

EFFECT OF DISTANCE ON LOCAL MAGNITUDES FOUND FROM STRONG-MOTION RECORDS

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ABSTRACT

Values of local magnitude M_L , are calculated from 56 strong-motion accelerograms recorded in the Imperial Valley earthquake of 15 October 1979 according to procedures developed earlier (Kanamori and Jennings, 1978). These data, plus similar data from the San Fernando earthquake of 9 February 1971 and additional, less numerous data from several other California earthquakes, are used to investigate the use of different measures of distance in near-field determinations of M_L : this investigation has relevance for similar uses of distances in determining seismic design criteria. In addition, the consistency of the values of M_L found from the strong-motion data is examined from the viewpoint of assessing the need for any correction in the standard attenuation curve, $-\log_{10}A_0(\Delta)$.

It was found that the most consistent values of M_L result when distance is measured to the closest point on the surface trace of the fault if a site lies within a circle with diameter equal to the extent of faulting and centered on the center of faulting (center of energy release). Outside this circle, the distance measured to the center of the circle is recommended.

A consistent trend in the values of M_L found from strong-motion records is seen in the data. The values start, at zero distance, at essentially the far-field value and then decrease to $-1/4$ unit at about 20 km. Then they rise to $+1/4$ unit at 50 to 60 km. A smooth revision to the standard attenuation curve is presented which removes this systematic trend.

INTRODUCTION

The local magnitude, M_L , was initially introduced by Richter (1935) as a relative measure of earthquakes in southern California. As originally defined, M_L is determined from the amplitude of motion recorded by the standard Wood-Anderson seismograph, which has a period of 0.8 sec, a damping constant of 80 per cent of critical, and a magnification of 2800. The period and damping of the Wood-Anderson instrument are such as to make it sensitive to ground motion in the period range of greatest engineering interest (typically 0.2 to 3 sec). This feature, plus the fact that M_L is determined from ground motions closer to the source than is the case for other magnitudes, means that M_L is of particular interest for most engineering applications, including the determination of seismic design criteria for major projects.

Kanamori and Jennings (1978), Jennings and Kanamori (1979), Espinosa (1980), and Boore (1980) have used strong-motion accelerograms obtained at short epicentral distances to determine the local magnitude. Whether seismograms from the Wood-Anderson instruments are used directly, or if synthetic Wood-Anderson seismograms are used as in Kanamori and Jennings (1978), the basis of the calculation of M_L from the maximum Wood-Anderson response is the amplitude attenuation curve (as a function of distance) constructed by Richter (1935) for a reference event. However, Richter's (1935) curve is given only for $\Delta \geq 25$ km. At distances $\Delta \leq 25$ km, the standard Wood-Anderson seismographs go off scale for events with $M_L \geq 4.5$; no reliable amplitude measurements can be made on this instrument at

$\Delta \leq 25$ km for events large enough to have much engineering significance. This is one of the reasons for using the accelerograph data in the studies mentioned above. Later, Gutenberg and Richter (1942) extended the attenuation curve to the distance range $0 \leq \Delta \leq 30$ km; however, the data for this range were obtained by $4\times$ torsion

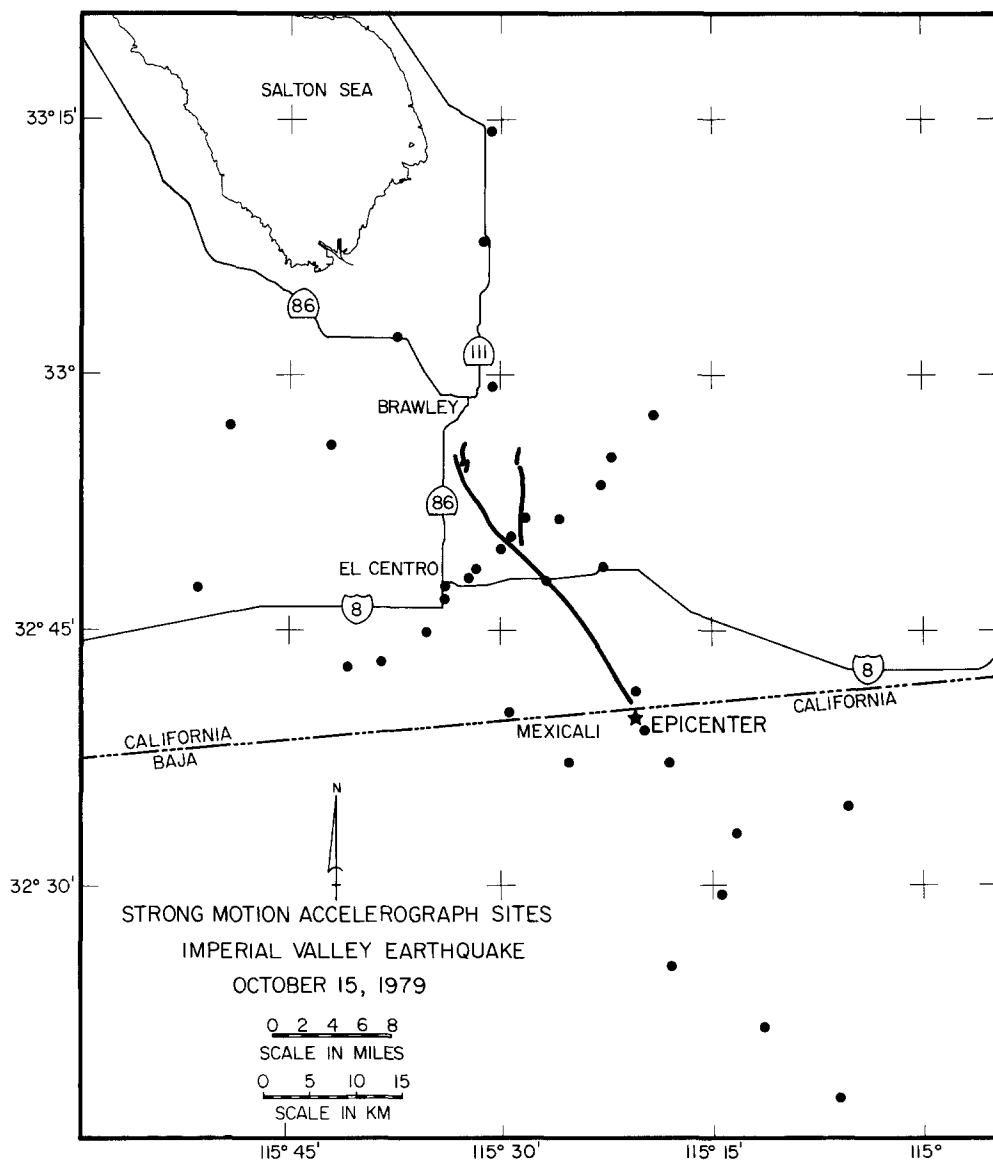


FIG. 1. Location of strong-motion accelerographs recording the Imperial Valley earthquake of 15 October 1979. A few more distant accelerographs triggered, but their records were very small and were not used in this study. The heavy line indicates the surface faulting.

seismometers whose response is different from the standard Wood-Anderson seismograph (the period is 10 sec and the damping near critical). Thus, the determination of M_L at short distances, particularly at $\Delta \leq 25$ km, requires some caution.

