0.00658	0.01274	-0.00542	0.01092	-0.00439	0.00921	-0.00350	0.00763	-0.00273	0.00621	-0.00210	0.00496	-0.00159	0.00374	-0.00109	0.00274
12	-0.00354	0.00686	-0.00276	0.00557	-0.00211	0.00443	-0.00158	0.00346	-0.00116	0.00264	-0.00083	0.00197	-0.00059	0.00138	-0.00034	0.00109
13	-0.00191	0.00369	-0.00141	0.00284	-0.00107	0.00213	-0.00072	0.00156	-0.00049	0.00112	-0.00033	0.00078	-0.00019	0.00044	-0.00014	0.00029
14	-0.00059	0.00115	-0.00042	0.00084	-0.00029	0.00061	-0.00019	0.00042	-0.00013	0.00029	-0.00008	0.00019	-0.00003	0.00014	-0.00001	0.00009
15	-0.00131	0.00251	-0.00086	0.00173	-0.00056	0.00116	-0.00035	0.00075	-0.00021	0.00048	-0.00012	0.00029	-0.00007	0.00014	-0.00001	0.00009
16	-0.00029	0.00054	-0.00017	0.00033	-0.00009	0.00019	-0.00005	0.00011	-0.00003	0.00006	-0.00001	0.00003	-0.00001	0.00001	-0.00001	0.00001
17	-0.00007	0.00012	-0.00003	0.00006	-0.00002	0.00003	-0.00001	0.00002	-0.00001	0.00001	-0.00001	0.00001	-0.00001	0.00001	-0.00001	0.00001
18	-0.00002	0.00003	-0.00001	0.00001	-0.00001	0.00001	-0.00001	0.00001	-0.00001	0.00001	-0.00001	0.00001	-0.00001	0.00001	-0.00001	0.00001
19	-0.00000	0.00001	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000	-0.00000	0.00000
T(SECS)	4.70			4.52				4.35				4.20		4.05		3.92
C(K/SEC)	3.500			3.450				3.400				3.350		3.300		3.250
M	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU	DC/DRHO	DC/DMU
1	-0.01123	0.00068	-0.01253	0.00079	-0.01405	0.00091	-0.01578	0.00106	-0.01777	0.00124	-0.02003	0.00145	-0.02236	0.00166	-0.02469	0.00187
2	-0.02018	0.00340	-0.02234	0.00401	-0.02481	0.00475	-0.02762	0.00562	-0.03080	0.00666	-0.03439	0.00788	-0.03799	0.00909	-0.04158	0.01030
3	-0.01428	0.00867	-0.01535	0.01025	-0.01651	0.01212	-0.01778	0.01433	-0.01915	0.01693	-0.02064	0.01996	-0.02166	0.02004	-0.02166	0.02004
4	-0.03378	0.02514	-0.03503	0.02702	-0.03627	0.02903	-0.03744	0.03113	-0.03856	0.03333	-0.03960	0.03563	-0.04069	0.03671	-0.04178	0.03779
5	-0.02932	0.02356	-0.03003	0.02505	-0.03066	0.02659	-0.03120	0.02814	-0.03163	0.02470	-0.03194	0.02126	-0.03226	0.01771	-0.03256	0.01421
6	-0.04315	0.04162	-0.04313	0.04343	-0.04292	0.04515	-0.04249	0.04675	-0.04185	0.04819	-0.04101	0.04946	-0.03949	0.04079	-0.03879	0.04169
7	-0.03122	0.04262	-0.03004	0.04258	-0.02870	0.04228	-0.02720	0.04169	-0.02558	0.04083	-0.02387	0.03972	-0.02216	0.03886	-0.02045	0.03771
8	-0.03532	0.05172	-0.03267	0.04548	-0.02992	0.04692	-0.02713	0.04407	-0.02435	0.04102	-0.02163	0.03783	-0.01899	0.03458	-0.01624	0.03158
9	-0.01287	0.02395	-0.01119	0.02151	-0.00962	0.02151	-0.00962	0.01909	-0.00816	0.01672	-0.00684	0.01447	-0.00566	0.01236	-0.00449	0.01019
10	-0.00428	0.01053	-0.00341	0.00874	-0.00268	0.00715	-0.00207	0.00575	-0.00158	0.00454	-0.00118	0.00357	-0.00084	0.00264	-0.00054	0.00219
11	-0.00158	0.00390	-0.00117	0.00300	-0.00085	0.00227	-0.00061	0.00168	-0.00042	0.00123	-0.00029	0.00088	-0.00019	0.00044	-0.00014	0.00029
12	-0.00058	0.00144	-0.00040	0.00103	-0.00027	0.00072	-0.00018	0.00049	-0.00011	0.000333						

