

Quantum efficiency enhancement by photon recycling with backscatter evasion

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The non-unity quantum efficiency (QE) in photodiodes (PD) causes deterioration of signal quality in quantum optical experiments due to photocurrent loss as well as the introduction of vacuum fluctuations into the measurement. In this article, we report that the QE enhancement of a PD was demonstrated by recycling the reflected photons. The effective external QE for an InGaAs PD was increased by 2–6% over a wide range of incident angles. Moreover, we confirmed that this technique does not increase backscattered light when the recycled beam is properly misaligned. © 2017 Optical Society of America

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Introduction — The quantum efficiency (QE) of photodiodes (PDs) is the measure of photon-to-carrier conversion efficiency. High QE PDs are particularly important in optical experiments where very small signals are handled or where the introduction of vacuum fluctuations due to optical losses are detrimental, such as gravitational wave detection and quantum optical experiments. In optical squeezing experiments [1, 2], in particular, the vacuum fluctuations induced by optical loss deteriorates the achievable squeezing level.

The reduction of the QE in a PD is caused by internal and external mechanisms. The internal loss comes from loss of photoconductive carriers in the PD substrate due to, e.g. free carrier absorption [3] and electron-hole pair recombination [4]. Since the internal loss is limited by the material properties and structure of the PD, it can be reduced by careful material growth and device design [5]. External loss is the loss of incident photons due to surface reflection and scattering.

In the technique described herein, the photons reflected by the surface of the PD are reflected back into the PD using a high reflectivity (HR) mirror. With careful misalignment of the HR mirror, the backscattering from the recycled beam can be suppressed. We call this technique *photon recycling*.

Various techniques have previously been proposed for reduction of the external loss: photodiode traps [6, 7], external light trapping for photovoltaic modules [8], resonant cavity enhanced photonic devices [9], and a PD with a custom anti-reflection coating [10]. The photon recycling technique has several advantages over these other techniques. This technique can be realized with a single PD and a simple mirror, and thus has an advantage in terms of the noise compared to the case that involves multiple PDs or a specifically designed light guide. This technique can be applied to off-the-shelf commercial PDs. The QE can be increased over a broad wavelength range by employing a broadband HR mirror.

In this article, the increase of the effective QE for an indium-gallium-arsenide (InGaAs) PD was demonstrated at 1064-nm. In addition, the backscattering from the PD and the photon recycling technique was experimentally evaluated. Similar technique to increase an external QE with a retroreflector was used in the previous experiments [11–13]. Our technique specifically includes the mitigation of backscattering. It was quantitatively confirmed that the technique does not significantly increase the backscattering into the upstream optics. This is a critical noise source to overcome when seeking ultra-low phase noise in quantum metrology.

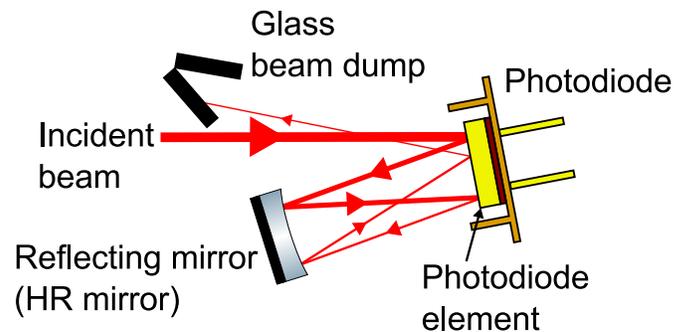


Fig. 1. Schematic of the photon recycling technique. This figure shows a 2-fold recycling case.

The general idea of photon recycling is depicted in Fig. 1. The incident beam (the primary beam hereafter) is mostly absorbed

by the substrate of a PD, while a part of the primary beam is reflected (the primary reflection). The primary reflection is sent back to the PD by a high reflecting mirror (RM). This beam (the secondary beam) is again mostly absorbed by the PD, increasing the effective QE. A part of the secondary beam is reflected by the PD and becomes the secondary reflection. This photon recycling technique can be extended to multi-fold recycling as shown in the figure. Here, the incident angle of the recycled beams is assumed to be the same as that of the primary beam. The secondary beam gives the dominant QE increase of $\eta_{\text{ext}} R_{\text{pd}} R_{\text{rm}}$, where η_{ext} , R_{pd} , and R_{rm} are the external QE of the PD, the reflectivity of the PD, and the reflectivity of the RM, respectively. When the folding number is increased, the eventual effective QE approaches $\eta_{\text{ext}} / (1 - R_{\text{pd}} R_{\text{rm}})$. If we consider the simplest case with zero scatter loss from the PD (i.e. $R_{\text{pd}} = 1 - \eta_{\text{ext}} / \eta_{\text{int}}$, where η_{int} is the internal QE of the PD), and a perfect RM (i.e. $R_{\text{rm}} = 1$), the external loss is recovered and the eventual effective QE agrees with the internal QE (η_{int}).