The extended attenuation curve is that which is tabulated in Richter (1958) and was used by us in our earlier studies [Kanamori and Jennings (1978); Jennings and Kanamori (1979)].

Another related problem concerns the measure of distance. The fact that the strength of shaking typically reduces with distance is of great importance in the determination of earthquake-resistant design criteria. In practice, the measure of distance used is not too significant if the site is relatively far away from the potential earthquake source; however, the definition of distance becomes important when the distance from the site to the fault is comparable to the postulated length of faulting or depth of focus. It is in the near-field, of course, where seismic design criteria are the most stringent and expensive to implement. For sites in the near-field, different

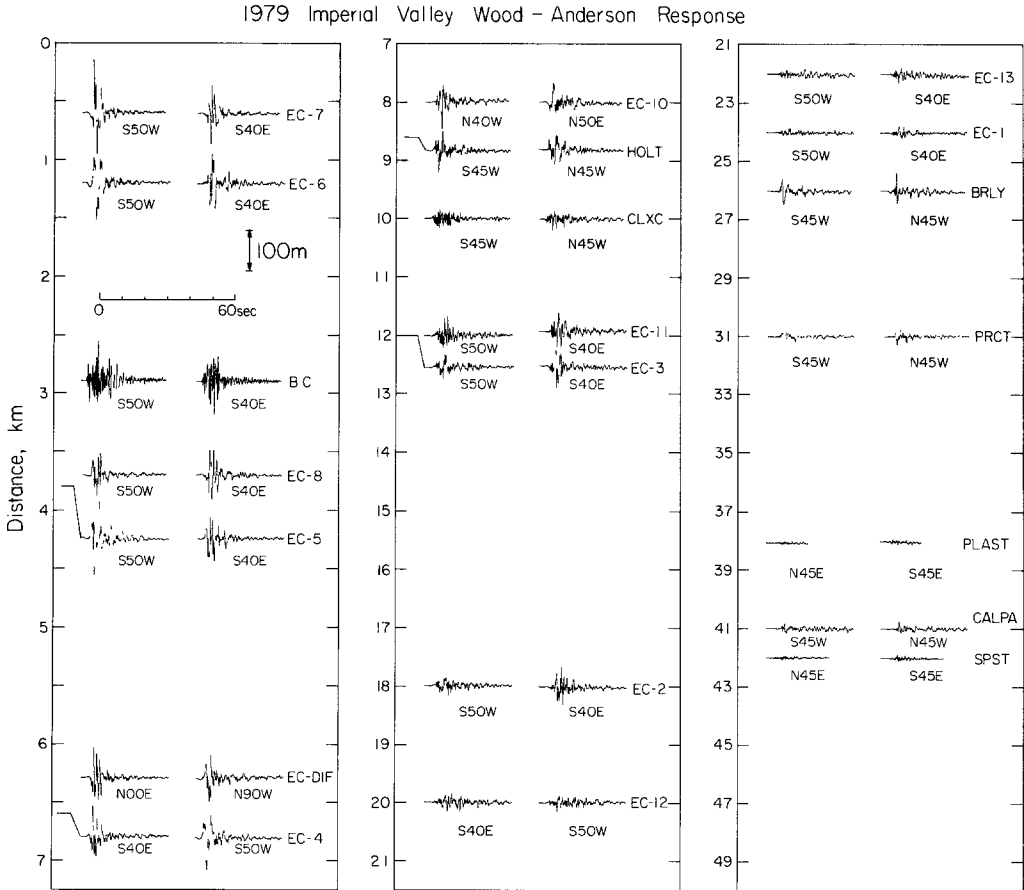


FIG. 2. Synthetic Wood-Anderson seismograms calculated from accelerograms from the Imperial Valley earthquake of 15 October 1979. The distance is from the fault, as discussed in the text. All seismograms are plotted to the time and amplitude scales shown in the *upper left corner* of the figure.

measures of distances can result in significantly different estimates of the expected strength of ground shaking, and there exists some controversy over the most appropriate measure. The studies of attenuation of ground motion with distance which are used to make estimates of strong ground motion for design implicitly assume that the magnitude computed for a given earthquake is the same regardless of the distance, aside from random statistical fluctuations. In particular, if local magnitude is used, the assumption is made that records from Wood-Anderson seismographs, when used with the selected measure of distance and the standard attenuation curve for M_L , give a value of M_L that is independent of distance, even

in the near-field. Again, random statistical fluctuations about a mean value are inevitable, but systematic trends with distance are assumed to be absent.

In order to investigate both the amplitude attenuation curve at short distances and the best measure of distance to be used for the study of the attenuation of strong ground motion, we analyzed an extensive set of strong-motion records

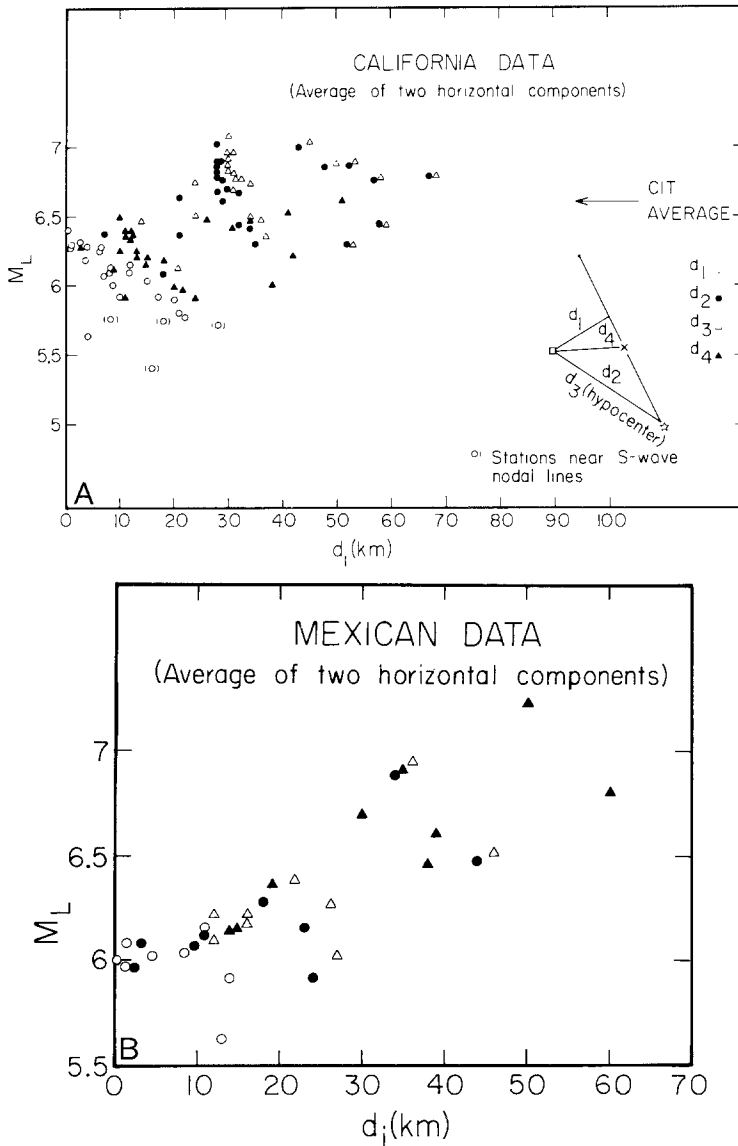


FIG. 3. Values of M_L for the Imperial Valley earthquake of 15 October 1979. Four measures of distance are used: d_1 , closest distance to the fault; d_2 , epicentral distance; d_3 , hypocentral distance; and d_4 , distance to center of faulting. (a) California data. (b) Mexican data. Data in parentheses are near-nodal lines for SH motion.