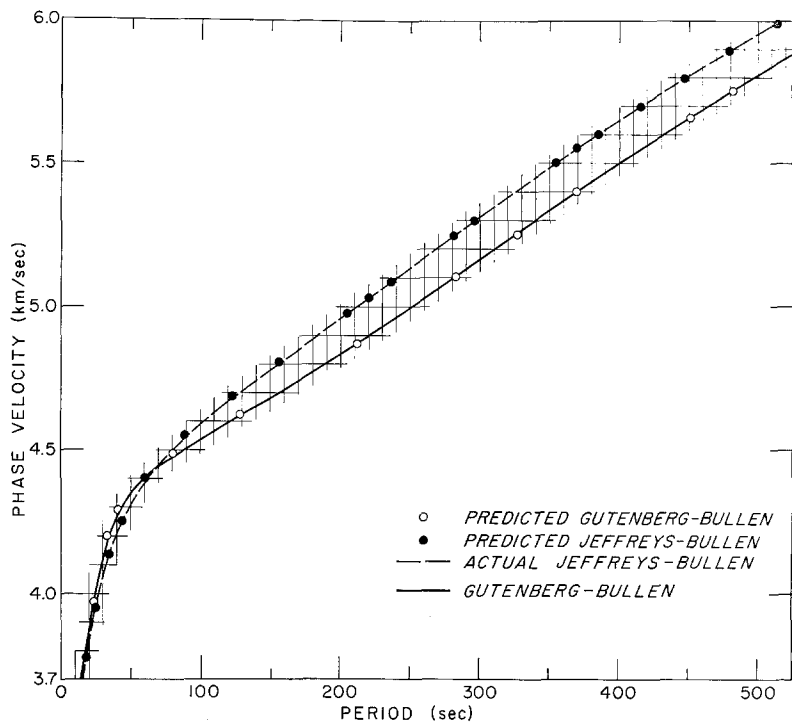


FIG. 1. Results of a numerical experiment in which the known dispersion results and partial derivative tables for a Jeffreys-Bullen type earth model are used to predict dispersion for a model with a Gutenberg-Bullen upper mantle and *vice versa*.

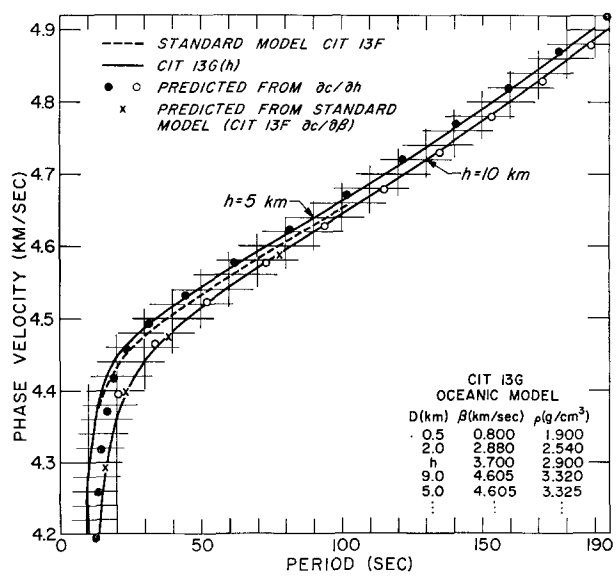


FIG. 2. Results of numerical experiment using equation 17 to predict effect of a change in thickness of a crustal layer compared with results obtained by modifying the shear velocities in the upper 250 km. of the standard model CIT13F so as to correspond to the desired structure.

