

## Surface Wave Energy from Point Sources in Plane Layered Earth Models<sup>1</sup>

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The total energy contained in a surface wave can be computed from its propagation-corrected spectrum by integrating over the surface of the earth and over the depth of the wave guide. The former requires knowledge of the radiation pattern of the source. The latter requires only a knowledge of the variation of physical properties with depth. In this paper the depth integration is performed for a continental and an oceanic earth model for three Rayleigh modes and four Love modes. The results are presented in tables and graphs in such a way that it is convenient to convert an observed surface wave displacement or displacement spectrum to total energy density. If the surface radiation pattern is known, the surface integration then yields the total energy in the observed spectrum. The partitioning of energy between surface wave modes is computed for several simple sources at the surface and at depth, making it possible to estimate the energy contained in frequency bands or modes which are inaccessible for direct analysis. The increasing importance of the higher modes in the total energy budget at short periods and for channel depth sources is demonstrated. The shapes of the spectrums are diagnostic of source orientation and depth.

### INTRODUCTION

Energy is an important concept in both theoretical and experimental seismology. It is involved in the derivation of the wave equation and in the variational methods of theoretical analysis. It has recently found application in the universal dispersion theory [Anderson, 1964], the earth anelasticity theory [Anderson and Archambeau, 1964], the inversion theory [Archambeau and Anderson, 1963], and the analytic calculation of group velocity [Jeffreys, 1961].

Energy radiation and energy partition of surface waves are important to our understanding of properties of the seismic source such as magnitude, mechanism, and depth. Even more fundamental is the question of energy balance of the earth. It has never been possible to measure all of the energy radiated in all directions at all frequencies from a single earthquake, much less the total annual tectonic energy release. It will never be possible, of course, to account for all the energy radiated by an earthquake, but the

present methods of estimating energy from the magnitude are clearly unsatisfactory.

In this paper we compute the partition of energy among various surface wave modes for horizontal and vertical point sources at various depths in realistic earth models. Basic to this task is the excitation theory of Harkrider [1964].

In addition to explaining the presence or absence of individual modes and their relative energies, the theoretical results allow us to estimate the energy in frequency bands and modes that are not accessible for direct measurement. The partition functions and observed surface amplitudes can then be used in calculating the minimum seismic energy associated with an earthquake. Magnitudes and magnitude scales will have to be consistent with this observed minimum energy. Also, the strain energy release of a proposed source mechanism must be able to account for the observed seismic energy release.

In this paper we give expressions for the surface wave spectral energy density for various source depths and orientations and obtain the short- and long-period asymptotes. Relations are also given for obtaining the necessary medium response functions in terms of normalized energy integrals. These expressions are then

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evaluated and tabulated for a continental and an oceanic earth model.

The energy integrals given in this paper are useful in calculating a great variety of important seismic parameters, such as:

(a) Accurate values of the group velocity and the variation of relative excitation with frequency and mode.

(b) The effect of any parameter in any layer on the phase velocity [Anderson, 1964].

(c) The attenuation of surface waves, given the variation of anelasticity with depth [Anderson and Archambeau, 1964; Anderson et al., 1965].

(d) The inverse of the two preceding problems.

(e) The energy for individual modes of surface waves from the observed or known spectrum of an identifiable mode.

(f) The energy partition as a function of depth of surface wave modes for seismic sources at the surface and at depth.

### Symbols.

$T^R, T^L$ , Rayleigh and Love kinetic energy density integrals, normalized to surface displacements.

$V^R, V^L$ , Rayleigh and Love potential energy density integrals, normalized to surface displacements.

$\omega$ , angular frequency.

$k_R, k_L$ , Rayleigh and Love angular wave numbers.

$z$ , vertical or depth coordinate.

$I_0^R, I_1^R, I_2^R, I_3^R$ , depth integrations defined by (3).

$I_0^L, I_1^L, I_2^L$ , depth integrations defined by (4).

$Q, W$ , normalized horizontal and vertical Rayleigh displacements.

$V$ , normalized Love displacements.

$\dot{u}^*(z)/\dot{w}_0, \dot{v}(z)/\dot{v}_0, \dot{w}(z)/\dot{w}_0$ , Haskell's plane wave particle velocity (or displacement) ratios at depth  $z$ .

$\sigma_R^*(z)$ , Haskell's plane wave normal stress factor at depth  $z$ .

$\tau_R(z), \tau_L^*(z)$ , Haskell's Rayleigh and Love tangential stress factors at depth  $z$ .

$d_j$ , thickness of layer  $j$ .

$\alpha_j$ , compressional velocity of layer  $j$ .

$\beta_j$ , shear velocity of layer  $j$ .

$\rho_j$ , density of layer  $j$ .

$\mu_j$ , rigidity of layer  $j$ .

$\lambda_j$ , Lamé's constant of layer  $j$ .

$C_R, C_L$ , Rayleigh and Love phase velocities.

$U_R, U_L$ , Rayleigh and Love group velocities.

$A_R, A_L$ , Rayleigh and Love medium response functions.

$\mu_P, \rho_P, \beta_P$ , composite plate rigidity, density, and velocity defined by (14).

$V_{Rj}$ , Rayleigh velocity of layer  $j$ .

$\gamma_j$ , layer  $j$  coefficient defined by (16).

$E^R, E^L$ , Rayleigh and Love spectrum energy densities per unit propagation path.

$r$ , epicenter distance.

$\theta$ , azimuth angle.

$h$ , source depth.

$[w_0(r, \theta, h)]_R$ , vertical spectral surface displacement for Rayleigh waves.

$[v_0(r, \theta, h)]_L$ , horizontal spectral surface displacement for Love waves.

$\langle L \rangle$ , spectral source strength.

$E_{V^R}, E_{V^L}$ , Rayleigh and Love spectrum energy densities per unit propagation path for a vertical force.

$E_{H^R}, E_{H^L}$ , Rayleigh and Love spectrum energy densities per unit propagation path for horizontal force.

### FUNDAMENTAL FORMULAS

The basic integrals for kinetic and potential energy density, normalized to the surface displacement, are given by

$$2T^R = \omega^2 I_0^R \quad (1)$$

$$2V^R = k_R^2 I_1^R + 2k_R I_2^R + I_3^R$$

for Rayleigh waves and

$$2T^L = \omega^2 I_0^L \quad (2)$$

$$2V^L = k_L^2 I_1^L + I_2^L$$

for Love waves, with

$$I_0^R = \int_0^\infty \rho(Q^2 + W^2) dz$$

$$I_1^R = \int_0^\infty \{(\lambda + 2\mu)Q^2 + \mu W^2\} dz \quad (3)$$

$$I_2^R = \int_0^\infty \left\{ \lambda Q \frac{dW}{dz} - \mu W \frac{dQ}{dz} \right\} dz$$

$$I_3^R = \int_0^\infty \left\{ (\lambda + 2\mu) \left( \frac{dW}{dz} \right)^2 + \mu \left( \frac{dQ}{dz} \right)^2 \right\} dz$$

and

$$\begin{aligned}
 I_0^L &= \int_0^\infty \rho V^2 dz \\
 I_1^L &= \int_0^\infty \mu V^2 dz \\
 I_2^L &= \int_0^\infty \mu \left( \frac{dV}{dz} \right)^2 dz
 \end{aligned} \tag{4}$$

[Jeffreys, 1961]. The normalized displacements and displacement derivatives in the integrands of (3) and (4) can be expressed in terms of the Thomson-Haskell layer vector elements [Haskell, 1953]:

$$\begin{aligned}
 Q &= \dot{u}^*(z)/\dot{w}_0 \\
 W &= \dot{w}(z)/\dot{w}_0
 \end{aligned} \tag{5}$$

$$\begin{aligned}
 \frac{dQ}{dz} &= \frac{k_R}{\mu} \left\{ \mu \left[ \frac{\dot{w}(z)}{\dot{w}_0} \right] + \left[ \frac{\tau_R(z) C_R}{\dot{w}_0} \right] \right\} \\
 \frac{dW}{dz} &= -\frac{k_R}{(\lambda + 2\mu)} \\
 &\quad \cdot \left\{ \lambda \left[ \frac{\dot{u}^*(z)}{\dot{w}_0} \right] + \left[ \frac{\sigma_R^*(z) C_R}{\dot{w}_0} \right] \right\}
 \end{aligned}$$

and

$$\begin{aligned}
 V &= \dot{v}(z)/\dot{v}_0 \\
 dV/dz &= -(k_L/\mu) [\tau_L^*(z) C_L/\dot{v}_0]
 \end{aligned} \tag{6}$$

for a layered half-space composed of  $n$  elastic layers, where  $\lambda_j = \rho_j(\alpha_j^2 - 2\beta_j^2)$  and  $\mu_j = \rho_j\beta_j^2$ . For computing purposes the relations between the vector elements, the phase velocities  $C_R$  and  $C_L$ , and the Thomson-Haskell layer matrices can be found in Harkrider [1964].