obtained for the Imperial Valley earthquake of 15 October 1979. For this earthquake, the accelerograph sites are particularly well located to study these two problems. In addition, we have supplemented this data set with those from the 1971 San Fernando earthquake and several other earthquakes in California.

TABLE 1

LOCAL MAGNITUDE, M_L , FOR THE 1979 IMPERIAL VALLEY EARTHQUAKE DETERMINED FROM STRONG-MOTION ACCELEROGRAMS—CALIFORNIA DATA

Ref. No.*	Station	Component	$PP/2^\dagger$ (m)	T^\ddagger (sec)	d_1 (km)	M_{L1}	d_2 (km)	M_{L2}	d_3 (km)	M_{L3}	d_4 (km)	M_{L4}
IIZ001	IMP BLD FF	N02E	43.1	1.3	7.00	6.07	29.0	6.69	31.0	6.77	13.0	6.19
		S88E	57.3	1.9		6.20		6.82		6.90		6.32
IIZ003	El Centro 7	S50W	117.0	1.9	0.60	6.47	28.0	7.09	30.0	7.17	10.0	6.57
		S40E	75.8	1.0		6.28		7.00		6.90		6.38
IIZ004	El Centro 6	S50W	75.5	3.2	1.20	6.28	28.0	6.90	30.0	6.98	11.0	6.40
		S40E	71.0	2.0		6.25		6.87		6.95		6.37
IIZ005	Bonds Corner	S50W	78.2	0.7	2.90	6.29	7.40	6.34	14.0	6.47	11.0	6.41
		S40E	72.5	0.7		6.26		6.31		6.44		6.38
IIZ006	El Centro 8	S50W	49.1	1.6	3.70	6.09	28.0	6.71	30.0	6.79	10.0	6.19
		S40E	61.8	1.7		6.19		6.81		6.89		6.29
IIZ007	El Centro 5	S50W	93.1	2.4	3.80	6.37	29.0	7.03	31.0	7.11	11.0	6.49
		S40E	51.1	1.2		6.11		6.77		6.85		6.23
IIZ008	E. C. D. ARY	N00E	62.6	1.4	6.30	6.22	28.0	6.82	30.0	6.90	12.0	6.34
		N90W	55.2	1.9		6.17		6.76		6.84		6.28
IIZ009	El Centro 4	S50W	67.3	3.2	6.60	6.26	28.0	6.85	30.0	6.93	12.0	6.37
		S40E	65.1	1.0		6.25		6.83		6.91		6.35
IIZ010	Brawley A.P.	N45W	39.6	1.3	8.60	6.07	43.0	7.06	45.0	7.10	26.0	6.54
		S45W	31.0	2.0		5.96		6.95		6.99		6.43
IIZ011	Holtville	N45W	36.7	2.4	8.60	6.04	21.0	6.31	24.0	6.43	8.80	6.04
		S45W	51.9	2.5		6.19		6.46		6.58		6.19
IIZ012	El Centro 10	S50W	36.3	2.0	8.00	6.02	28.0	6.58	31.0	6.70	13.0	6.12
		S40E	53.6	1.7		6.19		6.75		6.87		6.29
IIZ013	Calexico	N45W	23.7	1.4	10.0	5.88	18.0	6.04	21.0	6.12	11.0	5.90
		S45W	27.0	0.5		5.93		6.09		6.17		5.95
IIZ014	El Centro 11	S50W	38.0	1.2	12.0	6.12	30.0	6.68	32.0	6.76	15.0	6.18
		S40E	44.5	1.7		6.19		6.75		6.83		6.25
IIZ015	El Centro 3	S50W	29.2	2.1	12.0	6.01	29.0	6.53	31.0	6.61	15.0	6.07
		S40E	46.5	1.6		6.21		6.73		6.81		6.27
IIZ016	Parachute	N45W	22.2	2.2	7.80	5.80	48.0	6.91	50.0	6.95	31.0	6.49
		S45W	17.5	1.3		5.70		6.80		6.84		6.38
IIZ017	El Centro 2	S50W	22.1	1.1	15.0	5.94	32.0	6.52	34.0	6.60	18.0	6.00
		S40E	47.1	1.1		6.27		6.85		6.93		6.33
IIZ018	El Centro 12	S50W	19.1	1.8	17.0	5.92	32.0	6.46	34.0	6.54	20.0	5.98
		S40E	19.8	1.7		5.94		6.45		6.56		6.00
IIZ019	Calipatria	N45W	13.7	1.3	18.0	5.80	57.0	6.88	58.0	6.90	41.0	6.56
		S45W	12.3	1.6		5.74		6.83		6.85		6.51
IIZ020	El Centro 13	S50W	12.0	1.7	20.0	5.80	34.0	6.34	36.0	6.40	22.0	5.86
		S40E	20.1	1.9		6.00		6.56		6.62		6.08
IIZ021	El Centro 1	S50W	9.05	2.0	21.0	5.70	35.0	6.21	37.0	6.30	24.0	5.82
		S40E	14.5	1.6		5.90		6.46		6.50		6.02
IIZ022	Superstition	S45E	7.43	0.8	16.0	5.49	58.0	6.63	59.0	6.65	42.0	6.31
		N45E	4.55	1.1		5.28		6.42		6.44		6.10
IIZ023	Plaster City	S45E	5.93	1.1	28.0	5.79	52.0	6.41	53.0	6.43	38.0	6.13
		N45E	3.57	0.9		5.57		6.19		6.21		5.91
IIZ034	Niland	N90E	14.0	1.2	22.0	5.93	67.0	6.95	68.0	6.95	51.0	6.77
		N00E	6.75	1.2		5.61		6.63		6.63		6.45
IIZ035	Westmorland	S00E	16.2	2.5	4.00	5.61	52.0	6.85	53.0	6.87	34.0	6.47
		N90E	17.7	2.5		5.65		6.89		6.91		6.51
IIZ036	Meloland	N00E	71.4	1.7	1.20	6.25	21.0	6.59	24.0	6.71	3.00	6.25
		N90W	84.4	2.2		6.33		6.67		6.79		6.33

* Haroun (1980a, b).

† $PP/2$ denotes $\frac{1}{2}$ of the maximum peak-to-peak amplitude (in meters) of the synthetic Wood-Anderson record.‡ T is the approximate period of the Wood-Anderson response at maximum amplitude.

