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An efficient compound OPO cavity with narrow bandwidth

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ABSTRACT

By integrating a free running cavity and a narrow bandwidth cavity, it is possible to create a compound OPO design which possesses the most desirable properties of each. In this example, we have combined a 355 nm-pumped idler-resonated free running type I BBO OPO cavity with a grating-narrowed signal-reinjection arm using only standard, low-cost optics. The output from such an implementation retains the high efficiency and low divergence of the free-running OPO, but its bandwidth is dictated by that of the high resolution cavity.

Key words: OPO, compound cavity

OPO cavities which produce high spectral resolution in a compact, rugged design are finding increasing use in a variety of spectroscopic and remote sensing applications¹. In many commercial approaches, high energy pulses with narrow bandwidths are produced by oscillator/amplifier layouts in which a first, low efficiency, cavity produces narrow band pulses that are subsequently amplified in additional stages². Recently, however, it has become clear that it is possible to combine the oscillation and amplification stages into a single design through the use of compound cavities in which the control of the narrow bandwidth and amplification processes are performed on separate branches of the parametric process³.

For example, the compound OPO cavity presented in Figure 1 is the combination of a free running OPO cavity (defined by mirrors Mo, Mi, Ms and Mr) and a narrow bandwidth OPO cavity (formed by the optical elements Mo, Mi, Ms, Grating and Mt). The free running OPO cavity is a singly resonant type I BBO OPO resonated on its idler wave⁴. The narrow bandwidth OPO cavity is also a singly resonant OPO, but it is resonated on the signal wave and builds upon the design of Bosenberg, Pelouch, and Tang (1989)⁵. The properties of the various optical elements are as follows: Mo -- A 0° high reflector for the pump, in our case the 355nm 3rd harmonic of a Nd:YAG laser; Mi -- A 45° 355 nm pump input coupler; Mr & Mt -- Aluminized metallic mirrors; Ms -- A high reflectivity optic for the signal beam, with high transmission for the idler wave; Grating -- 2700 groves/mm grating in a 88° Littman configuration.

The pump laser for the compound OPO cavity is the third harmonic (355 nm) of an injection-seeded Nd:YAG laser, whose pulse width is approximately 10 ns. The BBO crystal is cut for type I phase matching, is 15 mm in length, and has a broadband AR coating which covers the near-UV and optical range. Under a wide range of conditions, the bandwidth of the compound OPO is dictated by the grating-narrowed arm of the cavity, while the beam quality and the efficiency of the compound OPO cavity is mainly decided by the free running, idler resonated arm -- which has much higher efficiency and therefore dominates the amplification process. By resonating on the idler wave of the free running OPO, a small divergence for the OPO output is obtained. Thus, the compound cavity in Figure 1 is found to possess the same high conversion efficiency and good beam quality of a free running OPO, yet the same bandwidth as a grating-narrowed OPO.

Table 1 summarizes the efficiency and bandwidth of the compound cavity over the tuning range measured to date. A single grating was used in these experiments, and, including the idler-wave, complete coverage can be obtained from 440-1830 nm. Figure 2 shows the $\sim 0.35\text{cm}^{-1}$ bandwidth of the compound cavity at 466nm as measured by a Burleigh pulsed spectrum analyzer. Similar measurements across the complete tuning range demonstrate that the compound cavity consistently produces a bandwidth of less than 0.5cm^{-1} , while the total (signal + idler) efficiency is higher than 40% when the pump intensity is twice that of the threshold intensity (which is some $25\text{-}35\text{ MW/cm}^2$, or about 65-70 mJ for the 4.5 mm diameter 355 nm pump beam).

To summarize, the compound cavity presented herein fully utilizes the signal and idler beams generated in the OPO process to optimize and simplify the OPO design. The results demonstrated to date prove that compound OPO cavities allow efficient generation of widely tunable, narrow bandwidth parametric radiation while easing the demands place on the pump laser.

REFERENCES:

1. P.I. Ionov, I. Bezel, S.I. Ionov, C. Wittig, *Chem. Phys. Lett.*, 272, 257-264 (1997)
2. B.C. Johnson, V.J. Newell, J.B. Clark, E.S. McPhee, *J. Opt. Soc. Am. B*, 12, 21222-21227 (1995)
3. Y. Zhou, Z.Y. Xu, D.Q. Deng, Y.F. Kong, X.A. Zhu, Z.H. Yan, *J. Opt. Soc. Am. B*, 14, 1496-1500 (1997)
4. S. Wu, G.A. Blake, Z.Y. Sun, J.W. Ling, *Appl. Optics* 36, 5898-5901, (1997)
5. W. R. Bosenberg, W.S. Pelouch and C.L. Tang, *Appl. Phys. Lett.* 55, 1952-1954 (1989)

Table 1. Performance of the compound cavity OPO

Wavelength	445nm	466nm	540nm	610nm	670nm
Bandwidth(cm^{-1})	0.45cm^{-1}	0.35cm^{-1}	0.35cm^{-1}	0.35cm^{-1}	0.30cm^{-1}
Efficiency	40%	42%	45%	46%	44%