The Thomson-Haskell matrix technique has been used in two ways to evaluate the energy integrals. Wu [1966] used the matrix method in calculating values of the integrands at various depths for the fundamental modes and then computed the kinetic energy in integrals of (1) and (2) by numerical integration. Anderson [1964] used the matrix-calculated eigenfunctions in an analytic evaluation of the Love wave integrals. Anderson's technique is used in this paper.

The energy integrals can be used in calculating group velocity and the medium response without differentiation. Group velocity is determined by equating the kinetic and potential

energy expressions in (1) and (2) and then invoking Rayleigh's principle [Meissner, 1926; Jeffreys, 1934, 1961]. The resulting expressions for group velocity are

$$\begin{aligned}
 U_R &= (I_1^R + I_2^R/k_R)/(C_R I_0^R) \\
 U_L &= I_1^L/(C_L I_0^L)
 \end{aligned} \tag{7} \tag{8}$$

This technique has been extended to group velocity calculations for spherical earth models by Takeuchi *et al.* [1962, 1964] and Kovach and Anderson [1964].

A modification of this technique allows one to calculate the changes in Rayleigh and Love wave phase velocities resulting from changes in the physical properties of the wave guide [Jeffreys, 1961; Anderson, 1964; Takeuchi *et al.*, 1964]. These perturbations can, in turn, be used for the calculation of the attenuation of surface waves as a function of period for realistic anelastic earth models [Anderson and Archambeau, 1964; Anderson *et al.*, 1965].

Integral relations similar to (7) and (8) can also be obtained for the medium response. Comparing the two-dimensional or line-source solutions of Neigaus [Kellis-Borok and Yanovskaya, 1962] with the three-dimensional or point-source solutions of Harkrider [1964], we see that the medium response can be expressed as

$$\begin{aligned}
 A_R &= [2C_R U_R I_0^R]^{-1} \\
 &= [2(I_1^R + I_2^R/k_R)]^{-1}
 \end{aligned} \tag{9}$$

$$A_L = [2C_L U_L I_0^L]^{-1} = [2I_1^L]^{-1} \tag{10}$$

It is interesting that in (7), (8), (9), and (10) we are able to express the group velocity and the medium response in terms of the normalized energies which are used to calculate phase velocity perturbations [Anderson, 1964; Takeuchi *et al.*, 1964]. These relations make it convenient to calculate partial derivatives, not only for phase velocity but for the complete spectral response of any reasonable structure due to a change of elastic parameter at depth.

By using analytical expressions for the depth integrations, we were able to derive the short- and long-period limits for the fundamental mode Rayleigh and Love wave energy integrals. For high frequencies, the asymptotic form of  $I_0^L$  is

$$I_0^L \rightarrow d_1 \rho_1 / 2 \tag{11}$$

TABLE 1. Layer parameters for the oceanic and shield earth models.

Ocean

| D     | ALPHA   | BETA   | RHO    | MU         | LAMDA      | DEPTH   | M  |
|-------|---------|--------|--------|------------|------------|---------|----|
| 5.00  | 1.5200  | 1.0000 | 1.0300 | 0.         | 2.379712   | 2.50    | 0  |
| 1.00  | 2.1000  | 1.0000 | 2.1000 | 2.100000   | 5.061000   | 5.50    | 1  |
| 5.00  | 4.00660 | 3.0000 | 3.4000 | 41.973539  | 42.029035  | 8.50    | 2  |
| 5.00  | 8.1100  | 4.6060 | 3.4000 | 72.131800  | 79.361530  | 15.50   | 3  |
| 5.00  | 8.1200  | 4.6110 | 3.4000 | 72.288488  | 79.599974  | 22.50   | 4  |
| 15.00 | 8.1200  | 4.6100 | 3.4000 | 72.257137  | 79.662676  | 32.50   | 5  |
| 20.00 | 8.0100  | 4.5600 | 3.3700 | 70.074429  | 76.070675  | 50.00   | 6  |
| 20.00 | 7.9500  | 4.5300 | 3.3700 | 70.774429  | 72.784563  | 70.00   | 7  |
| 20.00 | 7.7100  | 4.4000 | 3.3700 | 65.243197  | 69.840218  | 90.00   | 8  |
| 20.00 | 7.6800  | 4.3400 | 3.3300 | 62.722546  | 70.966294  | 110.00  | 9  |
| 20.00 | 7.7770  | 4.3400 | 3.3300 | 62.722546  | 75.999060  | 130.00  | 10 |
| 20.00 | 8.3500  | 4.3400 | 3.3300 | 62.722546  | 79.757827  | 150.00  | 11 |
| 20.00 | 8.1000  | 4.4500 | 3.3300 | 65.942324  | 86.596643  | 170.00  | 12 |
| 20.00 | 8.1200  | 4.4500 | 3.3300 | 65.942324  | 87.676895  | 190.00  | 13 |
| 20.00 | 8.1200  | 4.4500 | 3.3300 | 65.942324  | 87.676895  | 210.00  | 14 |
| 20.00 | 8.1200  | 4.4500 | 3.3300 | 65.942324  | 87.676895  | 230.00  | 15 |
| 20.00 | 8.1200  | 4.4500 | 3.3300 | 65.942324  | 87.676895  | 250.00  | 16 |
| 20.00 | 8.1200  | 4.4500 | 3.3300 | 65.942324  | 87.676895  | 270.00  | 17 |
| 20.00 | 8.1200  | 4.4500 | 3.3300 | 65.942324  | 87.676895  | 290.00  | 18 |
| 20.00 | 8.1200  | 4.4500 | 3.3300 | 65.942324  | 87.676895  | 310.00  | 19 |
| 20.00 | 8.1200  | 4.4500 | 3.3300 | 65.942324  | 87.676895  | 330.00  | 20 |
| 20.00 | 8.2400  | 4.5000 | 3.3900 | 68.647499  | 92.877855  | 350.00  | 21 |
| 10.00 | 8.3000  | 4.5300 | 3.4400 | 70.591894  | 95.797806  | 365.00  | 22 |
| 20.00 | 8.3600  | 4.5600 | 3.4400 | 72.777597  | 99.058397  | 400.00  | 23 |
| 25.00 | 8.7500  | 4.7950 | 3.6840 | 84.702617  | 112.651014 | 482.50  | 24 |
| 20.00 | 9.1500  | 5.1000 | 3.8800 | 98.558205  | 127.767883 | 625.00  | 25 |
| 10.00 | 9.4300  | 5.2170 | 3.9000 | 106.146643 | 134.513813 | 640.00  | 26 |
| 20.00 | 9.7600  | 5.4000 | 3.9200 | 114.307198 | 144.795391 | 655.00  | 27 |
| 25.00 | 9.7650  | 5.4000 | 3.9330 | 114.686278 | 145.695940 | 677.50  | 28 |
| 25.00 | 9.7750  | 5.4000 | 3.9330 | 115.954807 | 146.966506 | 702.50  | 29 |
| 25.00 | 9.7800  | 5.4000 | 3.9600 | 115.473598 | 147.820463 | 727.50  | 30 |
| 25.00 | 9.7840  | 5.4000 | 3.9880 | 116.290077 | 149.177738 | 752.50  | 31 |
| 25.00 | 9.7890  | 5.4000 | 4.0220 | 117.281517 | 150.764442 | 777.50  | 32 |
| 25.00 | 9.7920  | 5.4000 | 4.0560 | 118.272958 | 152.356596 | 802.50  | 33 |
| 25.00 | 9.7960  | 5.4000 | 4.0900 | 119.264398 | 153.948750 | 827.50  | 34 |
| 25.00 | 9.8000  | 5.4000 | 4.1200 | 120.193196 | 155.400395 | 852.50  | 35 |
| 25.00 | 10.1630 | 5.6000 | 4.1650 | 130.614395 | 168.959763 | 877.50  | 36 |
| 25.00 | 10.4880 | 5.8000 | 4.2120 | 141.691675 | 179.928814 | 902.50  | 37 |
| 25.00 | 10.8180 | 6.1000 | 4.2570 | 156.402966 | 191.387039 | 927.50  | 38 |
| 25.00 | 11.1200 | 6.2000 | 4.3000 | 165.291996 | 201.129906 | 952.50  | 39 |
| 25.00 | 11.1350 | 6.2050 | 4.4750 | 172.296558 | 210.254181 | 977.50  | 40 |
| 25.00 | 11.1500 | 6.2100 | 4.6330 | 178.667469 | 218.651192 | 1002.50 | 41 |
| 25.00 | 11.1650 | 6.2180 | 4.7970 | 185.468922 | 227.042854 | 1027.50 | 42 |
| 25.00 | 11.1800 | 6.2260 | 4.9600 | 191.951201 | 235.991001 | 1052.50 | 43 |
| 25.00 | 11.2240 | 6.2500 | 4.9425 | 193.066404 | 236.514317 | 1077.50 | 44 |
| 25.00 | 11.2670 | 6.2750 | 4.9450 | 194.712463 | 238.319519 | 1102.50 | 45 |
| 25.00 | 11.3100 | 6.2970 | 4.9475 | 196.179302 | 240.506287 | 1127.50 | 46 |
| 25.00 | 11.3520 | 6.3200 | 4.9500 | 197.490031 | 241.991287 | 1152.50 | 47 |
| 25.00 | 11.3920 | 6.3400 | 4.9517 | 199.036549 | 244.546944 | 1177.50 | 48 |
| 25.00 | 11.4340 | 6.3600 | 4.9534 | 200.363043 | 246.863354 | 1202.50 | 49 |
| 25.00 | 11.4760 | 6.3750 | 4.9550 | 201.374296 | 249.817837 | 1227.50 | 50 |
| 25.00 | 11.5180 | 6.3900 | 4.9567 | 202.392466 | 252.792294 | 1252.50 | 51 |
| 25.00 | 11.5600 | 6.4050 | 4.9584 | 203.413521 | 255.781784 | 1277.50 | 52 |
| 25.00 | 11.6000 | 6.4210 | 4.9600 | 204.497028 | 258.423523 | 1302.50 | 53 |