IMPERIAL VALLEY EARTHQUAKE, 15 OCTOBER 1979

The locations of the strong-motion accelerograph sites used in the study of the Imperial Valley earthquake of 15 October 1979 are shown in Figure 1, along with the epicenter and the observed locations of surface faulting. The data shown in Figure 1 come from three different sources. The epicenter, the location of the faulting, and the majority of the accelerograms recorded in the United States are from the U.S. Geological Survey (Porcella and Matthiesen, 1979). Additional United States data, including free-field motions from the Meloland Overcrossing and the Imperial County Services Building, were made available by the State of California's Office of Strong-Motion Studies (1980). The strong-motion data from Mexico were obtained from the University of California, San Diego (Brune *et al.*, 1979; Brandow and Leeds, 1980). The accelerograms from all these sources were corrected by standard

TABLE 2
LOCAL MAGNITUDE, M_L , FOR THE 1979 IMPERIAL VALLEY EARTHQUAKE DETERMINED FROM
STRONG-MOTION ACCELEROGRAMS—MEXICAN DATA

Station	Component	$PP/2^*$ (m)	T^\dagger (sec)	d_1 (km)	M_{L_1}	d_2 (km)	M_{L_2}	d_3 (km)	M_{L_3}	d_4 (km)	M_{L_4}
Agrarias	NO3E	48.7	1.4	1.30	6.09	3.30	6.09	12.0	6.23	19.0	6.37
	N87W	45.2	1.6		6.06		6.06		6.20		6.34
Cerro Prieto	S57W	25.4	0.9	14.0	5.99	23.0	6.23	26.0	6.35	39.0	6.79
	S33E	17.9	0.7		5.83		6.07		6.19		6.63
Chihuahua	N12E	35.4	0.8	4.70	5.95	18.0	6.21	22.0	6.33	35.0	6.85
	N78W	48.7	1.0		6.09		6.35		6.47		6.99
Compuertas	N75W	11.3	0.6	13.0	5.61	24.0	5.91	27.0	6.03	38.0	6.47
Delta	N08W	47.0	1.5	11.0	6.19	34.0	6.93	36.0	6.99	50.0	7.27
	S82W	38.1	0.6		6.10		6.84		6.90		7.18
Cucapah	N85E	39.6	1.4	0.00	6.00	11.0	6.12	16.0	6.22	30.0	6.70
Victoria	N75E	8.58	1.0			44.0	6.41	46.0	6.45	60.0	6.73
	N15W	11.6	0.8				6.54		6.58		6.86
Aeropuerto	N00E	30.1	0.9	1.40	5.88	2.30	5.88	12.0	6.02	14.0	6.06
	N90W	43.5	1.4		6.04		6.04		6.18		6.22
Mexicali	N00E	28.2	0.9	8.40	5.92	9.80	5.95	16.0	6.07	14.0	6.03
	N90W	46.9	0.6		6.14		6.17		6.29		6.25

* $PP/2$ denotes $\frac{1}{2}$ of the maximum peak-to-peak amplitude (in meters) of the synthetic Wood-Anderson record.

$\dagger T$ is the approximate period of the Wood-Anderson response at maximum amplitude.

procedures (to vol. I stage in Hudson *et al.*, 1969 to 1976) and plotted for examination (Haroun, 1980a, b, and c). After removal of some spike-like errors in some of the digital recordings from Mexico, the accelerograms were used to synthesize Wood-Anderson responses according to the procedures given in Kanamori and Jennings (1978). The resulting seismograms are shown in Figure 2. In this figure, the synthetic records are all to the same scales of time and amplitude, and are arranged according to the measure of distance recommended below. It is seen in Figure 2 that the synthetic Wood-Anderson records have amplitudes ranging from over 100 m down to about 10 m. Relating this with Figure 1 and reports of the damage caused by the earthquake (Brandow and Leeds, 1980), it can be concluded that for this earthquake, potentially damaging motion was associated with Wood-Anderson responses of tens of meters or more, well beyond the range of all standard Wood-Anderson seismographs except the 4 \times torsion seismographs. This fact, which also holds for other earthquakes (see Tables 1 to 3 in Kanamori and Jennings, 1978) illustrates the

extent of the extrapolation involved in estimating characteristics of potentially damaging ground motion from standard seismographic records. The use of synthetic seismograms based on strong-motion accelerograms reduces this extrapolation.

Using the maximum (1/2 peak-to-peak) values of Wood-Anderson response shown in Figure 2, values of M_L were determined using four different measures of distance, Δ . The results are shown in Figure 3, a and b. The four distances used, which are identified on the figure, are: d_1 , the closest distance to the surface trace of the fault; d_2 , the epicentral distance; d_3 , the hypocentral distance; and d_4 , the distance to the center of faulting, usually referred to as the center of energy release. The data shown in Figure 3 are included in Tables 1 and 2.

There is a general trend for the value of M_L in Figure 3 to increase with all measures of distance; (except for d_1) this feature will be discussed later in conjunction with the data from several other earthquakes. Concentrating on the trends seen when the different measures of distance are employed, some features can be identified. In the California data, for example, the use of the epicentral or hypocen-

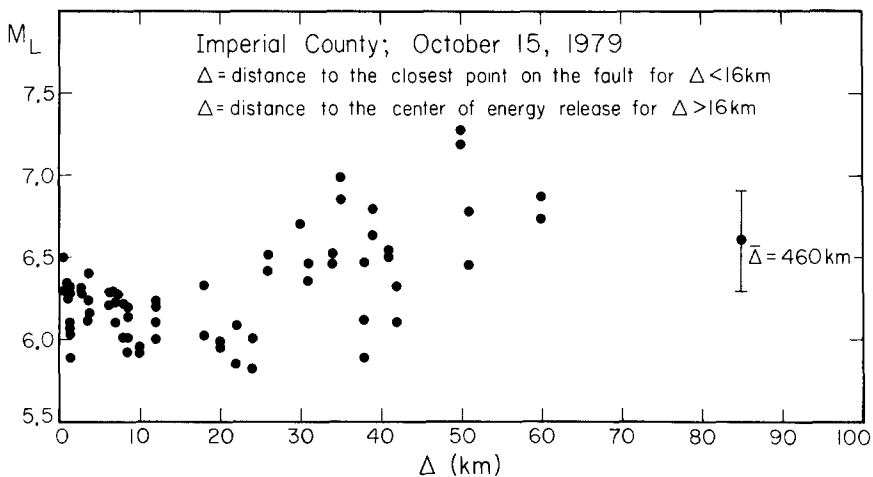


FIG. 4. Values of M_L for the Imperial Valley earthquake of 15 October 1979, all stations. The distance used is the closest distance to the fault for stations inside a circle whose diameter (32 km) is the length of faulting, and whose center is the center of faulting. Outside this circle, Δ is the distance to the center of the circle. The error bar indicates the standard deviation of the values obtained at seven stations within a distance range from 270 to 610 km.

tral distances, d_2 or d_3 , leads to a vertical clustering of data near 28 or 30 km. These data points are from the array crossing the fault at El Centro. If the closest fault distance d_1 is used, or the center-of-faulting distance d_4 , the data from the linear array appears in the near-field, from 0 to 25 km. In this case, the data have less scatter and show a trend to decrease with distance that is believed to be due, in part, to the azimuthal radiation pattern of the shear waves, as the more distant stations are near shear-wave nodal lines, and, in part, to a systematic decrease in M_L , discussed later. These trends, particularly the vertical stacking of M_L for d_3 and d_2 , are not seen in the Mexican data, Figure 3b. Because the epicenter was near the border, as was the closest surface faulting (see Figure 1), the differences in M_L as a result of the use of different measures of distance are less significant for the data from Mexico.