the resulting partial derivative curves shed considerable light on the meaning and interpretation of dispersion data. The partial derivative curves tend to be bell shaped (on semi-log and log-log graphs) and peak at periods corresponding to horizontal wave lengths of roughly 2 to 6 times the layer depth. The peak, or maximum effect, decreases with increasing depth of the layer for a layer of a given thickness. The near surface layers dominate over quite a wide frequency range and their properties must be well known before any attempt is made to analyze the deeper layers, i.e., structures should be designed from the top down.

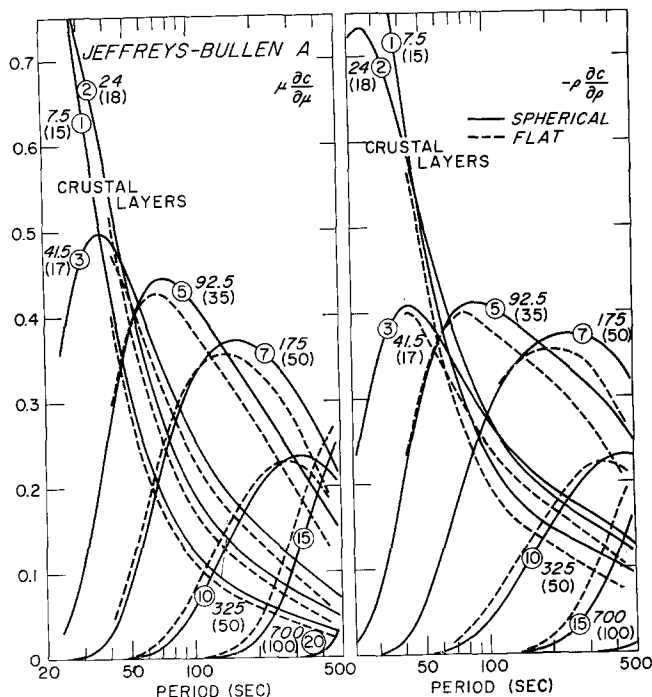


FIG. 3. Phase velocity perturbations (km/sec) for Jeffreys-Bullen A Earth Model. The parameters are layer number (circled), depth to layer midpoint (in km.) and layer thickness (in parentheses). To use, multiply the ordinate by the fractional change of the appropriate variable. Attenuation can be computed by allowing the perturbations to become complex.

These curves may be used to determine which section of the waveguide is contributing to an observed set of dispersion data and which sections are beyond the reach of the observations. They can be used to design a structure which satisfies the data and indicate how much freedom can be taken with the resulting model without violating the data to more than the experimental error.

Figure 3 shows partial derivative curves for the Jeffreys-Bullen Continental Model. In this model the rigidity and density increase monotonically with depth. Since the displacements for such a model die off approximately exponentially with depth, the partial derivative curves are roughly symmetrical on a logarithmic period scale and the peak effect divided by the layer thickness dies off uniformly with layer depth. Also shown are the partial derivatives for the equivalent flat layered model. Note that the effect of sphericity is to shift the curves to longer periods and slightly

reduce the symmetry. These curves may be normalized by dividing by the layer thickness.

Corresponding curves for the Gutenberg IV continental model (MacDonald and Ness, 1961) are shown in figure 4. This model has a velocity reversal in the upper mantle and the possibility exists for efficient channeling of certain periods. This effect shows up in a skewing of the partial derivative curves toward shorter periods.