Shield

| D     | ALPHA   | BETA   | RHO    | MU         | LAMDA      | DEPTH   | M  |
|-------|---------|--------|--------|------------|------------|---------|----|
| 10.00 | 6.1000  | 3.5400 | 2.3500 | 31.955579  | 30.974339  | 15.25   | 2  |
| 6.50  | 6.1000  | 3.4400 | 2.5000 | 31.955579  | 30.974339  | 13.25   | 2  |
| 5.00  | 6.4000  | 3.7000 | 3.0800 | 42.165199  | 41.826400  | 19.00   | 3  |
| 5.00  | 6.7000  | 3.9200 | 3.4200 | 52.553087  | 48.417622  | 24.00   | 4  |
| 5.00  | 6.7000  | 3.9200 | 3.4200 | 52.553087  | 48.417622  | 29.00   | 5  |
| 3.50  | 6.7000  | 3.9200 | 3.4200 | 52.553087  | 48.417622  | 33.25   | 6  |
| 5.00  | 6.1500  | 4.7500 | 3.4200 | 77.163750  | 77.163750  | 37.50   | 7  |
| 20.00 | 8.1600  | 4.7500 | 3.4200 | 77.163750  | 73.395247  | 50.00   | 8  |
| 20.00 | 8.2100  | 4.7500 | 3.4200 | 77.163750  | 76.794515  | 70.00   | 9  |
| 20.00 | 8.2600  | 4.7500 | 3.4200 | 77.163750  | 79.010887  | 90.00   | 10 |
| 20.00 | 8.3000  | 4.7500 | 3.4200 | 77.163750  | 82.413103  | 110.00  | 11 |
| 20.00 | 8.3000  | 4.7000 | 3.4000 | 75.105998  | 84.013996  | 130.00  | 12 |
| 20.00 | 8.2840  | 4.5800 | 3.4000 | 71.319757  | 80.684305  | 150.00  | 13 |
| 20.00 | 8.2840  | 4.5400 | 3.4000 | 70.079437  | 93.164946  | 170.00  | 14 |
| 20.00 | 8.2840  | 4.5000 | 3.4100 | 70.438961  | 95.438961  | 190.00  | 15 |
| 20.00 | 8.2840  | 4.5400 | 3.4200 | 70.491670  | 93.712975  | 210.00  | 16 |
| 20.00 | 8.2840  | 4.5400 | 3.4500 | 71.110018  | 94.535019  | 230.00  | 17 |
| 20.00 | 8.2840  | 4.5400 | 3.4500 | 71.110018  | 94.535019  | 250.00  | 18 |
| 20.00 | 8.2840  | 4.5400 | 3.4500 | 71.110018  | 94.535019  | 270.00  | 19 |
| 20.00 | 8.2840  | 4.5400 | 3.4500 | 71.110018  | 94.535019  | 290.00  | 20 |
| 20.00 | 8.2840  | 4.5400 | 3.4500 | 71.110018  | 94.535019  | 310.00  | 21 |
| 20.00 | 8.2840  | 4.5400 | 3.4500 | 71.110018  | 94.535019  | 330.00  | 22 |
| 20.00 | 8.3130  | 4.5400 | 3.4500 | 71.110018  | 96.195551  | 350.00  | 23 |
| 10.00 | 8.5070  | 4.6830 | 3.4500 | 74.331937  | 100.926821 | 365.00  | 24 |
| 20.00 | 8.7000  | 4.7500 | 3.4500 | 77.840624  | 105.449245 | 380.00  | 25 |
| 25.00 | 8.7400  | 4.7500 | 3.6600 | 82.578750  | 114.421106 | 402.50  | 26 |
| 20.00 | 8.7600  | 4.7500 | 3.8800 | 87.542500  | 122.656883 | 425.00  | 27 |
| 10.00 | 9.0380  | 5.0000 | 3.9000 | 97.499999  | 123.573225 | 440.00  | 28 |
| 20.00 | 9.4890  | 5.2500 | 3.9200 | 108.044999 | 136.871187 | 455.00  | 29 |
| 5.00  | 9.5000  | 5.2530 | 3.9300 | 108.527235 | 137.898777 | 477.50  | 30 |
| 25.00 | 9.5160  | 5.2570 | 3.9480 | 109.107119 | 139.293953 | 502.50  | 31 |
| 25.00 | 9.5600  | 5.2600 | 3.9500 | 109.563694 | 140.221516 | 527.50  | 32 |
| 25.00 | 9.5760  | 5.2850 | 3.9880 | 111.389723 | 142.919250 | 552.50  | 33 |
| 25.00 | 9.6300  | 5.3130 | 4.0220 | 113.532887 | 145.922029 | 577.50  | 34 |
| 25.00 | 9.6830  | 5.3400 | 4.0560 | 115.659271 | 148.973991 | 602.50  | 35 |
| 25.00 | 9.7360  | 5.3670 | 4.0900 | 117.811175 | 152.064795 | 627.50  | 36 |
| 25.00 | 9.7820  | 5.3950 | 4.1200 | 119.969498 | 154.883288 | 652.50  | 37 |
| 25.00 | 10.0140 | 5.5180 | 4.1650 | 126.817265 | 164.032475 | 677.50  | 38 |
| 25.00 | 10.1800 | 5.6300 | 4.2120 | 133.507339 | 169.484978 | 702.50  | 39 |
| 25.00 | 10.1900 | 5.7460 | 4.2570 | 140.551306 | 160.927654 | 727.50  | 40 |
| 25.00 | 10.3920 | 5.8500 | 4.2570 | 147.156744 | 179.039375 | 752.50  | 41 |
| 25.00 | 10.6770 | 5.9500 | 4.4750 | 158.426184 | 188.290142 | 777.50  | 42 |
| 25.00 | 10.8520 | 6.0440 | 4.6330 | 169.243189 | 207.123043 | 802.50  | 43 |
| 25.00 | 11.0250 | 6.1400 | 4.7970 | 180.844978 | 221.388382 | 827.50  | 44 |
| 25.00 | 11.1800 | 6.2300 | 4.9400 | 191.795720 | 233.991001 | 852.50  | 45 |
| 25.00 | 11.2240 | 6.2500 | 4.9425 | 193.066406 | 235.514317 | 877.50  | 46 |
| 25.00 | 11.2670 | 6.2750 | 4.9450 | 194.712463 | 238.319519 | 902.50  | 47 |
| 25.00 | 11.3100 | 6.2970 | 4.9475 | 196.179302 | 240.506287 | 927.50  | 48 |
| 25.00 | 11.3500 | 6.3220 | 4.9500 | 197.860031 | 241.991287 | 952.50  | 49 |
| 25.00 | 11.3920 | 6.3400 | 4.9517 | 199.636549 | 244.546944 | 977.50  | 50 |
| 25.00 | 11.4340 | 6.3600 | 4.9534 | 200.363043 | 246.863354 | 1002.50 | 51 |
| 25.00 | 11.4760 | 6.3750 | 4.9550 | 201.374296 | 249.817837 | 1027.50 | 52 |
| 25.00 | 11.5180 | 6.3900 | 4.9567 | 202.392466 | 252.792294 | 1052.50 | 53 |
| 25.00 | 11.5600 | 6.4050 | 4.9584 | 203.413521 | 255.781784 | 1077.50 | 54 |
| 25.00 | 11.6000 | 6.4210 | 4.9600 | 204.497028 | 258.423523 | 1102.50 | 55 |