In judging the merits of the different measures of distance, the primary criteria are the consistency of the resulting values of M_L and the consistency with the expected radiation pattern of the event. If a physically plausible measure of distance indicated a constant value of M_L with increasing distance, with minimal scatter, then the problem would be solved. The situation is not that clear, of course, but our examination of the data led us to conclude that the most consistent results occur if the closest distance to the fault, d_1 , is used for sites within a circle around the center of faulting whose diameter is the length of faulting (32 km in the case of the Imperial Valley earthquake). Outside of this circle, the choice of distance is not as critical and the distance to the center of the circle, i.e., the center of faulting, d_4 , is recommended. The values of M_L for the Imperial Valley earthquake using this measure of distance are plotted in Figure 4. This figure includes data from both California and Mexico. At a fixed distance, the range of the data is about one-half of a magnitude unit, occasionally more, and there is a tendency for the values of M_L to decrease with distance from 0 to about 20 km and then begin a gradual rise which continues at least to 50 km. The far-field value of M_L , determined by seismograms with an average distance of 460 km, is consistent with the data from strong-motion instruments in the 30- to 60-km range, but is somewhat higher than the near-field value of M_L indicated by the strong-motion data.

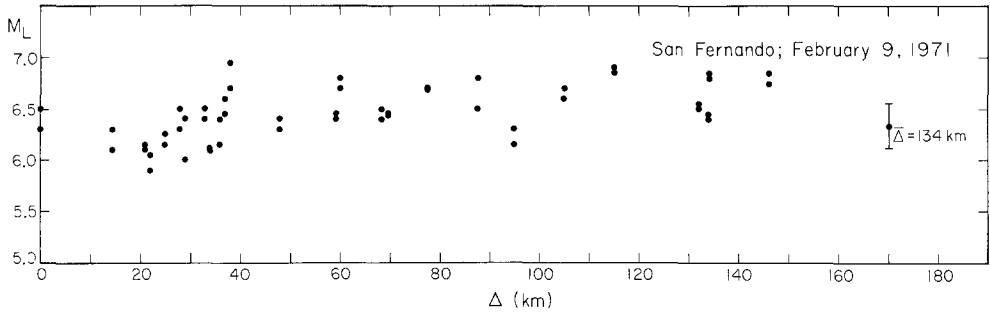


FIG. 5. Values of M_L from strong-motion data for the San Fernando earthquake of 9 February 1971. The distance, Δ , is defined in Figure 4. The error bar indicates the standard deviation of the values obtained at four stations within a distance range from 37 to 250 km.

These trends in the data for the Imperial Valley earthquake led us to look for similar trends in data from other earthquakes.

VALUES OF M_L FROM SEVERAL EARTHQUAKES

The values of M_L as a function of distance for several earthquakes are shown in Figures 5 through 11. In each case, the same measure of distance was used that was employed in the preparation of Figure 4. In many cases, particularly for more distant records from smaller earthquakes, all common measures of distance give about the same value. The data for these figures are taken from Kanamori and Jennings (1978), with the exception of the San Fernando earthquake for which additional data were prepared.

In the case of the San Fernando earthquake, the data are those included in Table 1 of Kanamori and Jennings (1978) plus the additional data given in Table 3. The additional accelerograms are from those digitized and processed by Hudson *et al.* (1969 to 1970). A total of 26 accelerograph sites were used. The additional 12 stations were selected to increase, to the extent possible, the data at larger distances and

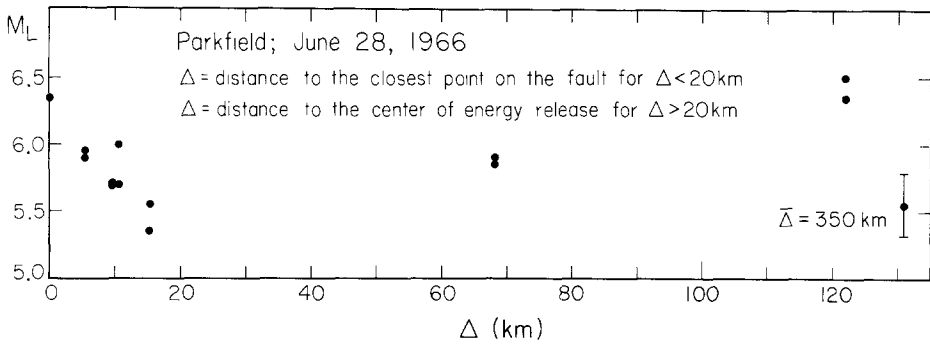


FIG. 6. Values of M_L from strong-motion data for the Parkfield earthquake of 28 June 1966. The distance, Δ , is as defined in Figure 4, with the diameter of the circle taken as 40 km. The error bar indicates the standard deviation of the values obtained at four stations within a distance range of 220 to 540 km.

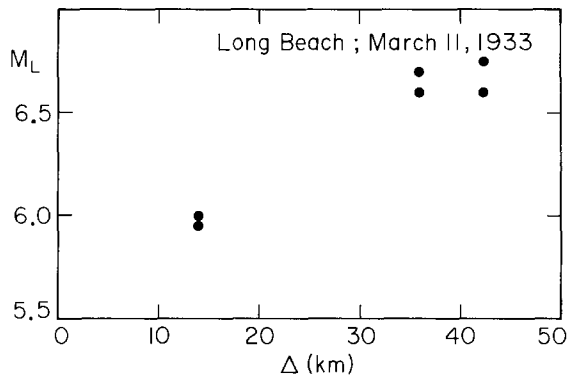


FIG. 7. Values of M_L from strong-motion data for the Long Beach earthquake of 11 March 1933. The distance, Δ , is defined in Figure 4.

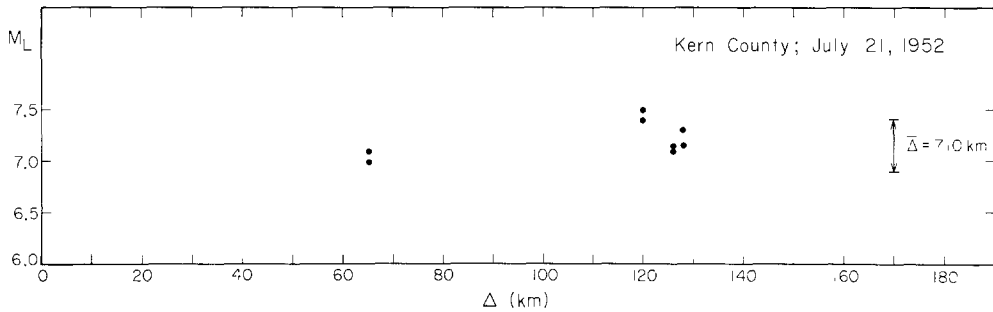


FIG. 8. Values of M_L from strong-motion data for the Kern County earthquake of 21 July 1952. The range of the two determinations at $\Delta = 630$ and 790 km is indicated by a vertical arrow.