Backscattering — Scattered light can be a phase noise limit in sensitive optical setups like interferometers for precision measurement [14–16]. The backscattering from PDs is particularly difficult to mitigate as optical attenuation is, in most cases, not allowed. The best way to reduce the scattering is to make the spot size smaller than the aperture size of the PD and tilt the PD away from the incident beam. Photon recycling risks increasing the amount of the backscattered light. For example, when the RM is aligned to reflect the primary reflection back into the same path, the secondary reflection directly goes back to the main optical instrument along the path of the primary beam. In practice, the backscattered field is composed of the light of the primary and secondary beams. Our target is to reduce the contribution of the secondary beam to be smaller than the one from the primary beam. The Gaussian beam overlap of the back reflection can be sufficiently reduced by tilting the RM by a few degree as well as the careful design of the beam parameters, especially the divergence angle. The backscattering is a function of the scattering angle and depends on the surface condition of the PD. Although the characterization of the scattering requires experimental evaluation, the scattered field, in general, goes smaller as the scattering angle becomes larger. Thus, reduction of the backscattering requires proper choice of the angle of the RM. In addition, the eventual reflection that exits from the PD must be blocked by a beam dump to prevent acoustic coupling from the environment.

Experimental setup — Figure 2 shows the experimental setup for demonstration and evaluation of photon recycling. The target PD was an InGaAs PD with an active area of 3 mm (Excelitas, C30665GH), whose glass window was removed. The nominal incident angle (θ_i) of the primary beam was 15 deg. The RM was a 12.7 mm mirror with a reflectivity higher than 99.5%, and a concave radius of curvature (RoC) of 25 cm. The RM was placed at 20 mm from the PD to form single-fold photon recycling. With this reflection geometry, the loss caused by large angle scattering that could not be sent back into the PD was estimated to be $< 0.06\%$ and by integrating the scattering shown in Fig. 4. To dump the secondary reflection, an iris was placed 50 mm upstream from the PD. The light source was a Nd:YAG NPRO laser (Lightwave Electronics, M126N-1064-500) with a wavelength of 1064 nm. The output beam went through a 5 m long polarization maintaining single-mode (PM-SM) fiber for spatial mode cleaning. The primary beam power was adjusted to be 11 mW by a half wave plate (HWP1) and a polarizing beam splitter (PBS1). The incident polarization on the PD was adjusted by another

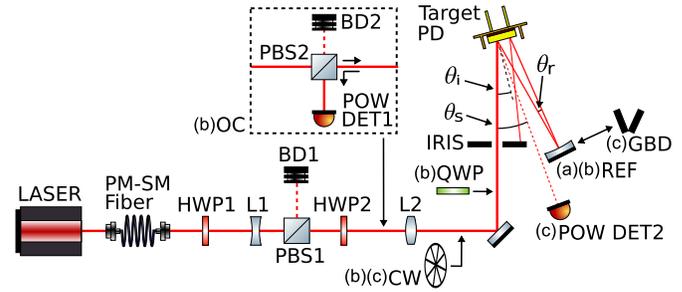


Fig. 2. Experimental setup. HWP, half wave plate; L, lens ($f = -200$ mm and $f = 150$ mm for L1 and L2, respectively); PBS, polarizing beam splitter; BD, beam dump; CW, chopping wheel; QWP, quarter wave plate; RM, reflecting mirror; GBD, black glass beam dump; POW DET, photodetector for power measurements; OC, optical circulator. Components labeled (a), (b), or (c) were used for respective measurements: (a) QE, (b) back-scattering, and (c) bidirectional reflectance distribution. The input and output optics for the PM-SM fiber have been omitted.

half wave plate (HWP2).

For reducing the Gaussian beam overlap between the primary and secondary beam, the divergence angle was designed to be less than 10% of the reflection angle (θ_r). This was also made large enough to reduce the contribution of the scatter from the secondary beam within the solid angle of the PD. Based on this criterion, we chose a beam separation of 1.5 mm. We placed the beam waist close to the PD to keep the beam size small enough for the PD. Consequently, θ_r was 4.3 deg, the waist position was upstream of the PD by 50 mm, and the waist radii of the primary and secondary beams were $80 \mu\text{m}$ and $110 \mu\text{m}$, respectively. Note that θ_r was adjusted to keep the resultant distance of the two beams (1.5 mm) depending on θ_{in} and the secondary beam waist does not exit in the actual optical path. The waist sizes of the primary and secondary beams correspond to divergence angles of 0.24 deg and 0.17 deg, respectively, which are less than 10% of θ_r . Two lenses, L1 and L2, and the RM were used to shape the beam. With this setup, the Gaussian beam overlap in this experiment was calculated to be negligibly small. As for the scattering, the contribution of the secondary beam with properly set θ_r was suppressed below the primary beam contribution as discussed later.