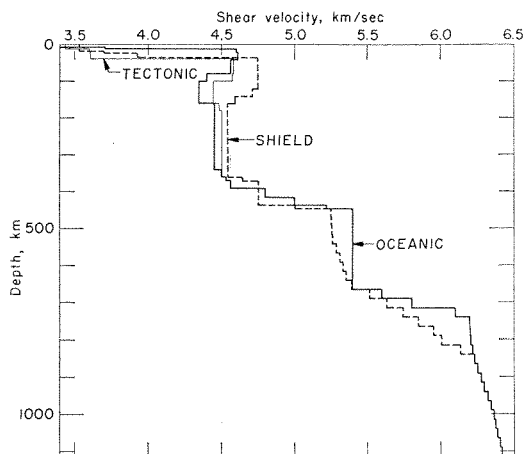


Fig. 1. Shear velocity as a function of depth for oceanic, tectonic, and shield earth models [Anderson and Toksöz, 1966; Anderson 1966].

and from (10)

$$A_L = (\mu_1 d_1)^{-1} \tag{12}$$

since  $C_L \rightarrow U_L \rightarrow \beta_1$  as  $\omega \rightarrow \infty$ . For long periods of the fundamental Love mode,  $I_0^L$  can be expressed in the limit as

$$I_0^L \rightarrow \mu_n^2 / [2\omega^2 d_p \mu_p (\beta_n^2 / \beta_p^2 - 1)] \tag{13}$$

where the subscript 1 designates the surface layer and  $n$  the  $n$ th layer or half-space. The new quantities are defined by

$$\begin{aligned} \mu_p &= \sum_{j=1}^{n-1} \frac{\mu_j d_j}{d_p} \\ \rho_p &= \sum_{j=1}^{n-1} \frac{\rho_j d_j}{d_p} \\ d_p &= \sum_{j=1}^{n-1} d_j \end{aligned} \tag{14}$$

and  $\beta_p^2 = \mu_p / \rho_p$

From (10) we obtain the long-period limit

$$A_L = \omega^2 d_p \mu_p (\beta_n^2 / \beta_p^2 - 1) / (\beta_n \mu_n)^2 \tag{15}$$

using the limits

$$C_L \rightarrow U_L \rightarrow \beta_n \text{ as } \omega \rightarrow 0$$

For Rayleigh waves the high-frequency and long-period asymptotes are

$$I_0^R \rightarrow 2V_{Ri} \rho_i D_i / \omega (1 - V_{Ri}^2 / \alpha_i^2)^{1/2} \tag{16}$$

where

$$\begin{aligned} D_i &= \beta_i^2 \gamma_i^2 (\alpha_i^2 + \beta_i^2 \\ &\quad - 2V_{Ri}^2) / [\alpha_i V_{Ri} (\gamma_i - 1)]^2 - (\gamma_i - 1) \\ \gamma_i &= 2(\beta_i / V_{Ri})^2 \end{aligned}$$

and from (10)

$$A_R \rightarrow \omega (1 - V_{Ri}^2 / \alpha_i^2)^{1/2} / (4\rho_i V_{Ri}^3 D_i) \tag{17}$$

since  $C_R \rightarrow U_R \rightarrow V_{Rj}$  with the subscript  $j = 1$  for  $\omega \rightarrow \infty$  and  $j = n$  for  $\omega \rightarrow 0$ . This short-period expression is only valid for an all solid model; for oceanic models the limit is different and is not given here.

Expressions 12, 15, and 17 are identical with the limits given by Harkrider [1966], which were obtained by taking the short- and long-period limits of the residue evaluation of the solutions for buried sources.

Since the kinetic and potential energy integrals of (1) and (2) are equal for surface waves, we can write the spectral energy densities per unit propagation path as

$$E^R = \int_0^{2\pi} \omega^2 I_0^R | [w_0(r, \theta, h)]_R |^2 r d\theta \tag{18}$$

$$E^L = \int_0^{2\pi} \omega^2 I_0^L | \{ V_0(r, \theta, h) \}_L |^2 r d\theta \tag{19}$$

Evaluating these expressions with the spectral solutions for buried sources in a multilayered medium [Harkrider, 1964; Ben-Menahem and Harkrider, 1964], we obtain at distances large in comparison with the wavelength

$$E_V^R = \omega \langle L \rangle^2 C_R A_R^2 I_0^R [\dot{w}(h) / \dot{w}_0]^2 \tag{20}$$

$$E_V^L \equiv 0 \tag{21}$$

for a vertical source at depth  $h$  and

$$E_H^R = (\omega/2) \langle L \rangle^2 C_R A_R^2 I_0^R [\dot{u}^*(h) / \dot{u}_0]^2 \tag{22}$$

$$E_H^L = (\omega/2) \langle L \rangle^2 C_L A_L^2 I_0^L [\dot{v}(h) / \dot{v}_0]^2 \tag{23}$$

for a horizontal source at the same depth with source strength  $\langle L \rangle$ .

### NUMERICAL RESULTS

The numerical calculations presented in this paper are for two extreme models of the earth's mantle structure. The oceanic and shield models are given in Table 1 and Figure 1. These structures were derived by applying the universal

TABLE 2. Normalized Rayleigh and Love energy integrals in units of  $10^5$  ergs/cm<sup>2</sup> for the ocean structure.

| RAYLEIGH |             |          |             |          |             |        |        |
|----------|-------------|----------|-------------|----------|-------------|--------|--------|
| MODE 1,1 |             | MODE 2,1 |             | MODE 1,2 |             |        |        |
| PERIOD   | ENERGY      | PERIOD   | ENERGY      | PERIOD   | ENERGY      | PERIOD | ENERGY |
| 350.     | 0.83660E 00 | 250.     | 0.16325E 02 | 110.     | 0.14421E 03 |        |        |
| 300.     | 0.81804E 00 | 225.     | 0.66546E 01 | 100.     | 0.49520E 02 |        |        |
| 250.     | 0.88346E 00 | 200.     | 0.69574E 01 | 90.      | 0.32500E 02 |        |        |
| 225.     | 0.96339E 00 | 175.     | 0.83638E 01 | 80.      | 0.22437E 02 |        |        |
| 200.     | 0.10855E 01 | 150.     | 0.10222E 02 | 70.      | 0.25950E 02 |        |        |
| 175.     | 0.12652E 01 | 140.     | 0.11232E 02 | 65.      | 0.33387E 02 |        |        |
| 150.     | 0.15293E 01 | 130.     | 0.12567E 02 | 60.      | 0.45168E 02 |        |        |
| 140.     | 0.16682E 01 | 120.     | 0.14339E 02 | 55.      | 0.60541E 02 |        |        |
| 130.     | 0.18320E 01 | 110.     | 0.16654E 02 | 50.      | 0.75620E 02 |        |        |
| 120.     | 0.20270E 01 | 100.     | 0.19313E 02 | 45.      | 0.85394E 02 |        |        |
| 110.     | 0.22610E 01 | 90.      | 0.21936E 02 | 40.      | 0.92823E 02 |        |        |
| 100.     | 0.25430E 01 | 80.      | 0.24208E 02 | 35.      | 0.11113E 03 |        |        |
| 90.      | 0.28900E 01 | 70.      | 0.27114E 02 | 30.      | 0.15659E 03 |        |        |
| 80.      | 0.33220E 01 | 65.      | 0.29716E 02 | 25.      | 0.26977E 03 |        |        |
| 70.      | 0.38762E 01 | 60.      | 0.34653E 02 | 20.      | 0.66291E 03 |        |        |
| 65.      | 0.42159E 01 | 55.      | 0.42459E 02 | 15.      | 0.34680E 04 |        |        |
| 60.      | 0.46101E 01 | 50.      | 0.55076E 02 | 10.      | 0.12420E 06 |        |        |
| 55.      | 0.50715E 01 | 45.      | 0.75520E 02 |          |             |        |        |
| 50.      | 0.56159E 01 | 40.      | 0.10937E 03 |          |             |        |        |
| 45.      | 0.62220E 01 | 35.      | 0.16760E 03 |          |             |        |        |
| 40.      | 0.70303E 01 | 30.      | 0.27535E 03 |          |             |        |        |
| 35.      | 0.79392E 01 | 25.      | 0.48540E 03 |          |             |        |        |
| 30.      | 0.89970E 01 | 20.      | 0.10092E 04 |          |             |        |        |
| 25.      | 0.10176E 02 | 15.      | 0.34319E 04 |          |             |        |        |
| 20.      | 0.11292E 02 | 10.      | 0.49341E 05 |          |             |        |        |
| 15.      | 0.12641E 02 |          |             |          |             |        |        |
| 10.      | 0.37182E 02 |          |             |          |             |        |        |