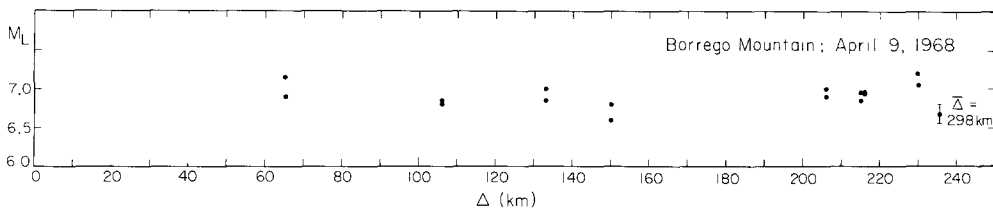


FIG. 9. Values of M_L from strong-motion data for the Borrego Mountain earthquake of 9 April 1968. The distance, Δ , is defined in Figure 4. The error bar indicates the standard deviation of the values obtained at four stations within a distance range of 150 to 430 km.

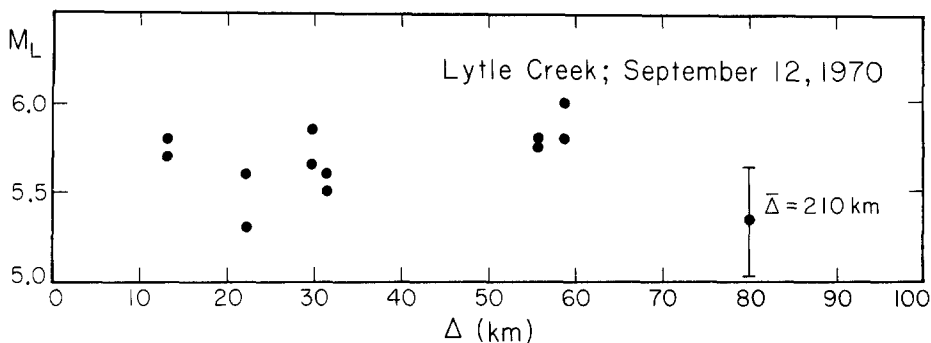


FIG. 10. Values of M_L from strong-motion data for the Lytle Creek earthquake of 12 September 1970. The distance, Δ , is defined in Figure 4. The error bar indicates the standard deviation of the values obtained at four stations within a distance range of 70 to 320 km.

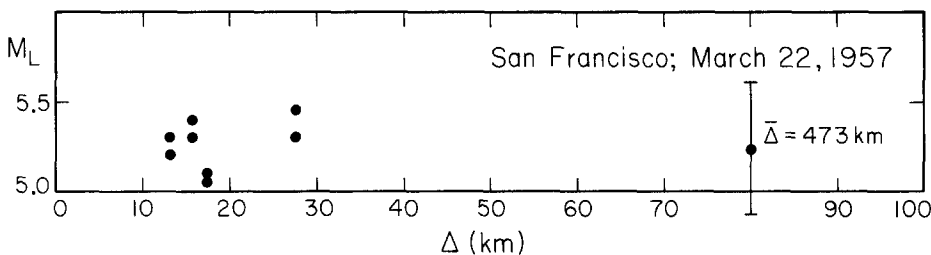


FIG. 11. Values of M_L from strong-motion data for the San Francisco earthquake of 22 March 1957. The distance, Δ , is defined in Figure 4. The error bar indicates the standard deviation of the values obtained at seven stations.

TABLE 3

LOCAL MAGNITUDE, M_L , FOR THE 1971 SAN FERNANDO EARTHQUAKE DETERMINED FROM STRONG-MOTION ACCELEROGRAMS—DATA ADDITIONAL TO KANAMORI AND JENNINGS (1978)

Station	Ref. No.*	Component	Δ (km)	$PP/2\ddagger$ (m)	$T\ddagger$ (sec)	M_L
Carbon Can Dam	N185	S50E	68.3	4.13	0.7	6.42
		S40W		5.23	0.5	6.52
Palos Verdes	N191	N65E	59.2	4.16	1.5	6.40
		S25E		4.55	1.0	6.44
Wrightwood	N183	N65W	69.8	4.32	0.8	6.44
		N25E		4.32	0.5	6.44
Oso Pump Plant	F104	N90W	60.0	7.94	1.3	6.70
		N00E		9.16	1.4	6.77
Costa Mesa	P220	S00W	8.78	3.54	1.5	6.51
		N90E		6.88	1.0	6.79
S.J. Capistrano	N195	N33E	115.0	5.88	0.7	6.87
		N57W		6.40	1.1	6.91
S. Bernardino	O206	N00E	105.0	4.52	0.8	6.71
		N90E		3.64	0.8	6.61
San Onofre	L171	N57W	132.0	2.27	1.2	6.56
		N33E		2.08	1.4	6.52
Port Hueneme	P222	S00W	77.5	6.42	2.4	6.68
		S90W		6.39	1.1	6.68
Hemet	O210	S45W	146.0	3.79	0.6	6.84
		S45E		2.95	0.6	6.73
Wheeler Ridge	E071	N90E	96.0	1.97	1.4	6.29
		S00W		1.45	0.9	6.16
Taft	P225	S69E	134.0	1.94	1.5	6.49
		N21E		1.86	1.6	6.47

* Hudson *et al.* (1969–1976).

† $PP/2$ denotes $\frac{1}{2}$ of the maximum peak-to-peak amplitude (in meters) of the synthetic Wood-Anderson record.

‡ T is the approximate period of the Wood-Anderson response at maximum amplitude.