QE measurement — The QE of the PD was measured with an incident angle of θ_i scanned from 10–60 deg. The QEs were compared with and without the presence of the RM. The results for each incident polarization are shown in Fig. 3. The QEs without the RM were measured to be 86–92%, and the dependence on the PD reflectivity is clearly visible. The QEs with the RM placed were measured to be 92–94% independently of the polarizations, showing enhancement of the QE and less sensitivity to the incident angle. If the scattering and reflection losses are negligible, the enhancement of the external QE with the RM is estimated to be $\eta_{\text{ext}}(1 + R_{\text{pd}})$ and is shown in the figure. The difference between the incident angles of the primary and secondary beams affects the enhancement of the QEs less than 0.1% and can be neglected. The gap between the measured and estimated QE with the RM is less than 1% for $\theta_i \leq 50$ deg.

The statistical error of the QE measurement comes from the fluctuation of the measurement values. Besides the statistical error plotted in the figure, the absolute level of the QE has a

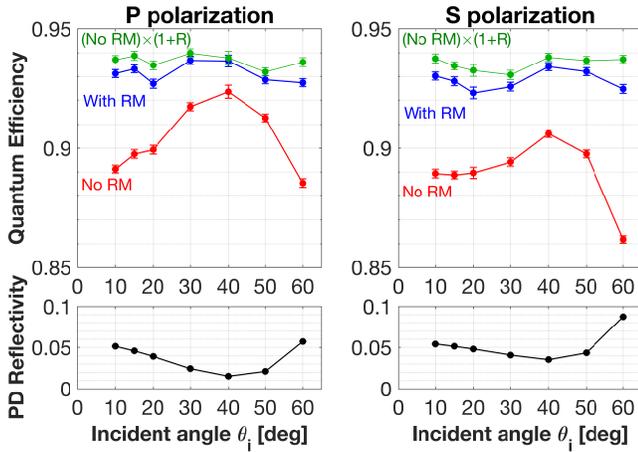


Fig. 3. Dependence of QE and reflectivity on incident angle and polarization. The upper and lower panels show QE and reflectivity, respectively. The left and right panels show the p-polarized and s-polarized cases, respectively.

systematic calibration error of 4%, which consists of the accuracy of the power meter for the incident power measurement (3%) and the accuracy of the transimpedance of the PD readout (2%). Although this calibration error may shift the curves up and down, this does not affect the relative difference between the measurements. The error of the reflectivity measurement is mainly composed of the systematic error of the photodetector for measuring the laser power of 2%. This error is negligibly small in the figure.

Backscattering evaluation — The effect of the backscattering is evaluated in terms of the bidirectional reflectance distribution function (BRDF), i.e. scattered light power density per solid angle normalized by the incident power, as

$$\text{BRDF} = \frac{P_s}{P_i \Omega \cos \theta_s}, \quad (1)$$

where P_s is the scattered light power, P_i is the incident light power, Ω is the detector subtending solid angle, and θ_s is the scattering angle [17].

The amount of the backscattered light was evaluated using an optical circulator and an optical chopper, as shown in Fig. 2-(b). The optical circulator was formed by a quarter wave plate (QWP) and polarizing beam splitter (PBS2) to separate backscattered light from the main beam path. The power of the separated light was measured by a power detector (POW DET; Thorlabs PDA100A). The chopper wheel (CW) was inserted downstream of PBS2 to modulate the incident light at 253 Hz, and the output of the power detector at the modulation frequency was obtained with a spectrum analyzer (Stanford Research Systems SR785). The optical chopping enables us to measure the reflected power at the modulation frequency where the dark noise of the detector is low. Also, the measurement removes the effects of spurious coupling of environmental illumination. The chopper in fact causes undesirable modulated reflection towards PBS2. Since the reflected field is P-polarized, PBS2 significantly attenuates it before it reaches the power detector.

For the purpose of evaluating the dependence of the backscattering light on the reflection angle θ_r , the measurements were carried out without the RM and with it placed at two different distances (20 mm and 50 mm) from the target PD. In the cases

Table 1. Measured BRDF for various RM distances, 20 and 50 mm. The BRDF measured without RM was used as reference to see the increment by adding the RM.

Distance of the RM (mm)	Reflection angle (deg)	BRDF (10^{-4} /sr)	
		Measured	Increment
No RM	—	8.3 ± 0.5	—
20	4.3	8.2 ± 0.5	-0.1 ± 0.7
50	1.7	9.4 ± 0.5	1.1 ± 0.8

with the RM, the beams separation at the PD was kept to be 1.5 mm. These configurations correspond to θ_r of 4.3 deg and 1.7 deg, respectively.