The oceanic model CIT 9 has a more pronounced low-velocity zone and the skewing in figures 5 and 6 is even more apparent. An additional phenomenon, that of a cut-off period, also shows up now. A low rigidity region partially decouples the crust from the mantle. At periods greater than the decoupling period, which in this

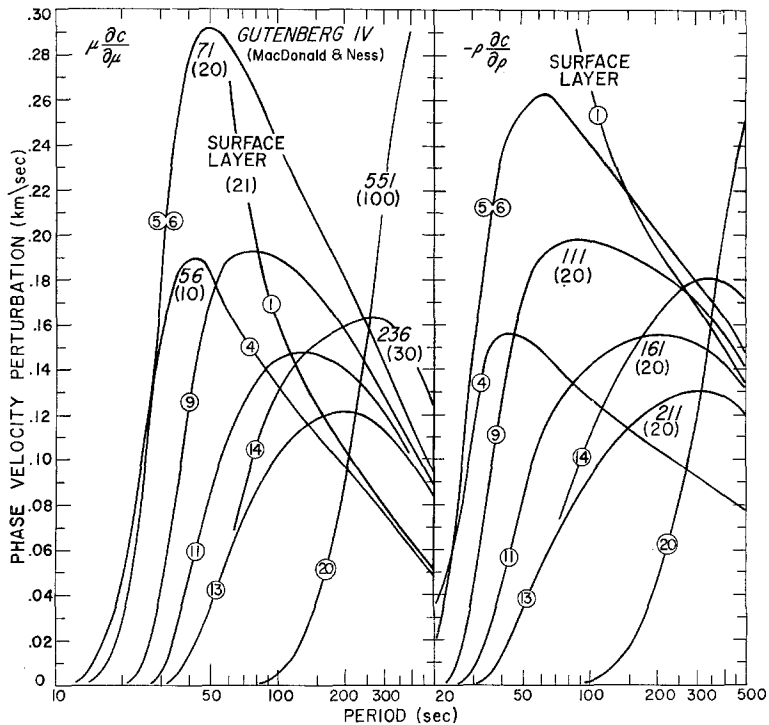


FIG. 4. Phase velocity perturbations (km/sec) for Gutenberg IV Earth Model.

case is about 23 seconds, a large amount of energy is in the low-velocity channel. At shorter periods most of the energy is in the crustal layers. The decoupling phenomenon also manifests itself by nearly vertical portions in the phase and group velocity curves.

Figures 7 and 8 show the partial derivative curves for the standard model designated CIT13F for the period range 10 to 1000 seconds. Note the double logarithmic scale. Figure 9 shows the shear velocity structure of this model and, for comparison, two other proposed oceanic models. The ticks on the ordinate show how this model was split into layers.

These curves all show the equal role played by density and rigidity in the Love wave problem. These are the natural variables in any theoretical discussion. However, the shear velocity and the density are more often the variables of interest in

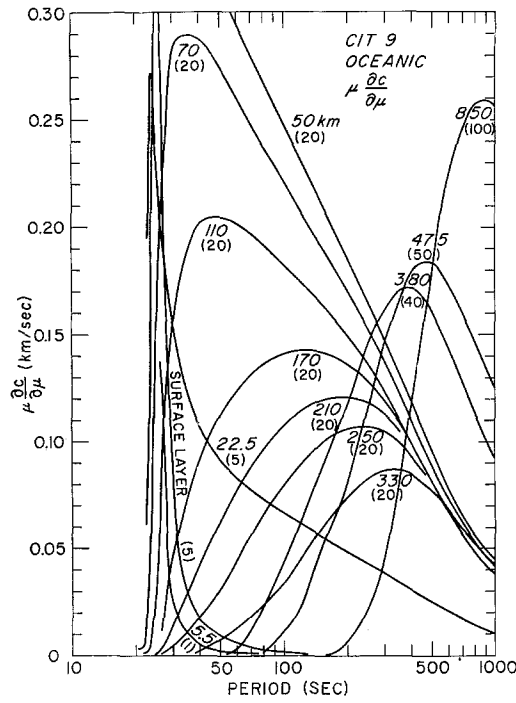


FIG. 5. Phase velocity perturbations due to a change in various layer rigidities (density held constant) for model CIT9.