| LOVE   |             |        |             |        |             |        |             |
|--------|-------------|--------|-------------|--------|-------------|--------|-------------|
| MODE 0 |             | MODE 1 |             | MODE 2 |             | MODE 3 |             |
| PERIOD | ENERGY      | PERIOD | ENERGY      | PERIOD | ENERGY      | PERIOD | ENERGY      |
| 350.   | 0.46970E 00 | 200.   | 0.17491E 02 | 100.   | 0.42066E 02 | 65.    | 0.3565E 02  |
| 300.   | 0.56053E 00 | 175.   | 0.49721E 01 | 90.    | 0.13147E 02 | 60.    | 0.23841E 02 |
| 250.   | 0.71589E 00 | 150.   | 0.42305E 01 | 80.    | 0.12220E 02 | 55.    | 0.23117E 02 |
| 225.   | 0.83493E 00 | 140.   | 0.42787E 01 | 70.    | 0.14460E 02 | 50.    | 0.27401E 02 |
| 200.   | 0.99260E 00 | 130.   | 0.44409E 01 | 65.    | 0.15934E 02 | 45.    | 0.35680E 02 |
| 175.   | 0.12362E 01 | 120.   | 0.46938E 01 | 60.    | 0.17069E 02 | 40.    | 0.41048E 02 |
| 150.   | 0.15944E 01 | 110.   | 0.50199E 01 | 55.    | 0.17456E 02 | 35.    | 0.35297E 02 |
| 140.   | 0.17918E 01 | 100.   | 0.54117E 01 | 50.    | 0.17236E 02 | 30.    | 0.33503E 02 |
| 130.   | 0.20350E 01 | 90.    | 0.58904E 01 | 45.    | 0.17241E 02 | 25.    | 0.39507E 02 |
| 120.   | 0.23395E 01 | 80.    | 0.65398E 01 | 40.    | 0.18159E 02 | 20.    | 0.52621E 02 |
| 110.   | 0.27288E 01 | 70.    | 0.75425E 01 | 35.    | 0.20012E 02 | 15.    | 0.92548E 02 |
| 100.   | 0.32387E 01 | 65.    | 0.82664E 01 | 30.    | 0.22536E 02 | 10.    | 0.10480E 04 |
| 90.    | 0.39260E 01 | 60.    | 0.92062E 01 | 25.    | 0.25166E 02 |        |             |
| 80.    | 0.48667E 01 | 55.    | 0.10432E 02 | 20.    | 0.26649E 02 |        |             |
| 70.    | 0.62922E 01 | 50.    | 0.1203E 02  | 15.    | 0.27114E 02 |        |             |
| 65.    | 0.72535E 01 | 45.    | 0.14372E 02 | 10.    | 0.29341E 04 |        |             |
| 60.    | 0.84760E 01 | 40.    | 0.17039E 02 |        |             |        |             |
| 55.    | 0.10058E 02 | 35.    | 0.20976E 02 |        |             |        |             |
| 50.    | 0.12161E 02 | 30.    | 0.26519E 02 |        |             |        |             |
| 45.    | 0.15050E 02 | 25.    | 0.34478E 02 |        |             |        |             |
| 40.    | 0.19177E 02 | 20.    | 0.45036E 02 |        |             |        |             |
| 35.    | 0.25378E 02 | 15.    | 0.41085E 02 |        |             |        |             |
| 30.    | 0.35308E 02 | 10.    | 0.96181E 02 |        |             |        |             |
| 25.    | 0.52538E 02 |        |             |        |             |        |             |
| 20.    | 0.85064E 02 |        |             |        |             |        |             |
| 15.    | 0.14116E 03 |        |             |        |             |        |             |
| 10.    | 0.11985E 02 |        |             |        |             |        |             |

dispersion theory of Anderson [1964] to the great-circle data of Toksöz and Anderson [1966]. Approximately 53 layers are used in each case to define the mantle structure.

For each model we provide in tables and/or figures the basic quantities necessary for calculating the surface wave energies for the first three Rayleigh and the first four Love modes.

The effect of source depth is presented for the oceanic model, but tables for including the source depth can be found in Harkrider [1966] for a much wider range of depths for both models.

It is advisable at this point to mention some of the basic differences between the two structural models. The most pronounced difference

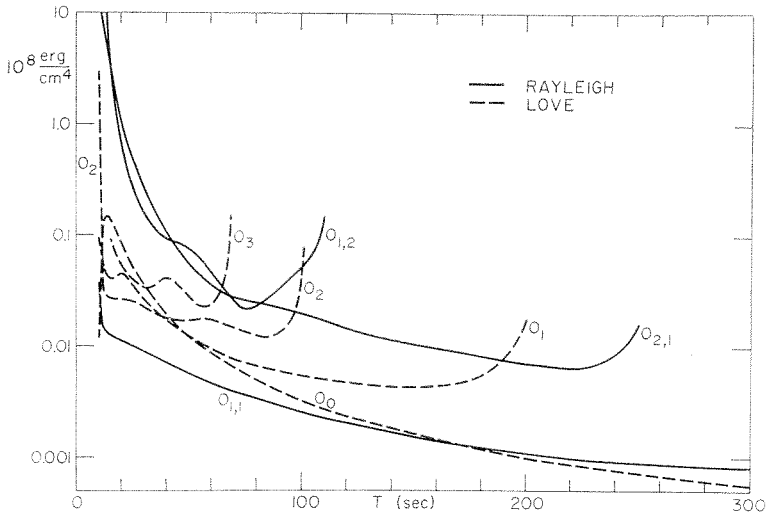


Fig. 2. Normalized Love and Rayleigh energy density integrals for the oceanic structure.

(Figure 1) occurs in the mantle low-velocity zone between 100 and 400 km. The oceanic model has a shallower and more pronounced low-velocity zone in addition to a thinner crustal wave guide. Thus, if any differences between models occur in the numerical results, we would expect them to be most apparent in the trapped modes, i.e., Love waves and the higher-mode Rayleigh waves. These are waves whose very existence depends on the presence of wave guides either at the surface or at depth, and they are thus more sensitive to the details of wave guides than the fundamental Rayleigh wave. The two pronounced upper mantle discontinuities at depths near 400 and 700 km are important features of recent conclusions regarding surface wave dispersion.

For the oceanic model, the sum of the normalized kinetic and potential energy density integrals are given in Table 2 and Figure 2. Since these two integrals are equal, the curves represent  $2T^k$  and  $2T^p$ , given in (1) and (2). The same quantities are given for the shield model in Table 3 and Figure 3. From the limits (16) we see that the energy density integral for fundamental Rayleigh waves is inversely proportional to period at both the long and short periods. For the fundamental Love wave, the limits (11 and 13) require that the energy density integral approach a constant value at long periods and be inversely proportional to the square of the period at short periods.

From the figures we see that the long-period asymptotic behavior of the energy integrals is beyond the range of the tabulated results. In fact, on the basis of the figures alone, we might suspect that the quoted long-period trends of Love and Rayleigh waves had been interchanged. To verify the limits, we calculated the energy for very long periods, and the results agree with the theory.

At short periods the asymptotic trends of the Rayleigh and Love fundamental modes for the shield model can be seen in Figure 3. The relatively complicated behavior (Figure 2) at short periods is associated with the surface, crustal, and upper mantle wave guides. Complications occur at shorter periods for the oceanic model because of the thinner crust and shallower low-velocity zone.

As suggested earlier, the contrast between models is greatest in the trapped modes, especially the Love modes. Very little difference in the normalized energy densities of the fundamental Rayleigh waves occurs over the range of calculated periods.

Energy curves obtained by numerical integration can be found for additional earth models in *Wu* [1966].

To calculate the actual variation of energy with frequency and mode, we must operate on the normalized energies with the spectrum of surface displacements obtained from a given source.