The sparser data sets from the other earthquakes, Figures 7 through 11, are discussed next. In general, the data in each case are too meager to establish trends, so these sets of data were examined from the viewpoint of whether the trends seen in data from the Imperial County, San Fernando, and Parkfield earthquakes were consistent with the remaining data. The tendency for M_L to decrease in the near-field to a low around 20 km and thereafter to rise appears not to be contradicted by the sparse data from these other earthquakes. This is clearly so for the Long Beach data shown in Figure 7. Nor do the Kern County data, although very sparse, contradict this trend. The Borrego Mountain data are more numerous than the

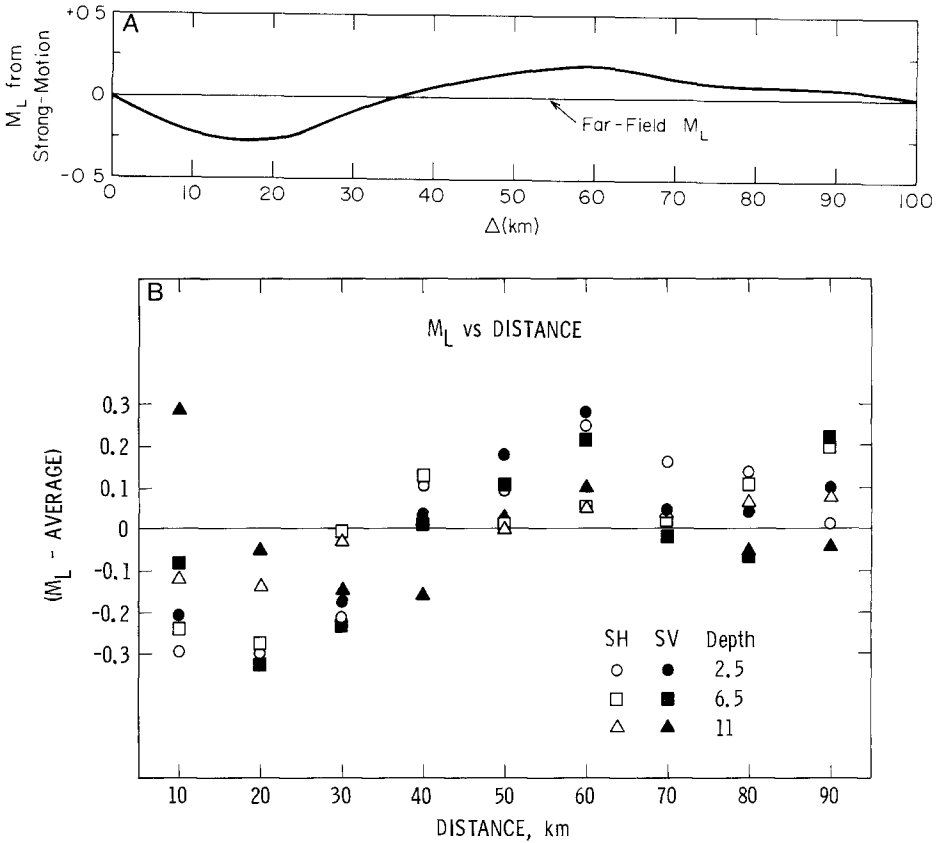


FIG. 13. Trends in values of M_L from near-field motion: (A) from the results of this study using strong-motion data; (B) from numerical studies by Hadley *et al.* (1982).

Kern County data; they show a similar, roughly constant trend in the range beyond 60 km. The data from the smaller earthquakes (Lytle Creek, 1970 and San Francisco, 1957) also are consistent with the trends seen in the three larger data sets; in the case of Lytle Creek, the data are mildly supportive, whereas those from San Francisco, although not contradictory, are not of much significance to the present discussion.

The tendency for the value of M_L to decrease with distance to a low point near 20 km and then to rise at greater distances is clear in those earthquakes where the data are most abundant. In addition, this trend is at least not contradicted by the other

earthquakes for which the data are less numerous. This leads us to suggest that there is a systematic effect of distance in the values of M_L calculated from strong ground motion and that a correction to the commonly used attenuation curves for Wood-Anderson response is warranted. This is particularly the case for engineering applications of local magnitude, wherein M_L is often used as a determinant in setting the level of ground motion for design. The nature of the correction thought required is shown in Figure 13a. Using the far-field value of M_L as a reference, the correction inferred from the strong-motion data is zero at zero distance, but dips to about $-1/4$ unit near 15 to 20 km, then rises gradually to a high point of $+1/4$ unit at around 60 to 70 km. The details of the curve shown in Figure 13a, including the approach to zero for distances beyond 70 km, are based both on the strong-motion data and on the desire to have the suggested revision of the attenuation curve used to determine M_L be relatively smooth. Based on the strong-motion data alone, it would not be inconsistent to continue the $+1/4$ unit correction near 60 km in Figure

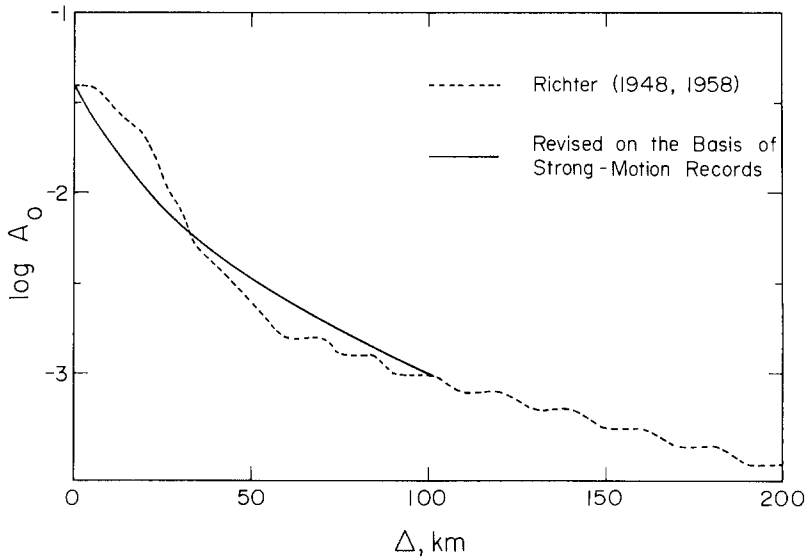


FIG. 14. Revised curve of $\log_{10}A_0$ versus Δ for determination of local magnitude, M_L . Numerical values of the revision are given in Table 4.

13a on out to 100 km and beyond. This point will have to await data from future earthquakes.

COMPARISON WITH NUMERICAL RESULTS

The discussion to this point is based entirely on empirical observations. It is interesting, therefore, to compare our result with that obtained numerically by Hadley *et al.* (1982). These authors computed theoretical transfer functions of seismic signals for a crustal model appropriate for southern California. They assumed that an accelerogram recorded at a short distance ($\Delta = 5.75$ km) from the 1975 Horse Canyon, California, earthquake ($M_L = 4.8$) represents the source function of an earthquake. By convolving the calculated transfer function with this source function, a Q function ($Q_B = 300$ was assumed) and the Wood-Anderson instrument response, they computed M_L at various distances. Their results are shown in Figure 13B. Open

and closed symbols show the results for *SH* and *P-SV* components, respectively. Although the value of M_L varies considerably depending upon the depth of the source and the wave type, the overall trend is very similar to that which we found empirically. As Δ increases, the value of M_L decreases to a minimum at $\Delta = 20$ km, and then increases to a maximum at $\Delta = 60$ km. The range of M_L is about 0.5 unit.