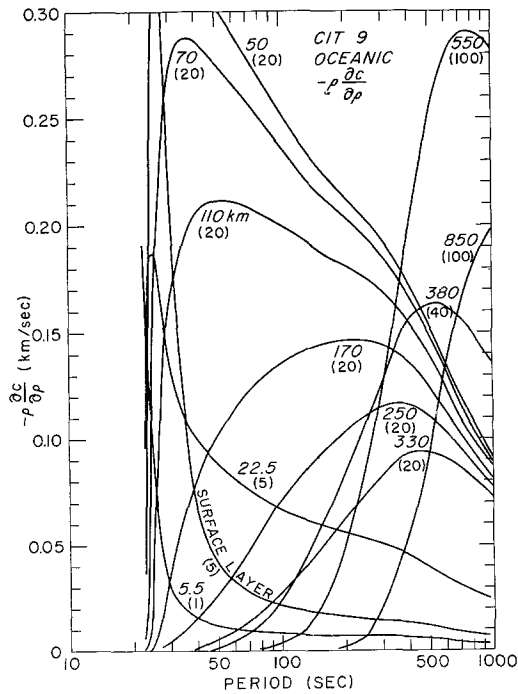


FIG. 6. Phase velocity perturbations due to a change in various layer densities (rigidity held constant) for model CIT9.

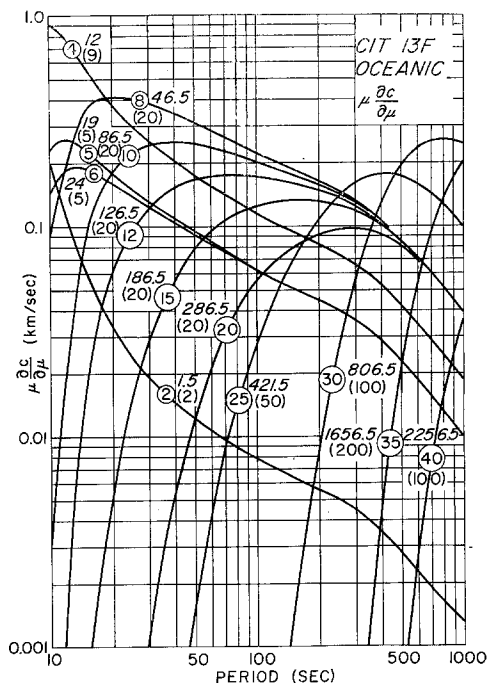


FIG. 7. Phase velocity perturbations corresponding to rigidity changes (density held constant) in various layers of the CIT13F Standard Oceanic Model. To use multiply ordinate by the fractional change in the layer rigidity being modified. The circled numbers are layer designations, italicized numbers are depths to layer midpoints, parenthetical numbers are layer thicknesses.

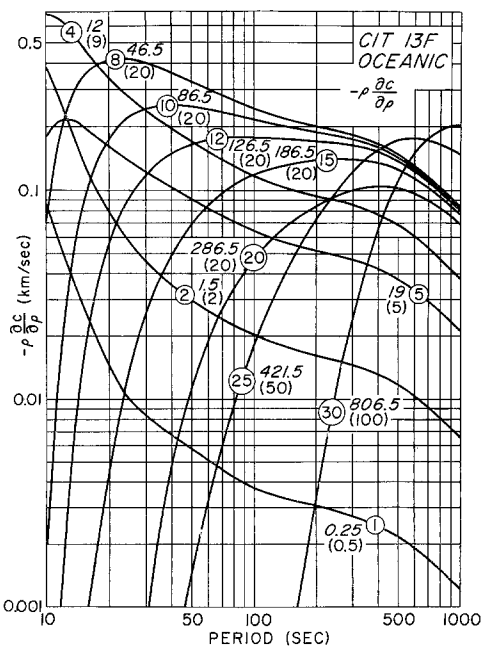


FIG. 8. Phase velocity perturbations corresponding to density changes (rigidity held constant) in various layers of the CIT13F Standard Oceanic Model. See caption of figure 7 for explanation. If the parameter perturbations are imaginary, then the curves are proportional to the resulting Q^{-1} .