TABLE 3. Normalized Rayleigh and Love energy integrals in units of  $10^5$  ergs/cm<sup>2</sup> for the shield structure.

| RAYLEIGH |             |          |             |          |             |
|----------|-------------|----------|-------------|----------|-------------|
| MODE 1,1 |             | MODE 2,1 |             | MODE 1,2 |             |
| PERIOD   | ENERGY      | PERIOD   | ENERGY      | PERIOD   | ENERGY      |
| 350.     | 0.8251E 00  | 250.     | 0.10227E 02 | 110.     | 0.92987E 02 |
| 300.     | 0.84075E 00 | 225.     | 0.76901E 01 | 100.     | 0.49643E 02 |
| 250.     | 0.95077E 00 | 200.     | 0.87048E 01 | 90.      | 0.39277E 02 |
| 225.     | 0.10551E 01 | 175.     | 0.10385E 02 | 80.      | 0.29952E 02 |
| 200.     | 0.12047E 01 | 150.     | 0.12264E 02 | 70.      | 0.30036E 02 |
| 175.     | 0.14179E 01 | 140.     | 0.13251E 02 | 65.      | 0.35445E 02 |
| 150.     | 0.17265E 01 | 130.     | 0.14631E 02 | 60.      | 0.45002E 02 |
| 140.     | 0.18881E 01 | 120.     | 0.16466E 02 | 55.      | 0.59229E 02 |
| 130.     | 0.20745E 01 | 110.     | 0.19500E 02 | 50.      | 0.77096E 02 |
| 120.     | 0.23041E 01 | 100.     | 0.23265E 02 | 45.      | 0.94808E 02 |
| 110.     | 0.25733E 01 | 90.      | 0.27776E 02 | 40.      | 0.10864E 03 |
| 100.     | 0.29562E 01 | 80.      | 0.32732E 02 | 35.      | 0.12475E 03 |
| 90.      | 0.32859E 01 | 70.      | 0.38627E 02 | 30.      | 0.16470E 03 |
| 80.      | 0.37588E 01 | 65.      | 0.42406E 02 | 25.      | 0.27525E 03 |
| 70.      | 0.43286E 01 | 60.      | 0.48223E 02 | 20.      | 0.62521E 03 |
| 65.      | 0.46578E 03 | 55.      | 0.57510E 02 | 15.      | 0.20244E 04 |
| 60.      | 0.50181E 01 | 50.      | 0.73056E 02 | 10.      | 0.59904E 05 |
| 55.      | 0.54102E 01 | 45.      | 0.10031E 03 |          |             |
| 50.      | 0.58320E 01 | 40.      | 0.15168E 03 |          |             |
| 45.      | 0.62715E 01 | 35.      | 0.26502E 03 |          |             |
| 40.      | 0.67344E 01 | 30.      | 0.53339E 03 |          |             |
| 35.      | 0.71799E 01 | 25.      | 0.14271E 04 |          |             |
| 30.      | 0.75815E 01 | 20.      | 0.57889E 04 |          |             |
| 25.      | 0.84450E 01 | 15.      | 0.41642E 05 |          |             |
| 20.      | 0.84183E 01 | 10.      | 0.76074E 02 |          |             |
| 15.      | 0.98794E 01 |          |             |          |             |
| 10.      | 0.14450E 02 |          |             |          |             |

| LOVE   |             |        |             |        |             |        |             |
|--------|-------------|--------|-------------|--------|-------------|--------|-------------|
| MODE 0 |             | MODE 1 |             | MODE 2 |             | MODE 3 |             |
| PERIOD | ENERGY      | PERIOD | ENERGY      | PERIOD | ENERGY      | PERIOD | ENERGY      |
| 350.   | 0.50423E 00 | 200.   | 0.91849E 01 | 100.   | 0.18666E 02 | 70.    | 0.68627E 02 |
| 300.   | 0.60347E 00 | 175.   | 0.44218E 01 | 90.    | 0.11096E 02 | 65.    | 0.24230E 02 |
| 250.   | 0.76636E 00 | 150.   | 0.40184E 01 | 80.    | 0.10993E 02 | 60.    | 0.21196E 02 |
| 225.   | 0.88682E 00 | 140.   | 0.41098E 01 | 70.    | 0.13121E 02 | 55.    | 0.21948E 02 |
| 200.   | 0.10479E 01 | 130.   | 0.42951E 01 | 65.    | 0.14771E 02 | 50.    | 0.25579E 02 |
| 175.   | 0.12688E 01 | 120.   | 0.45574E 01 | 60.    | 0.16608E 02 | 45.    | 0.32761E 02 |
| 150.   | 0.15899E 01 | 110.   | 0.49806E 01 | 55.    | 0.18410E 02 | 40.    | 0.42492E 02 |
| 140.   | 0.17420E 01 | 100.   | 0.52507E 01 | 50.    | 0.20192E 02 | 35.    | 0.49513E 02 |
| 130.   | 0.19304E 01 | 90.    | 0.56674E 01 | 45.    | 0.22752E 02 | 30.    | 0.58877E 02 |
| 120.   | 0.21513E 01 | 80.    | 0.61762E 01 | 40.    | 0.28264E 02 | 25.    | 0.92299E 02 |
| 110.   | 0.25166E 01 | 70.    | 0.69340E 01 | 35.    | 0.41724E 02 | 20.    | 0.19191E 03 |
| 100.   | 0.27134E 01 | 65.    | 0.75198E 01 | 30.    | 0.78427E 02 | 15.    | 0.49828E 03 |
| 90.    | 0.30613E 01 | 60.    | 0.83746E 01 | 25.    | 0.20224E 03 | 10.    | 0.33544E 02 |
| 80.    | 0.34450E 01 | 55.    | 0.97237E 01 | 20.    | 0.79618E 03 |        |             |
| 70.    | 0.38260E 01 | 50.    | 0.12099E 02 | 15.    | 0.57286E 04 |        |             |
| 65.    | 0.39884E 01 | 45.    | 0.16761E 02 | 10.    | 0.37570E 04 |        |             |
| 60.    | 0.41073E 01 | 40.    | 0.28948E 02 |        |             |        |             |
| 55.    | 0.41997E 01 | 35.    | 0.65257E 02 |        |             |        |             |
| 50.    | 0.41301E 01 | 30.    | 0.20271E 03 |        |             |        |             |
| 45.    | 0.40342E 01 | 25.    | 0.88935E 03 |        |             |        |             |
| 40.    | 0.39429E 01 | 20.    | 0.59845E 04 |        |             |        |             |
| 35.    | 0.39808E 01 | 15.    | 0.71766E 05 |        |             |        |             |
| 30.    | 0.42414E 01 | 10.    | 0.34283E 06 |        |             |        |             |
| 25.    | 0.48462E 01 |        |             |        |             |        |             |
| 20.    | 0.60703E 01 |        |             |        |             |        |             |
| 15.    | 0.87437E 01 |        |             |        |             |        |             |
| 10.    | 0.15755E 02 |        |             |        |             |        |             |

To facilitate computation and comparison, we adopt as a standard spectrum that due to a surface point source. The spectral density of surface displacement due to a surface source is referred to as relative excitation in this paper. The relative excitations for Rayleigh and Love waves for the oceanic and shield models are given in Figures 4 and 5.

As with the normalized energy integrals, there

is little difference between the two models in the relative excitation of fundamental Rayleigh waves from 300 to 20 seconds. The major differences occur in the trapped modes, especially the Love waves. The shift in amplitude toward the high frequencies in the oceanic relative to the shield model is presumably due to the thinner oceanic wave guide with the maximums for Love waves shifted approximately from 50



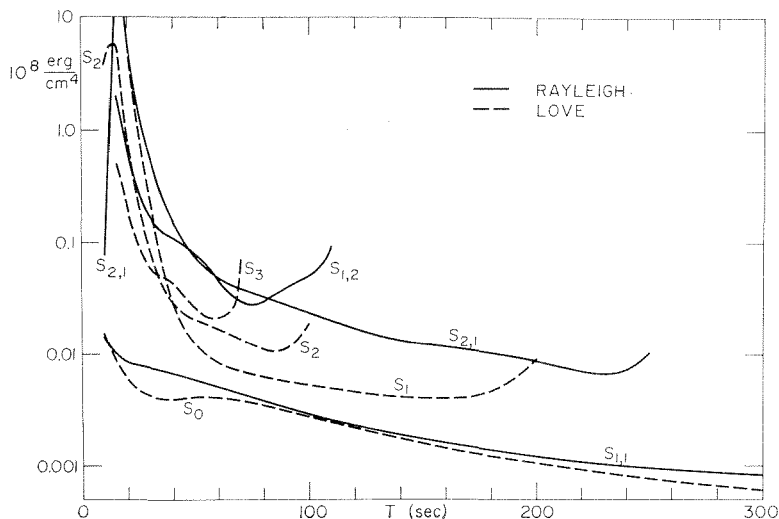


Fig. 3. Normalized Love and Rayleigh energy density integrals for the shield structure.

to 20 seconds. Note the increasing importance of the higher modes relative to the fundamental mode at intermediate periods.

Physically, these curves are the response of the medium to a surface source. Thus we would expect the amplitude of the trapped modes to become much smaller than the fundamental Rayleigh mode at low and high frequencies. This is reasonable because, at these limits, we are approaching half-space conditions for which Love waves and higher modes do not exist.

In Figure 6 we show the Rayleigh and Love wave energy densities per unit propagation path for surface sources at different orientations for oceanic and shield structures. In the figures, the single-subscripted dashed curves are Love modes, and the double-subscripted solid curves refer to Rayleigh modes. A vertical source, of course, does not generate Love waves.

In all cases the energy of the higher-mode Rayleigh waves is at least an order of magnitude less than that contained in the fundamental Rayleigh mode. This is in direct contrast to the normalized energies (Figures 2 and 3) where the opposite was true. Also, the energy in higher modes drops at both the long and short periods and, in all modes, at the long periods. The energies contained in the fundamental Love and Rayleigh modes are roughly comparable for a horizontal surface source, and the higher Love modes are much more energetic than the corresponding Rayleigh modes.