REVISED ATTENUATION CURVE

On the basis of our empirical results, as well as the numerical results of Hadley *et al.* (1982), we revised Richter's attenuation curve as shown in Figure 14 and Table 4. In view of the various uncertainties involved in the determination of local magnitude, we tried to remove only the average trend in the M_L versus Δ curves

TABLE 4
REVISED ATTENUATION CURVE, $-\log_{10}A_0(\Delta)$, FOR
DETERMINATION OF LOCAL MAGNITUDE, M_L

km	$-\log_{10} A_0(\Delta)$	Difference*
0	1.40	0.00
5	1.58	-0.18
10	1.72	-0.22
15	1.86	-0.26
20	1.98	-0.28
25	2.08	-0.18
30	2.18	-0.08
35	2.26	0.04
40	2.34	0.06
45	2.40	0.10
50	2.47	0.13
55	2.53	0.17
60	2.60	0.20
65	2.65	0.15
70	2.70	0.10
80	2.80	0.10
85	2.86	0.04
90	2.91	0.09
95	2.96	0.04
100	3.00	0.00

* From the standard attenuation curve [Richter (1935, 1958)] shown in Figure 14.

obtained for various earthquakes, rather than the trend observed for any individual event.

DISCUSSION

There are two major results of the present study. The first relates to the most consistent measure of distance for determination of M_L from near-field records and the related problem of the use of distance in estimating the strength of ground motion at a given site in the event of an earthquake of a specified local magnitude. The second problem arises in determining the seismic design criteria for major projects. The data from the Imperial Valley earthquake are particularly well-suited to investigate this question, whereas previous data have been less suitable.

Our investigations led us to conclude that the most consistent results are obtained

if the closest distance to the surface trace of the fault is used for sites located within a circle whose diameter is equal to the length of faulting, and whose center is the center of faulting. For sites outside of this circle, the measure of distance used is not as critical, but the distance to the center of faulting, the center of the aforementioned circle, is recommended.

The second result concerns the consistency of M_L , as a function of distance. For sites with Δ less than about 25 km, the standard Wood-Anderson seismograph goes off-scale, and the values used in the standard attenuation curve are based on the response of the 4 \times torsion seismometer, whose properties are different from the standard Wood-Anderson instrument. The strong-motion accelerometer data allow determination of the Wood-Anderson response in the near-field via the use of accurate, synthetic seismograms. The best data sets for examining the variation of M_L are from the Imperial Valley, San Fernando, and Parkfield earthquakes. Data from these earthquakes show that at $\Delta = 0$, the value of M_L is essentially equal to the far-field value. As Δ increases, the value of M_L drops to about 1/4 unit below this value at a distance near 20 km, then rises to about 1/4 unit higher than the far-field value at around 50 km. Beyond 50 km, the trend is less clear; the values of M_L appear to remain high for an appreciable distance. This trend in M_L is either mildly supported by, or at least not contradicted by, similar data from several other earthquakes. In addition, it is consistent with numerical results obtained independently by Hadley *et al.* (1982).

To eliminate this observed trend in the values of local magnitude determined from strong-motion accelerograms recorded in the near-field of major earthquakes, a revised version of the standard attenuation curve, $-\log_{10}A_0(\Delta)$, is presented in Figure 14 and Table 4. This revision removes the trend observed from the strong-motion data and smooths the standard curve somewhat in the range $0 \leq \Delta \leq 100$ km, the range of the proposed revision.

Using the revised attenuation curve, Heaton (personal communication, 1981) has recalculated the local magnitudes of four major southern California earthquakes. The recalculated values are averages, and use the computed values of Wood-Anderson response presented here and in Kanamori and Jennings (1978). The results are: San Fernando, 9 February 1971, 6.4; Imperial Valley, 15 October 1979, 6.4; Borrego Mountain, 9 April 1968, 6.9; and Kern County, 21 July 1952, 7.2. The values are within 0.1 unit of those reported in our 1978 paper; larger changes, up to 0.25, could be expected when only one or two records are used to determine M_L .

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REFERENCES

- Boore, D. M. (1980). On the attenuation of peak velocity, *Proc. of the Seventh World Conf. on Earthquake Engrng.*, vol. II, Turkish National Committee on Earthquake Engineering, Istanbul, Turkey, 577-584.
- Brune, J., J. Prince, F. Vernon, III, E. Mena, and R. Simons (1979). Strong-motion data recorded in Mexico, in *Imperial Valley Earthquake of October 15, 1979, U.S. Geol. Surv. Profess. Paper 1254* (in press).
- Brandow, G. (Coordinator) and D. J. Leeds (Editor) (1980). Reconnaissance Report, Imperial County, California earthquake, October 15, 1979, Earthquake Engineering Research Institute, 194 pp.

- Espinosa, A. F. (1980). Attenuation of strong horizontal ground accelerations in the western United States and their relation to M_L , *Bull. Seism. Soc. Am.* **70**, 583-616.
- Gutenberg, B. and C. F. Richter (1942). Earthquake magnitude, intensity, energy, and acceleration, *Bull. Seism. Soc. Am.* **32**, 163-191.
- Hadley, D. M., D. V. Helmberger, and J. A. Orcutt (1982). Peak acceleration scaling studies, *Bull. Seism. Soc. Am.* **72**, 959-979.
- Haroun, M. (1980a). Corrected accelerograms, Imperial Valley earthquake of October 15, 1979, strong motion data recorded by the U.S. Geological Survey, Earthquake Engineering Research Laboratory, California Institute of Technology, Pasadena, California.
- Haroun, M. (1980b). Corrected accelerograms, Imperial Valley earthquake of October 15, 1979, recorded motions of the Imperial County Services Building, Earthquake Engineering Research Laboratory, California Institute of Technology, Pasadena, California.
- Haroun, M. (1980c). Corrected accelerograms, Imperial Valley earthquake of October 15, 1979, strong motion data recorded in Mexico, Earthquake Engineering Research Laboratory, California Institute of Technology, Pasadena, California.
- Hudson, D. E., M. D. Trifunac, and A. G. Brady (1969 to 1976). Analysis of strong-motion accelerograms, vol. I, parts A-Y; vol. II, parts A-Y; vol. III, parts A-Y; vol. IV, parts A-Y; Index vol. (EERL Report No. 76-02), Earthquake Engineering Research Laboratory, California Institute of Technology, Pasadena, California.
- Jennings, P. C. and H. Kanamori (1979). Determination of local magnitude, M_L , from seismoscope records, *Bull. Seism. Soc. Am.* **69**, 1267-1288.
- Kanamori, H. and P. C. Jennings (1978). Determination of local magnitude, M_L , from strong-motion accelerograms, *Bull. Seism. Soc. Am.* **68**, 471-485.
- McJunkin, R. D. and J. T. Ragsdale (1980). Compilation of strong-motion data from the Imperial Valley earthquake of 15 October 1979, Preliminary Report 26, Office of Strong-Motion Studies, California Division of Mines and Geology.
- Porcella, R. L. and R. B. Matthiesen (1979). Preliminary summary of the U.S. Geological Survey strong-motion records from the October 15, 1979 Imperial Valley earthquake, *U.S. Geol. Surv. Open-File Rept. 79-1654*, 41 pp.
- Richter, C. F. (1935). An instrumental earthquake scale. *Bull. Seism. Soc. Am.* **25**, 1-32.
- Richter, C. F. (1948). *Publ. Bureau Central Seismologique International, Ser. A* **17**, 217-224.
- Richter, C. F. (1958). *Elementary Seismology*, W. H. Freeman, San Francisco, 768 pp.

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