the corresponding experimental problem since travel time results provide the starting point for most surface wave interpretations. Figure 10 shows the relative effect of shear velocity perturbations (density held constant) and density perturbations (velocity held constant) and indicates the predominant role played by the shear velocity. It is clear that the reliability of density determinations using Love wave results will be an order of magnitude less than the reliability of the shear velocity determinations. The situation improves, of course, if the shear velocity is known

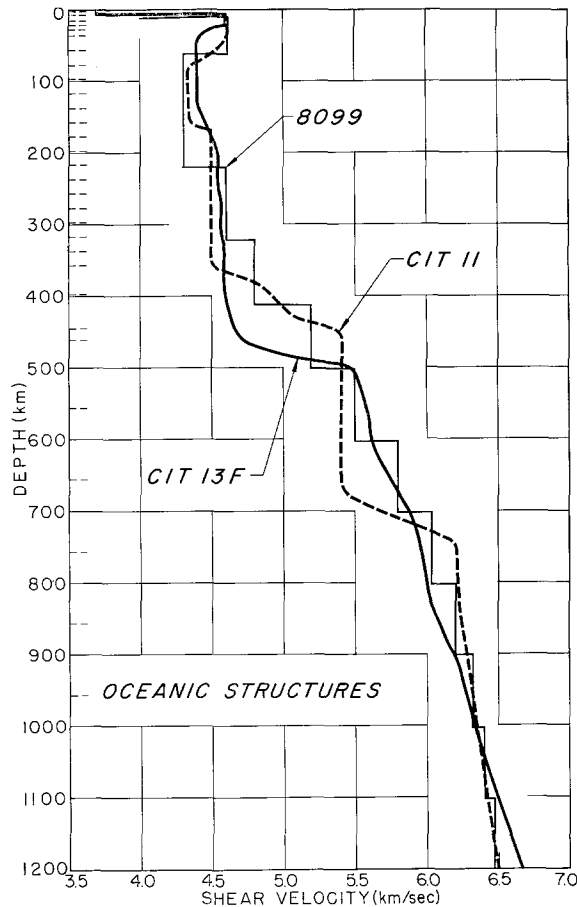


FIG. 9. Shear velocity structures for CIT13F, CIT11 and 8099.

independently. In fact, surface waves and free oscillations promise to be an important additional source of information concerning the density structure in regions of the Earth where the seismic velocities are well known.

The similarity in shape of the partial derivative curves for the various layers suggests that a considerable lack of uniqueness is involved when an attempt is made to find a linear combination of the theoretical perturbation curves that match an observed "discrepancy curve." This question is discussed more rigorously in a forthcoming paper (Archambeau and Anderson, in preparation). Ambiguity can be reduced by using higher mode data as a supplementary constraint. Phase velocity

perturbations for the 2nd Love Mode for the Gutenberg-Birch Continental Model are shown in figure 11. Note the double peaked character of these curves compared with the single peak fundamental mode curves. Of particular interest here is the suggestion that this mode, the so-called *Sa* wave, in the period range of about 15–20 seconds, “sees” the upper mantle from about 80–150 km. more than it sees the crustal layers, making this a particularly powerful phase for the study of the upper mantle.

The direct calculation of group velocity perturbations requires special techniques not covered in this paper. It is easy, however, to devise numerical schemes for determining a group velocity correction from derived phase velocity corrections.