The importance of the short-period surface waves in any estimate of total surface wave energy is obvious from these figures. From (20), (22), and (23) we see that at long periods the fundamental Rayleigh mode is of the order of  $\omega^2$  and the fundamental Love mode is of the order  $\omega^3$ . The greater energy in the trapped modes of the oceanic model relative to the shield model for a surface source reflects the relative nearness to the surface of the oceanic wave guides. As noted earlier for other spectral quantities, the energies for the fundamental Rayleigh mode are remarkably similar for the two models.

For a horizontal surface force, the energy density of the fundamental Rayleigh mode decreases by a factor of about 4. This can be seen quantitatively by comparing (20) with (22), since the square of surface ellipticity for fundamental Rayleigh waves is about 0.5 for a wide range of periods.

An assumption of equipartition of energy density between all surface wave modes is obviously not valid even for estimation purposes. On the other hand, there is to some degree an equipartition of energy density between the fundamental Rayleigh and fundamental Love modes for a horizontal surface source. This is true for both models. Also, as noted above, the higher Love modes contain more energy than the higher Rayleigh modes.

For certain frequencies the energy densities

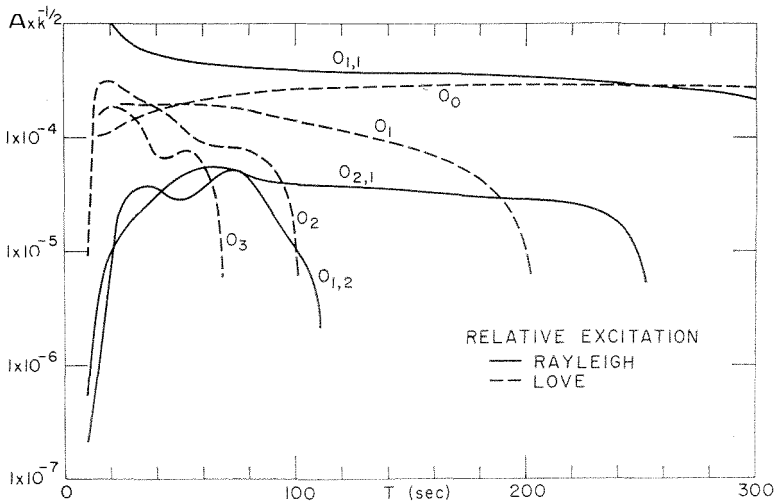


Fig. 4. Relative spectral excitation for the oceanic structure in units of  $10^{-12.5}$  cm<sup>3/2</sup>/dyne.

of higher-mode Rayleigh waves are approximately equal, and similarly for the higher-mode Love waves. Thus, in these frequency bands, a rough equipartition of energy density is obtained for the higher modes of Rayleigh and Love waves. For the oceanic model the equipartition includes the fundamental Love wave with its higher modes.

The effect of source depth on the first three Rayleigh modes for a vertical force in an oceanic model is illustrated in Figure 7. The figure at the top left is for the surface source given in Figure 6 and is used as a reference. At the top

right we show the spectral energy density per unit propagation path for the fundamental mode for a surface focus and for three other source depths.

In general, increasing the depth decreases the amount of energy in the fundamental mode. However, a focus at 50 km, which is the top of the low-velocity zone, can generate Rayleigh waves with slightly more energy for certain frequencies than a surface source. The higher modes all have critical depths at which they are excited most efficiently and also periods at which they are not excited at all. For a given

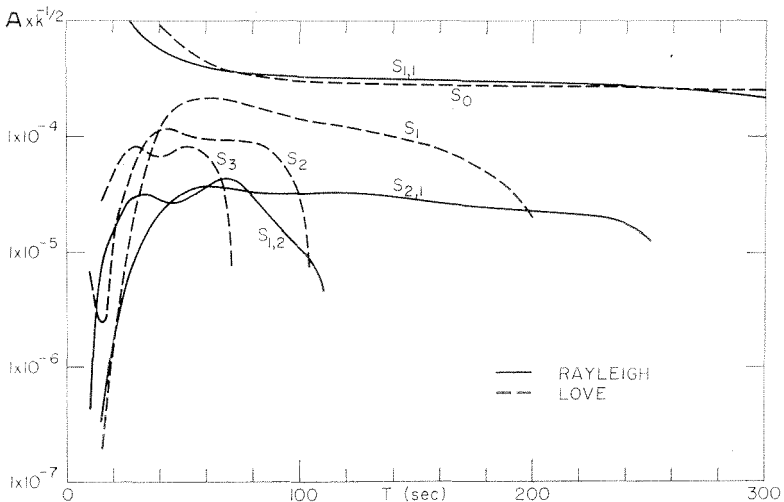


Fig. 5. Relative spectral excitation for the shield structure in units of  $10^{-12.5}$  cm<sup>3/2</sup>/dyne.

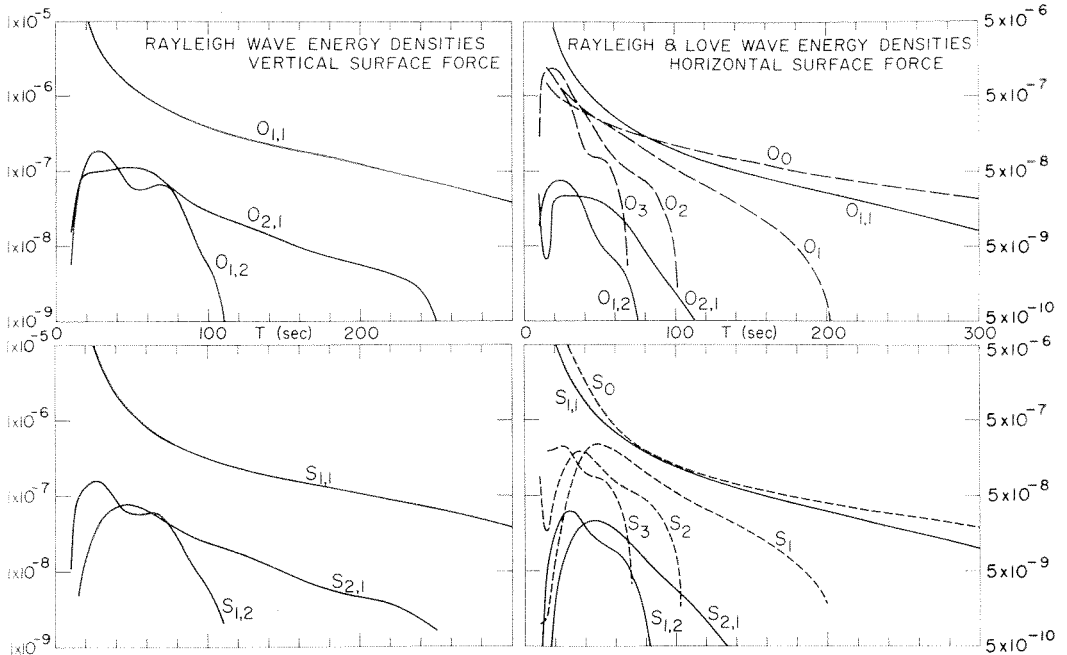


Fig. 6. Spectral energy densities per unit propagation path in units of  $10^{15}$  ergs/km for a surface force of strength  $\langle L \rangle = 10^{15}$  dynes sec.

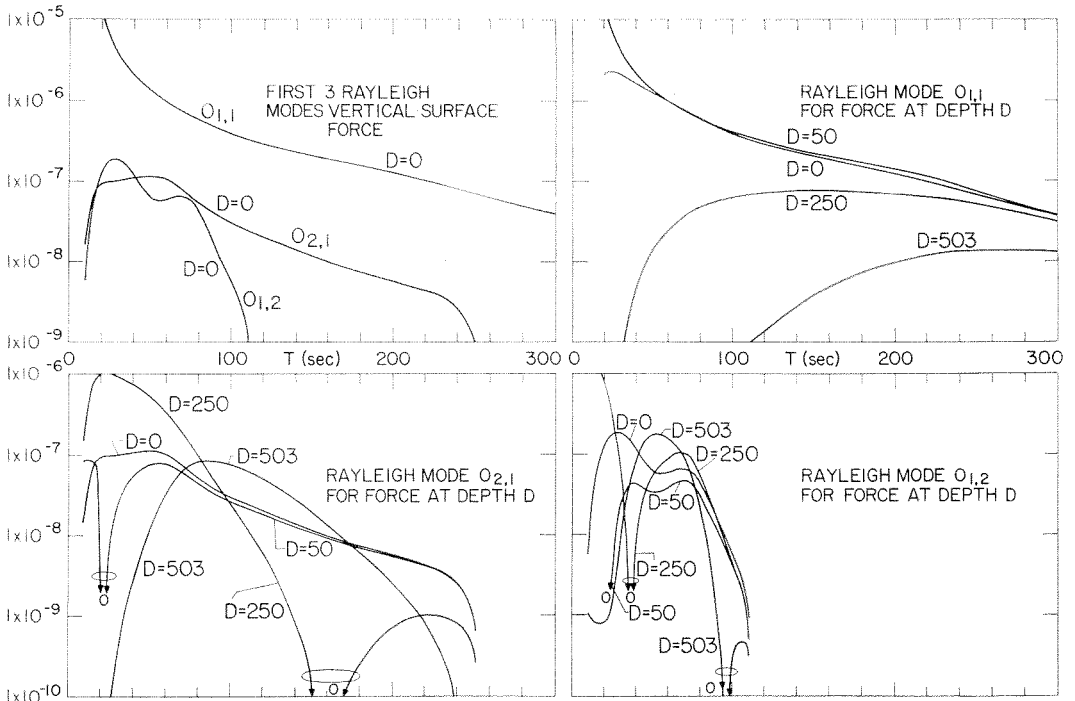


Fig. 7. Rayleigh wave spectrum energy densities per unit oceanic propagation path in units of  $10^{15}$  ergs/km for buried vertical forces of strength  $\langle L \rangle = 10^{15}$  dynes sec.