The measurement results are summarized in Table 1. When the reflection angle was 4.3 deg, there was no significant increase of the BRDF observed, while the case with 1.7 deg caused a visible but minor increase of BRDF. Thus, we can conclude that the secondary reflection does not produce a significant increase of the backscattering when the secondary beam is properly misaligned. Note that the errors were dominated by the systematic error of the power measurement for the incident power and the back scattered power.

BRDF measurement — The above conclusion can also be verified by examining the BRDF of the PD itself. This BRDF was measured with the setup shown in Fig. 2-(c). In the measurement, the primary beam was p-polarized at an incident angle of 15 deg, and chopped at 253 Hz. The scattered light power was measured with the power detector placed at various scattering angles (θ_s). In order to mitigate the influence of the scattering from the primary reflection, the primary reflection was blocked with a glass beam dump (GBD). The GBD consists of black welding glass and has low scattering thanks to its smooth surface.

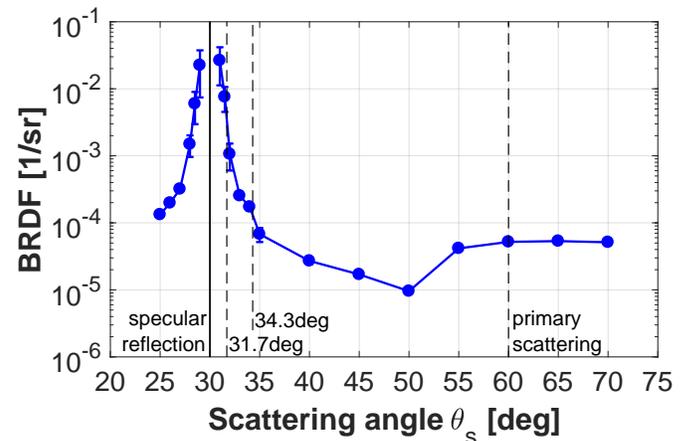


Fig. 4. Measured BRDF of the target PD at 15 deg incident angle for p-polarized light. The primary reflected beam is located at 30 deg (vertical thick line).

Figure 4 shows the measured BRDF of the PD. The remarkable feature is that the BRDF is high around the $\theta_s = 30$ deg. This angle corresponds to the specular reflection. Note that the measured points are located well outside of the Gaussian power distribution of the primary reflection. The BRDF falls rapidly

with θ_s away from the specular reflection and becomes flat above $\theta_s > 35$ deg.

Now we compare the contribution of the primary and secondary scattering to the BRDF. Since the measurement at $(\theta_s) < 25$ deg was geometrically restricted by the input optics, we assume the BRDF is symmetric with regard to $\theta_s - 30$ deg. Namely, we obtain $\text{BRDF}(0 \text{ deg}) = \text{BRDF}(60 \text{ deg}) = (5.2 \pm 0.5) \times 10^{-5}$. The contribution of the secondary beam is $R_{\text{pd}}(\theta_i) \times \text{BRDF}(2\theta_i + \theta_r)$. For $\theta_r = 4.3$ deg and 1.7 deg, the contributions of the secondary are $(6.5 \pm 0.8) \times 10^{-6}$ 1/sr and $(2.3 \pm 0.9) \times 10^{-4}$ 1/sr, respectively. This means that the scattering from the secondary beam was successfully reduced below the one from the primary beam when the misalignment angle was properly set.

The primary scattering inferred from the BRDF is about a factor of 16 smaller than the one obtained from the direct backscatter measurement in the second experiment. This excess may indicate that the direct backscatter measurement could have been dominated by the scattering from the input optics located upstream of the PD. Nevertheless our conclusion about the comparison of the primary and secondary scattering remains unchanged.

Conclusion — The photon recycling technique allows an enhancement of the external QE for a PD towards the limitation set by the internal QE by adding a reflecting mirror close to the PD. The effective external QE for an InGaAs PD was enhanced by 2–6% over a wide range of incident angles. The enhancement of the QE was consistent with the prediction from the reflectivity of the PD within 1% in terms of the QE. It was validated that the technique does not induce significant backscattering generated by the retro reflected scattered light when proper alignment is used. QE enhancement can be applied within a spectral range determined by the characteristics of the PD materials. For example, when absorption length of the diode is shorter than the thickness, interference effect should be considered. However, if the absorption length is too short, carrier-recombination effect may occur. It is also worth noticing that this technique requires a large enough diode and could limit the dynamic performances of the device. We expect that QE enhancement can be applied for Si PDs in visible wavelengths and for extended InGaAs PDs in the near infrared, e.g. 1.5–2.2 μm .

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