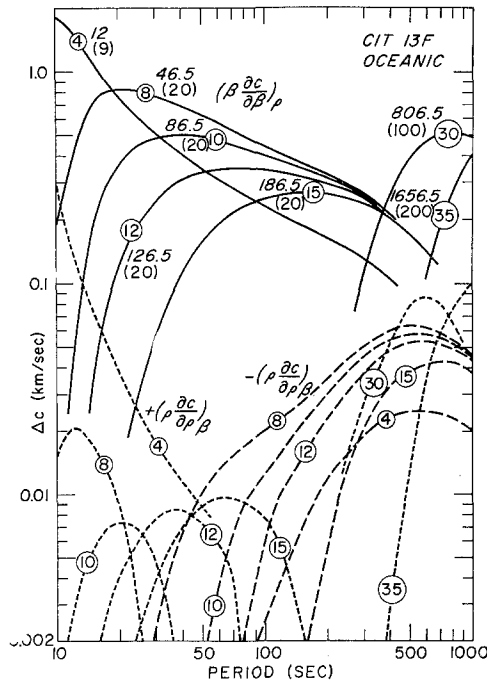


FIG. 10. Phase velocity perturbations for CIT13F Standard Oceanic Model with shear velocity and density as the independent variables.

For example, a two-point difference scheme yields

$$U = U_0(1 + \alpha)$$

where

$$\alpha = (\delta k_{-1} - \delta k_{+1}) / (k_{+1} - k_{-1})$$

$$\delta k = -(k \delta c / c)$$

$$k = 2\pi / cT$$

where the δk are those determined at periods adjacent to the period for which group velocity is desired. Tables 12 and 13 provide group velocity information for the standard models.

A later paper will deal with the free oscillation problem. The question in this case is how the period (σ) of a free oscillation of order n is affected by changes in the physical properties. Meanwhile, torsional oscillation data for periods less

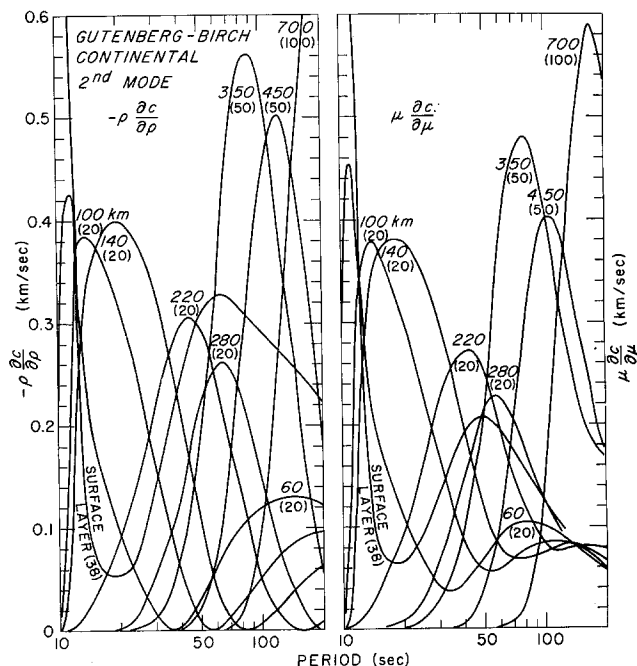


FIG. 11. Phase velocity perturbations for 1st higher Love mode for Gutenberg-Birch Continental Model. Note the "windows" that occur in certain period ranges which allow deeper layers to be seen through the nearer surface layers.

than 1000 seconds may be interpreted by converting it to dispersion data by computing

$$T = 2\pi/\sigma$$

$$c = 2\pi/[(n + \frac{1}{2}) \cdot T]$$

and proceeding as in the travelling wave case.