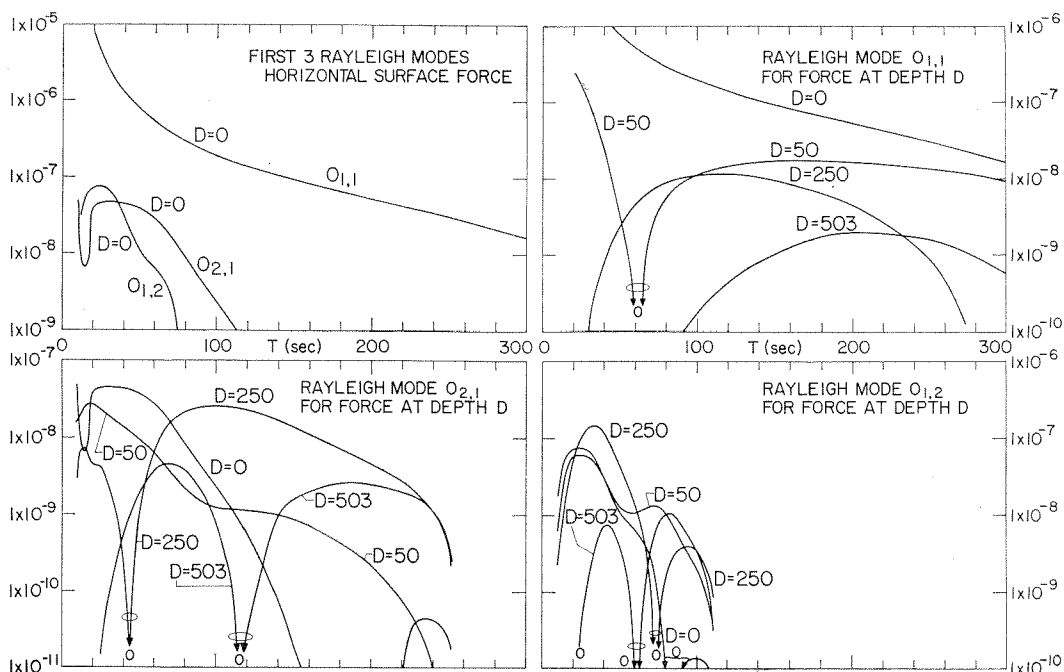


Fig. 8. Rayleigh wave spectrum energy densities per unit oceanic propagation path in units of  $10^{15}$  ergs/km for buried horizontal forces of strength  $\langle L \rangle = 2 \times 10^{15}$  dynes sec.

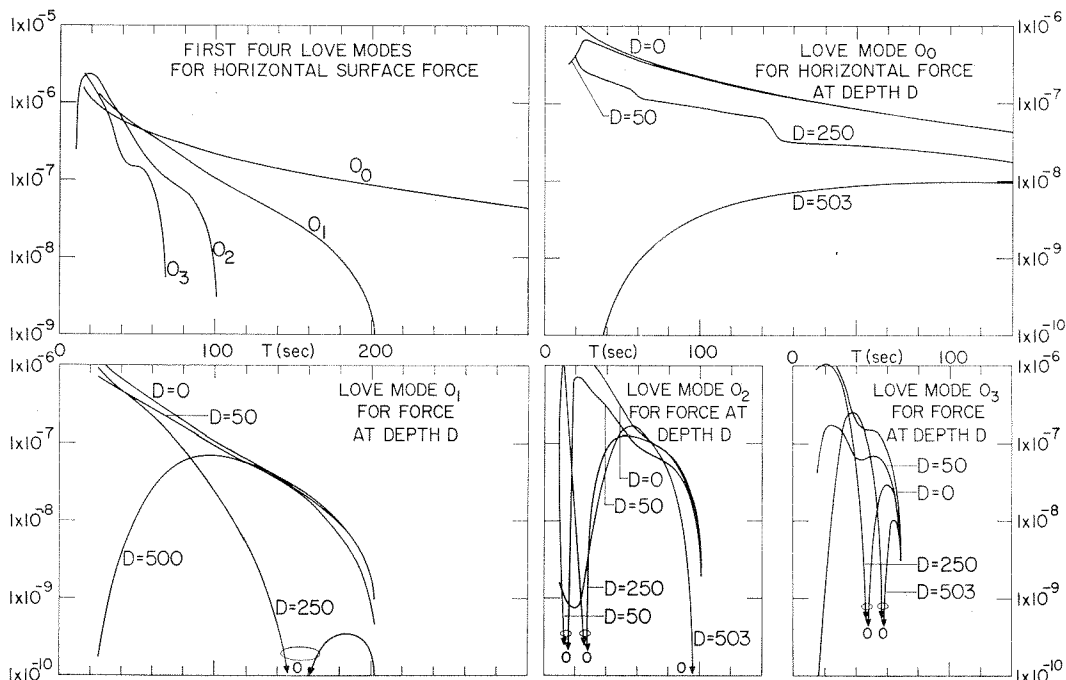


Fig. 9. Love wave spectrum energy densities per unit oceanic propagation path in units of  $10^{15}$  ergs/km for buried horizontal forces of strength  $\langle L \rangle = 2 \times 10^{15}$  dynes sec.

source orientation these zeros are diagnostic of source depth. Note the shift of the zeros with frequency for increasing source depth. The successively deeper sources have zeros at successively longer periods. A source at 250 km, which is in the low-velocity channel, is a very efficient generator of higher-mode waves.

Figure 8 shows the Rayleigh wave energy densities for horizontal forces at various depths. The important difference, for vertical and horizontal forces, is the shift in the location of the energy zeros. The zero locations for the two forces are governed by the nodes of horizontal displacements for horizontal forces and the nodes of the vertical displacements for vertical forces. The most efficient level for the generation of the fundamental mode for periods greater than 20 seconds is at the surface. A source in the channel generates less higher-mode energy than sources at other depths only for periods which involve a vertical displacement node in the channel. This again illustrates the channel wave characteristic of higher modes.

Even though a source in the channel is especially efficient in the generation of higher modes, it should be emphasized that this does not necessarily mean high surface amplitudes. Most of the energy is in the channel. On the other hand, small surface amplitudes of the higher modes do not mean low total energies. One cannot neglect the energy content of higher modes simply because they have low surface amplitudes.

The corresponding Love wave energy densities are displayed in Figure 9. As before, the holes in the energy spectrum of the higher modes are diagnostic of source depth.

#### CONCLUSIONS

The tables given in this paper make it possible to convert an observed surface wave amplitude at a given period to the total energy in the wave at that period, or to convert an observed amplitude spectrum over a certain frequency band to the total energy contained in that band. The figures given here and the tables in *Harkrider* [1966] make it possible to estimate the partitioning of energy among the various surface wave modes. The use of spectrums and nodal spectral ratios to recover source depth and orientation is discussed further in *Harkrider* [1966].

To estimate the energy in a frequency band

from a seismic source, the data from several stations are needed to define the radiation pattern and source characteristics, which in turn are required for the surface integration. The experimental frequency band should be as wide as possible and, in particular, should include as much information as possible from the short-period arrivals. The curves presented here in conjunction with the asymptotic limits can be used in estimating the energy outside the measured band. The energy content of modes not directly analyzed can also be estimated if enough properties of the source are known. The experimental amplitude spectrums should, of course, be corrected for propagation effects such as spreading and attenuation.

*Acknowledgment.* This research was supported by the Advanced Research Projects Agency and was monitored by the Air Force Office of Scientific Research under contract AF-49(638)-1337.

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(Manuscript received January 17, 1966.)