The pump laser has a beam size of 4.5mm in diameter, and when pumped at 135mJ (~2 times above operation threshold), we measured the efficiency

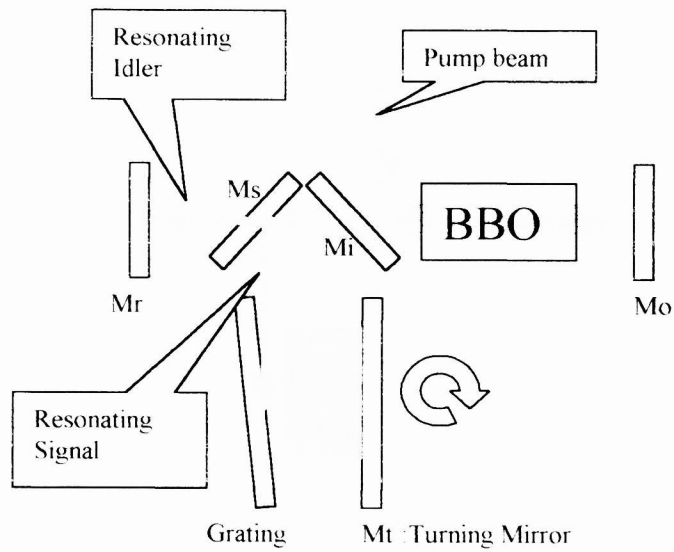


Figure 1.

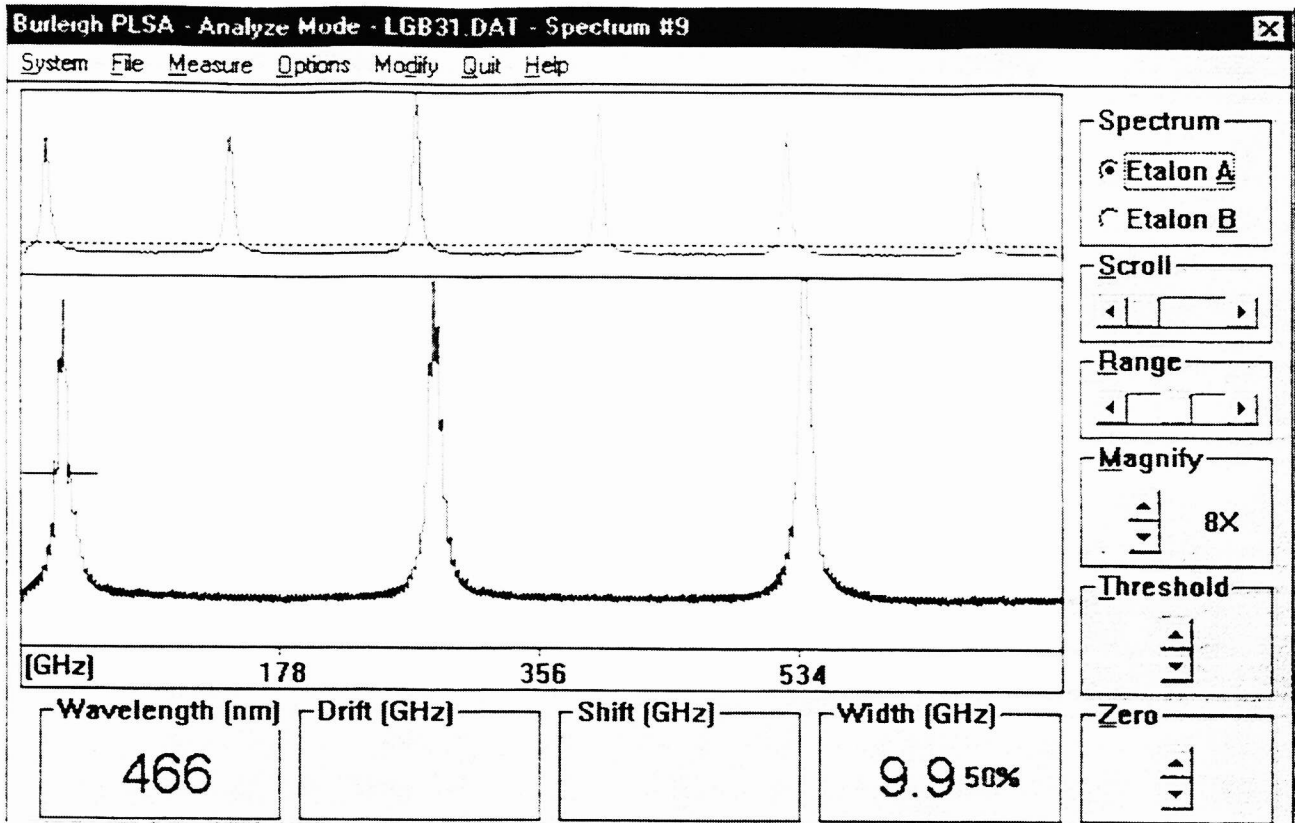


Figure 2. Bandwidth (Full width at half maximum) of the compound OPO cavity, measured with a Burleigh Pulsed Spectrum Analyzer. This plot is the average result of 50 shots in 5 seconds.