THE INVERSE SURFACE WAVE PROBLEM

The usual method of interpreting surface wave data is by an indirect trial and error procedure. The tables and graphs in this paper can be used as guidelines in a technique of this sort. Dorman and Ewing (1962) systematized the trial and error method by numerically solving a simultaneous set of linear equations relating empirically determined parameter corrections to the discrepancy between the

observed and the numerical trial dispersion data. The tables of theoretical partial derivatives presented in this paper can be used to replace the numerical derivatives in this technique. Preliminary results utilizing this approach were presented at the recent IUGG meeting (Anderson, *et al.* (1963), Archambeau and Anderson (1963)). Alternatively, the closed form expressions for the various partial derivatives can be used to do the same sort of thing completely analytically to avoid the numerical difficulties arising in the attempted inversion of almost singular matrices.

TABLE 12
PERIOD (T), PHASE VELOCITY (c) AND GROUP VELOCITY (U) FOR GUTENBERG BIRCH II
CONTINENTAL MODEL

T (secs)	c (km/sec)	U (km/sec)	T (secs)	c (km/sec)	U (km/sec)
1079.48	6.72	6.060	60.37	4.41	4.1240
951.57	6.62	5.783	56.60	4.39	4.0967
861.17	6.52	5.576	53.17	4.37	4.0664
788.74	6.42	5.406	50.07	4.35	4.0339
673.13	6.22	5.131	47.28	4.33	3.9994
580.00	6.02	4.912	44.78	4.31	3.9637
500.19	5.82	4.734	42.52	4.29	3.9273
422.12	5.60	4.5792	40.47	4.27	3.8909
388.89	5.50	4.5220	38.62	4.25	3.8549
356.64	5.40	4.4727	36.92	4.23	3.8198
325.10	5.30	4.4307	35.36	4.21	3.7860
294.04	5.20	4.3955	33.91	4.19	3.7537
263.25	5.10	4.3664	32.57	4.17	3.7231
232.54	5.00	4.3424	31.31	4.15	3.6944
201.79	4.90	4.3222	30.12	4.13	3.6678
170.93	4.80	4.3039	28.99	4.11	3.6431
155.49	4.75	4.2946	27.91	4.09	3.6204
140.07	4.70	4.2847	26.88	4.07	3.5998
124.77	4.65	4.2732	25.89	4.05	3.5812
109.70	4.60	4.2588	24.93	4.03	3.5645
106.74	4.59	4.2554	23.99	4.01	3.5497
100.87	4.57	4.2479	23.53	4.00	3.5430
95.10	4.55	4.2393	21.30	3.95	3.5161
89.47	4.53	4.2293	19.14	3.90	3.4993
84.00	4.51	4.2177	17.00	3.85	3.4916
81.33	4.50	4.2111	14.83	3.80	3.4917
78.73	4.49	4.2041	12.56	3.75	3.4982
73.70	4.47	4.1883	10.15	3.70	3.5089
68.94	4.45	4.1698	7.50	3.65	3.5089
64.49	4.43	4.1484	4.52	3.60	3.5309

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TABLE 13
PERIOD (T), PHASE VELOCITY (c), AND GROUP VELOCITY (U) FOR CIT13F OCEANIC MODEL

T (secs)	c (km/sec)	U (km/sec)
1009.06	6.72	5.96
899.29	6.62	5.71
818.64	6.52	5.52
696.84	6.32	5.216
602.14	6.12	4.978
522.28	5.92	4.787
451.55	5.72	4.635
412.00	5.60	4.561
380.15	5.50	4.509
318.19	5.30	4.433
287.45	5.20	4.4093
256.41	5.10	4.3944
224.67	5.00	4.3886
191.71	4.90	4.3915
156.82	4.80	4.4020
119.10	4.70	4.4162
98.96	4.65	4.4211
78.14	4.60	4.4206
57.53	4.55	4.4109
38.58	4.50	4.3927
23.42	4.45	4.354
15.56	4.40	4.2349
12.55	4.35	4.0593
11.00	4.30	3.889
9.23	4.20	3.605
7.29	4.00	3.2067
6.32	3.85	2.9920
4.05	3.30	2.281

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